

QC
Avro
C-105
P/WT/20
Vol. III

QCX
Avro
CF105
P-WT-20
v.3 (25)

FILE IN VAULT

C-105 ANALYZED P/WIND TUNNEL/20
DERIVATIVES AND ZERO VALUES
VOLUME III
LATERAL CONTROL
Copy No. 2 June 1954
UNCLASSIFIED



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et de génie mécanique

TO
A

DATE

Dec. 7, 1992

Report no.: QCX - AVRO - CF105-P-WT-20 V.3

has been downgraded to: _____

de-classified

by (Name): Michel W. Drapeau

(Dept.): A/DND Coordinator, Access to Information

Date: Dec. 7, 1992

R. Anger
Signature



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A. V ROE CANADA LIMITED
MALTON - ONTARIO

TECHNICAL DEPARTMENT (Aircraft)

AIRCRAFT: C-105

REPORT NO. P/W.T./20

FILE NO:

NO OF SHEETS: _____

TITLE:

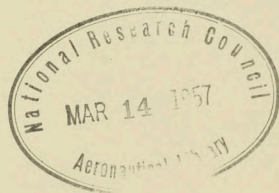
ANALYZED

DERIVATIVES AND ZERO VALVES

VOLUME III

LATERAL CONTROL

confirmed as:
 Classification ~~cancelled~~ / changed to: UNCLASSIFIED
 By authority of: DRDA 7/DARFT 5-8/DAS Eng 6-4-5
 Date: 5 Nov 1992
 Signature: B. Aubrey
 Unit / Rank / Appointment: DSIS 3, Secretary CRAD HQ DRP



PREPARED BY _____ DATE June 54
 CHECKED BY _____ DATE _____
 SUPERVISED BY _____ DATE _____
 APPROVED BY _____ DATE _____

ISSUE NO	REVISION NO	REVISED BY	APPROVED BY	DATE	REMARKS

45116

12416802

FORM 1316A

TECHNICAL DEPARTMENT (Aircraft)

REPORT No F/W.T./20

SHEET No 1

AIRCRAFT

PREPARED BY

DATE

J. Clark

June 54

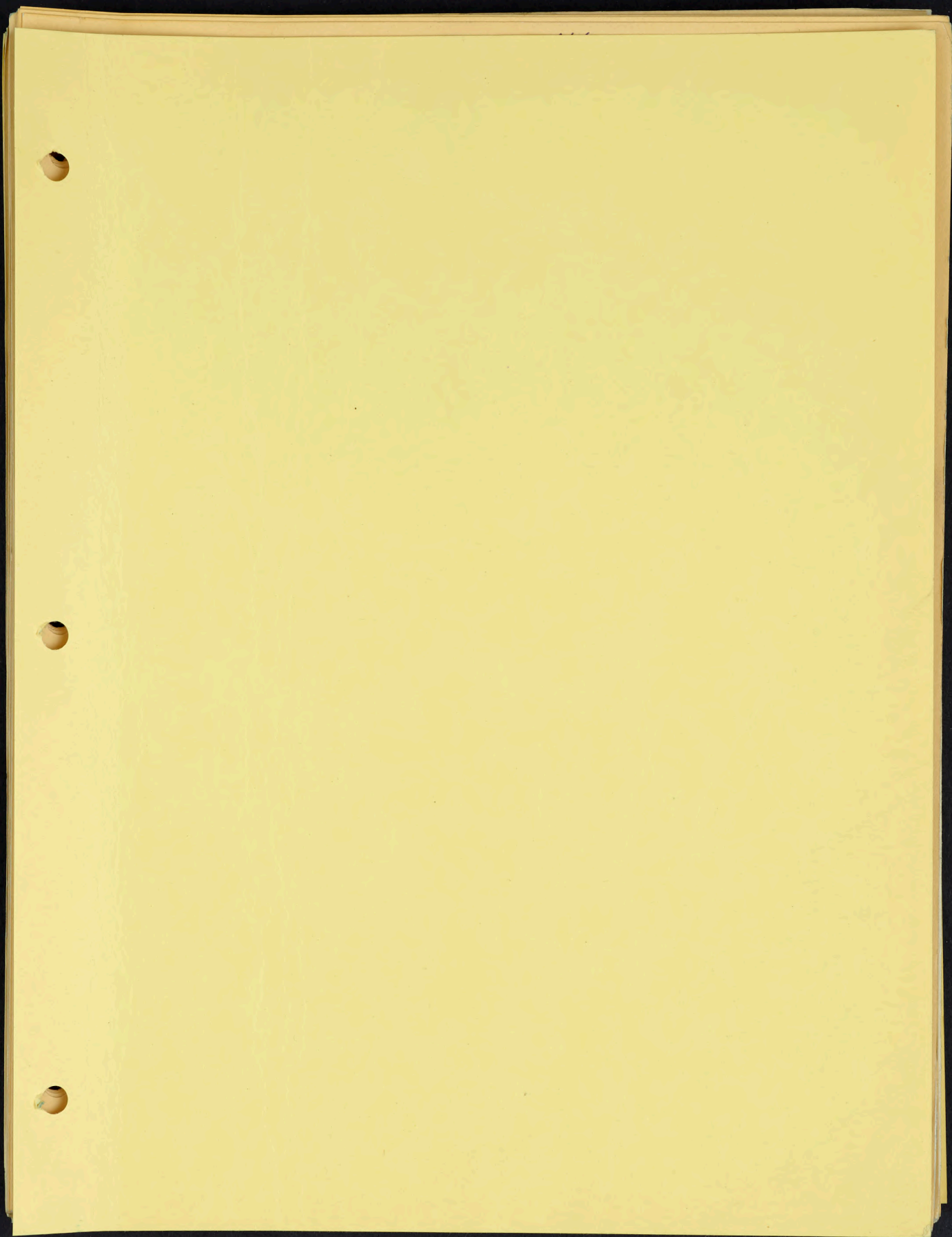
CHECKED BY

DATE

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SIDESLIP RANGE $-10^\circ < \beta < -2^\circ$

SIDESLIP RANGE $-2^\circ < \beta < 2^\circ$

$a_1(N)$

.05

.04

.03

.02

.01

0

C-105

C.A.L. WIND TUNNEL TESTS

$a_1(V)$ vs M

$\alpha = -2.1^\circ$

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.5

.6

.7

.8

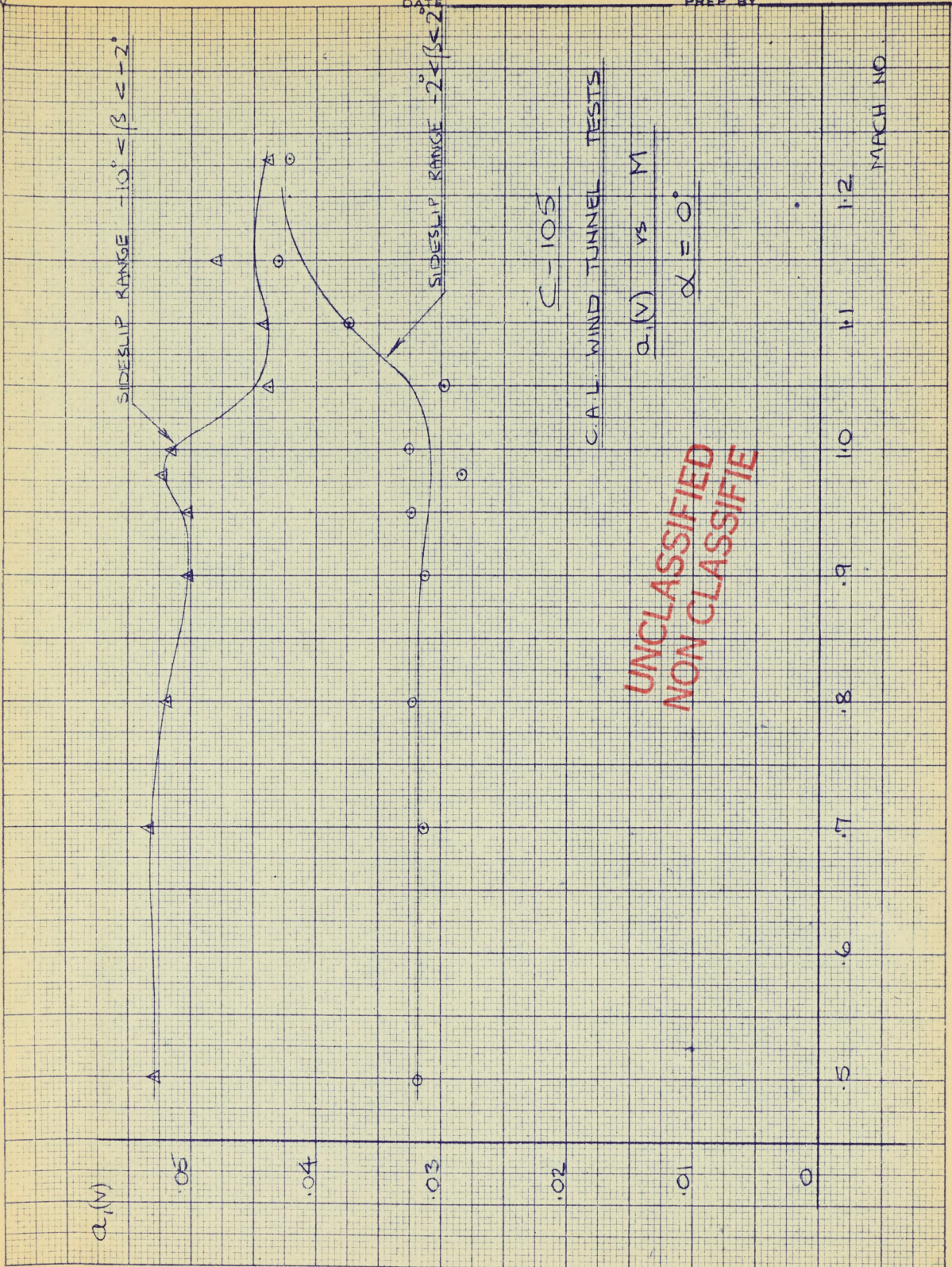
.9

1.0

1.1

1.2

MACH NO.



C-105

C.A.L. WIND TUNNEL TESTS

$\alpha(V)$ vs M

$\alpha = 0^\circ$

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NON CLASSIFIE

MARCH NO.

1.2

1.1

1.0

.9

.8

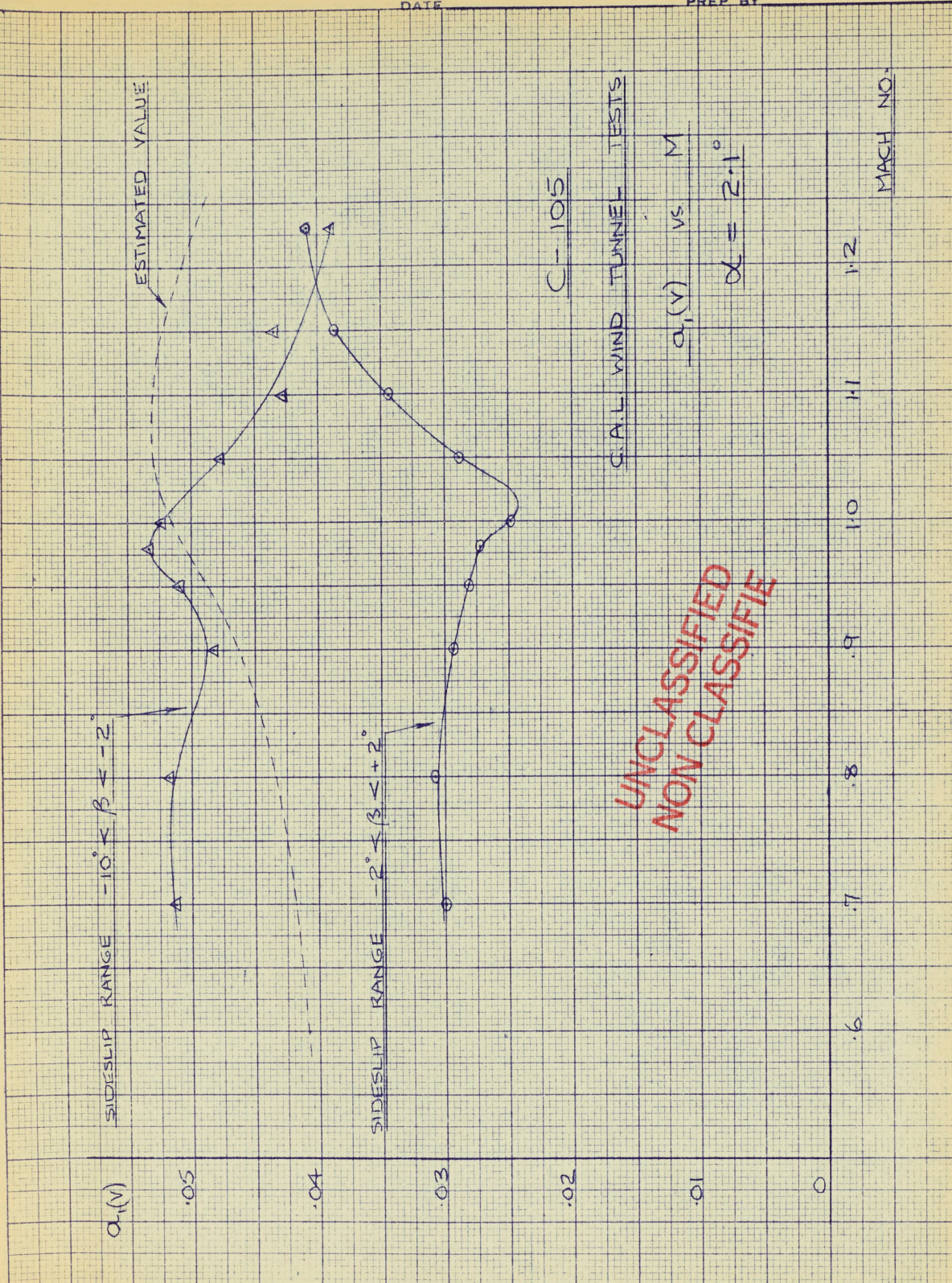
.7

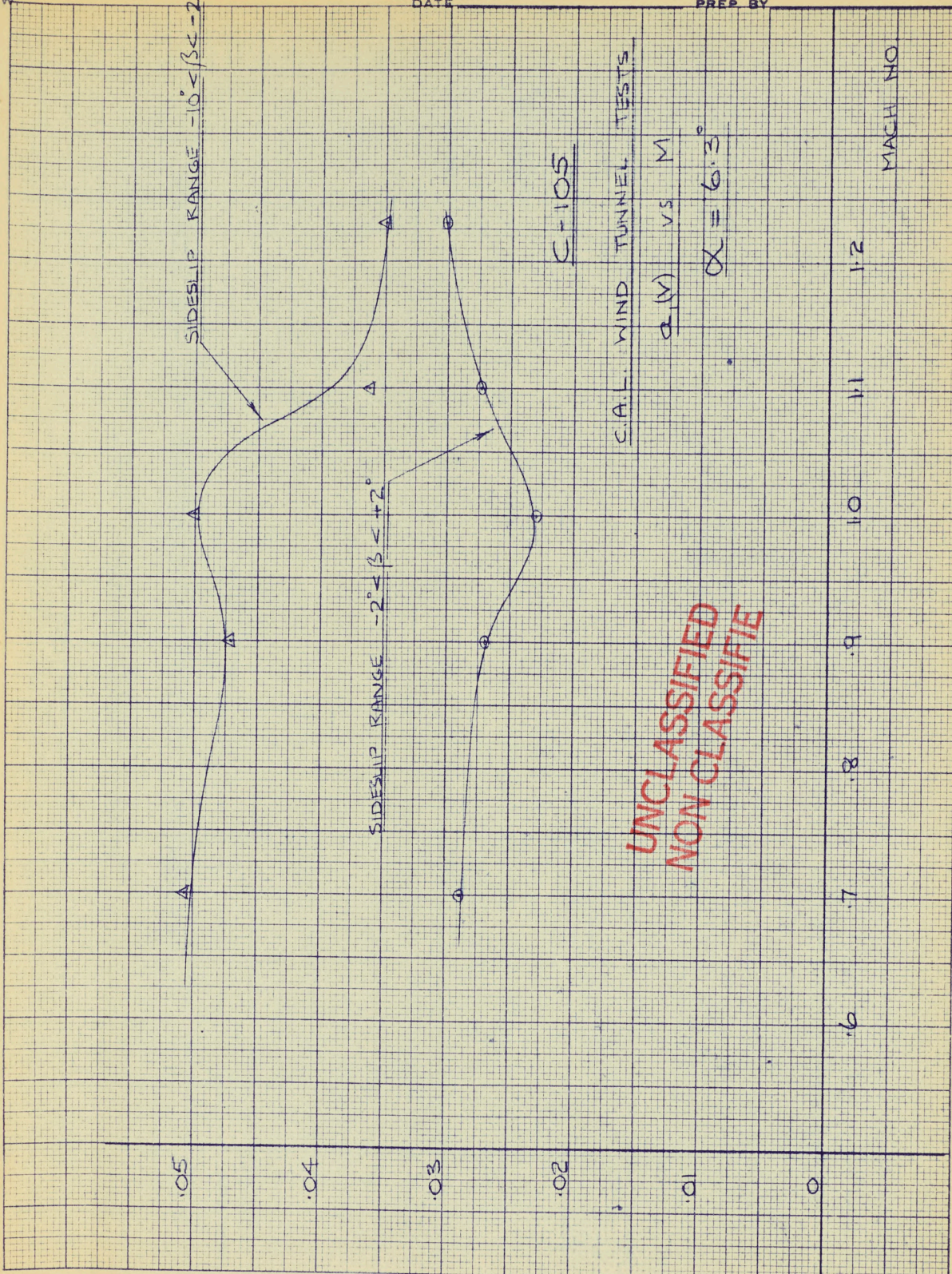
.6

.5

48912 - BUFFEL, E. E. & S. E. CO.
10 x 10 to the 12 inch grid lines ascended
MADE IN U.S.A.

FORM 10 - KODUFEEL & SLESER CO.
10 x 10 to the 1/2 inch. 5th time recommended
MADE IN U.S.A.





59-12 KEUFFEL & ESSER CO.
10 x 10 to the 12 inch 500 film standard
MADE IN U.S.A.

C-105

CAL. WIND TUNNEL TESTS

CHORDWISE CENTRE OF PRESSURE ~ FIN & RUDDER

$\alpha = -2$

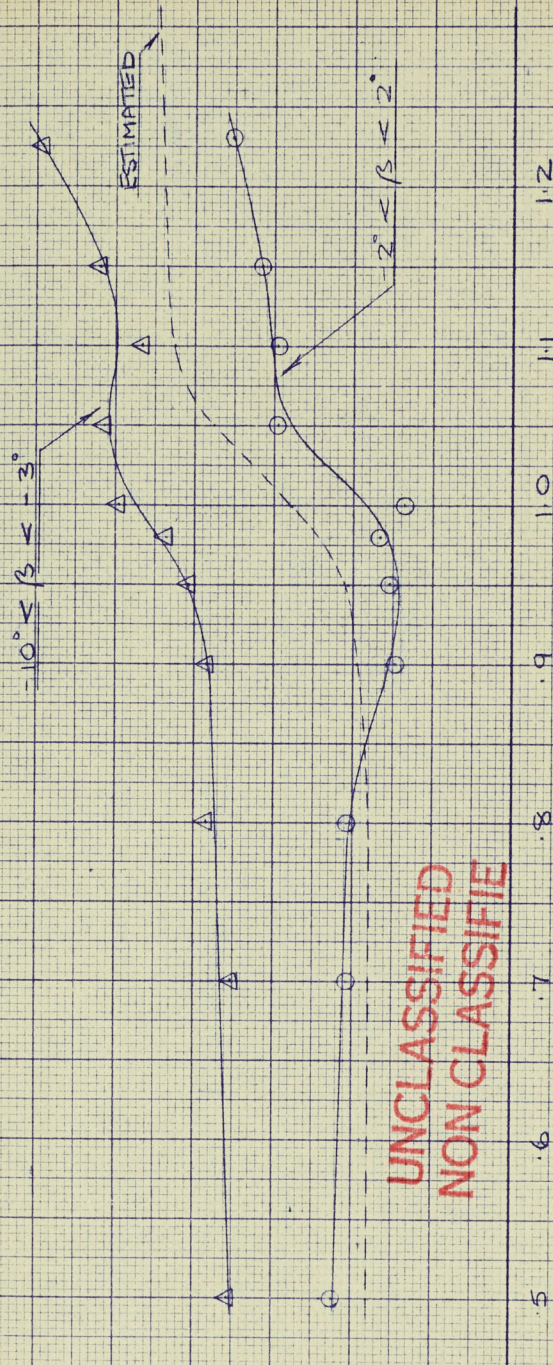
C. OF P.
(FRACTION
M.A.C.)

.6

.5

.4

.3



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M

C-105

CAL WIND TUNNEL TESTS

CHORDWISE CENTRE OF PRESSURE ~ FIN & RUDDER

$\alpha = 0^\circ$

C. of P
(FRACTION
M.A.C.)

.6

.5

.4

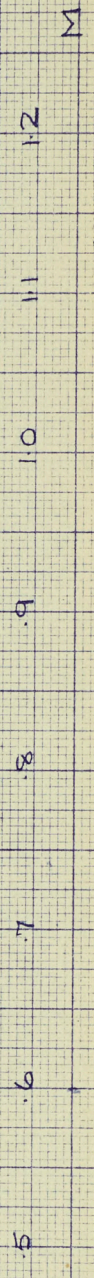
.3

$-10^\circ < \beta < -3^\circ$

ESTIMATED

$-2^\circ < \beta < 2^\circ$

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$C = 105$

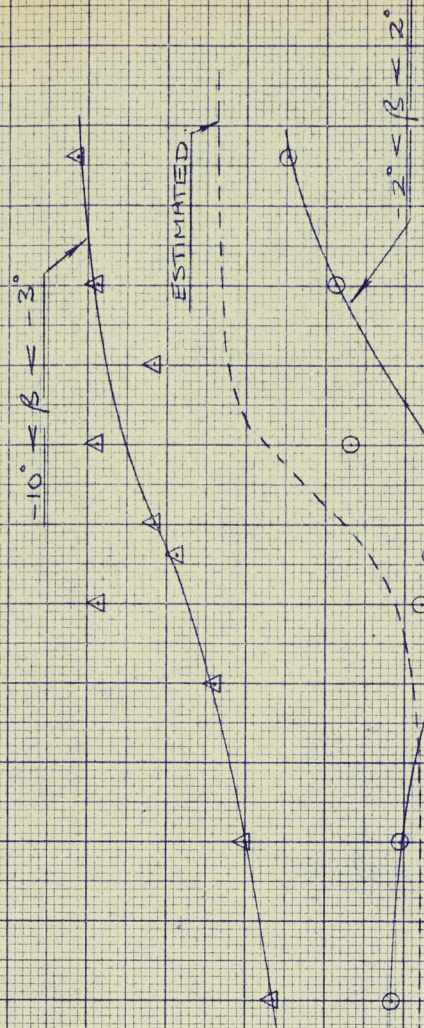
C.A.L. WIND TUNNEL TESTS

CHORDWISE CENTRE OF PRESSURE ~ FIN & RUDDER

$\alpha = 2^\circ$

C. OF P.
 (FRACTION
 M.P.C.)

.6
 .5
 .4
 .3



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.5 .6 .7 .8 .9 1.0 1.1 1.2 M

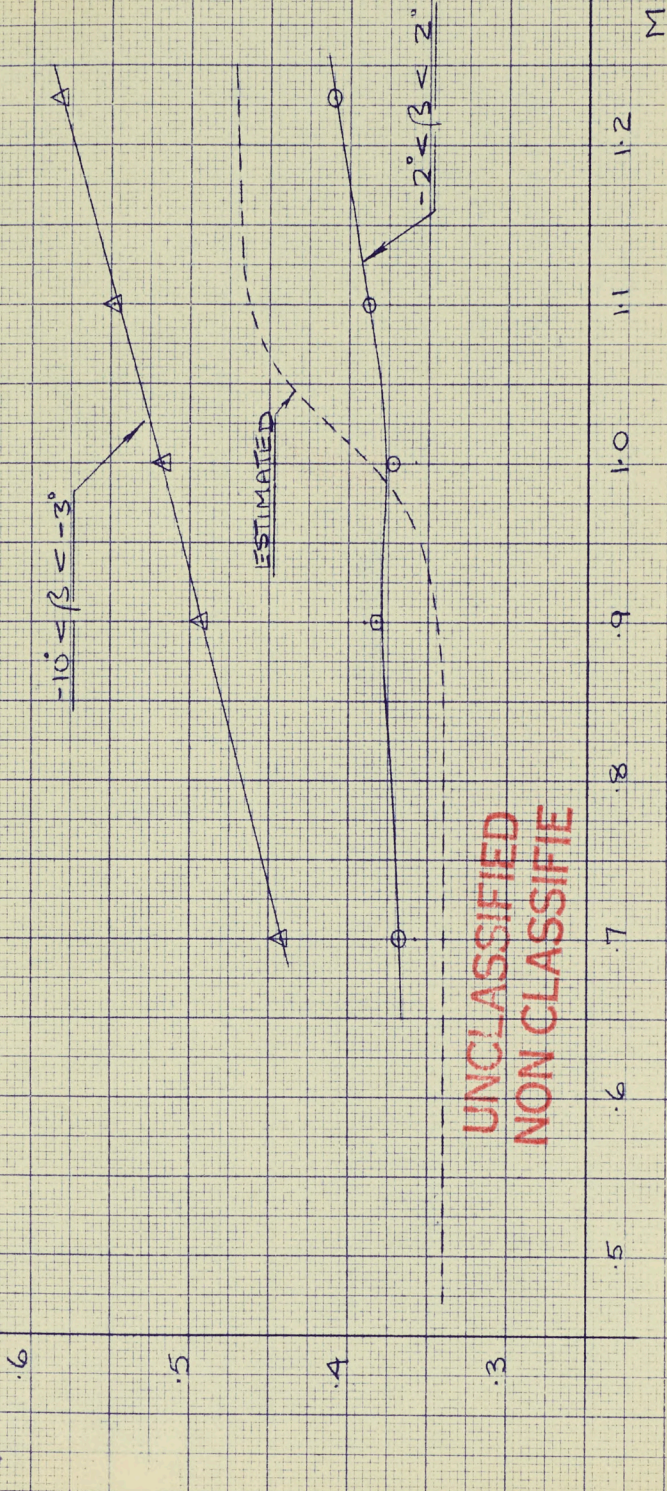
C-105

C.A.L. WIND TUNNEL TESTS

CHORDWISE CENTRE OF PRESSURE ~ FIN & RUDDER

$\alpha = 6^\circ$

C. OF P.
(FRACTION
M.A.C.)



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C-105

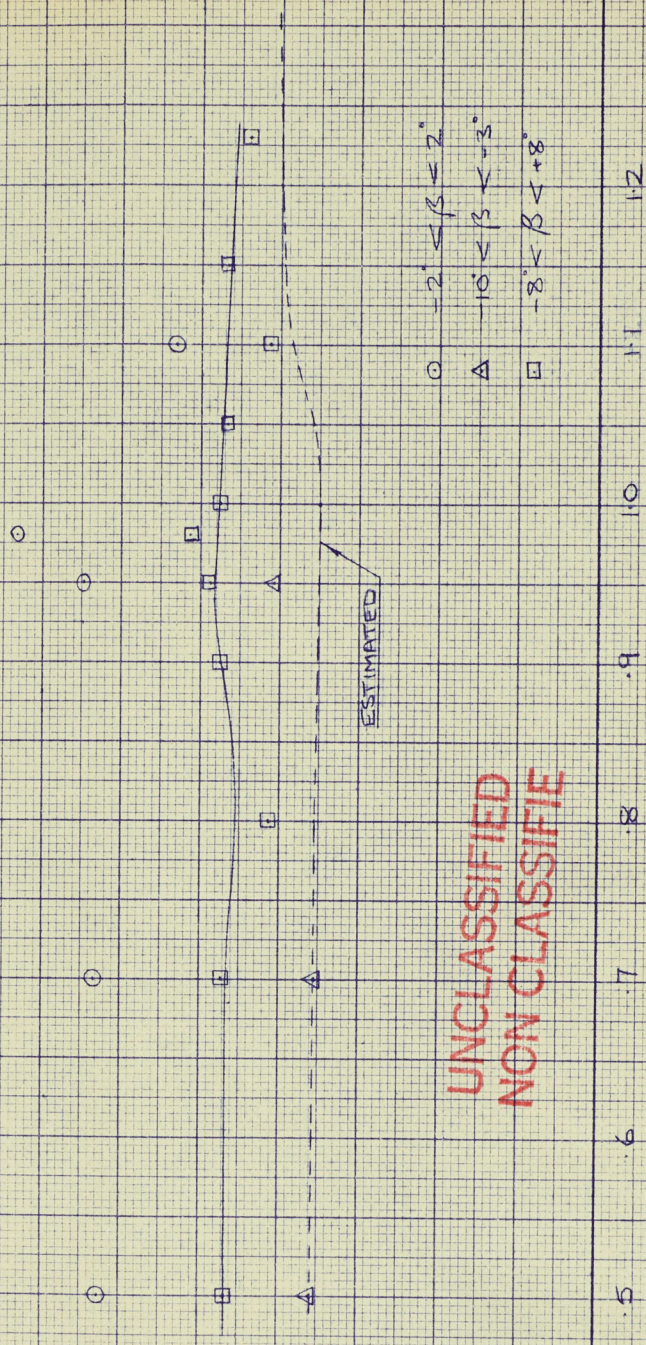
C. A. L. WIND TUNNEL TESTS.

SPANWISE CENTRE OF PRESSURE ~ FIN & RUDDER

$\alpha = -2^\circ$

η (C.P.)
(FRACTION OF SPAN) .6

UNCLASSIFIED
NON CLASSIFIE



$\circ -2^\circ < \beta < 2^\circ$
 $\Delta -10^\circ < \beta < -3^\circ$
 $\square -8^\circ < \beta < +8^\circ$

M.

58912 KAUTER & ESSER CO
10 x 10 to the 12 inch 5th lines account
MADE IN U.S.A.

C-105

CIA WIND TUNNEL TESTS

SPANWISE CENTRE OF PRESSURE ~ HN & RUDDER

$\alpha = 0^\circ$

η_{CIP}

(FRACTION OF SPAN) .6

0

.5

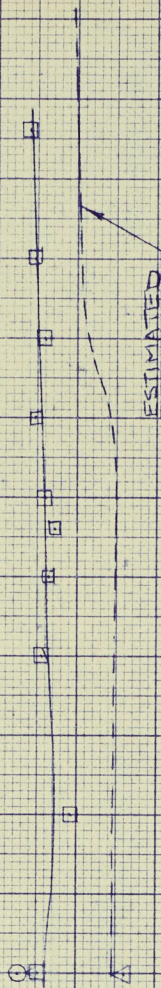
0

□

△

.4

.3



ESTIMATED

- $-2^\circ < \beta < +2^\circ$
- △ $-10^\circ < \beta < -3^\circ$
- $-8^\circ < \beta < +8^\circ$

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NON CLASSIFIE

12

11

10

.9

.8

.7

.6

.5

M

C-105

C.A.L. WIND TUNNEL TESTS

SPANWISE CENTRE OF PRESSURE ~ FIN & RUDDER

$\alpha = 2^\circ$

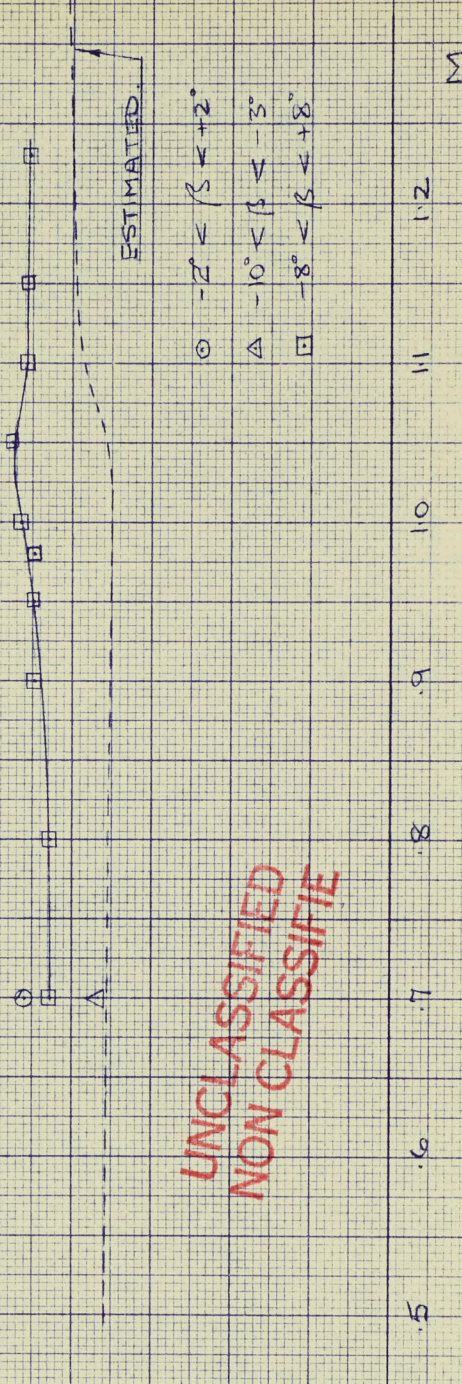
η_{cp}
(FRACTION
OF
SPAN)

.6

.5

.4

.3



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NON CLASSIFIE

.5 .6 .7 .8 .9 1.0 1.1 1.2 M

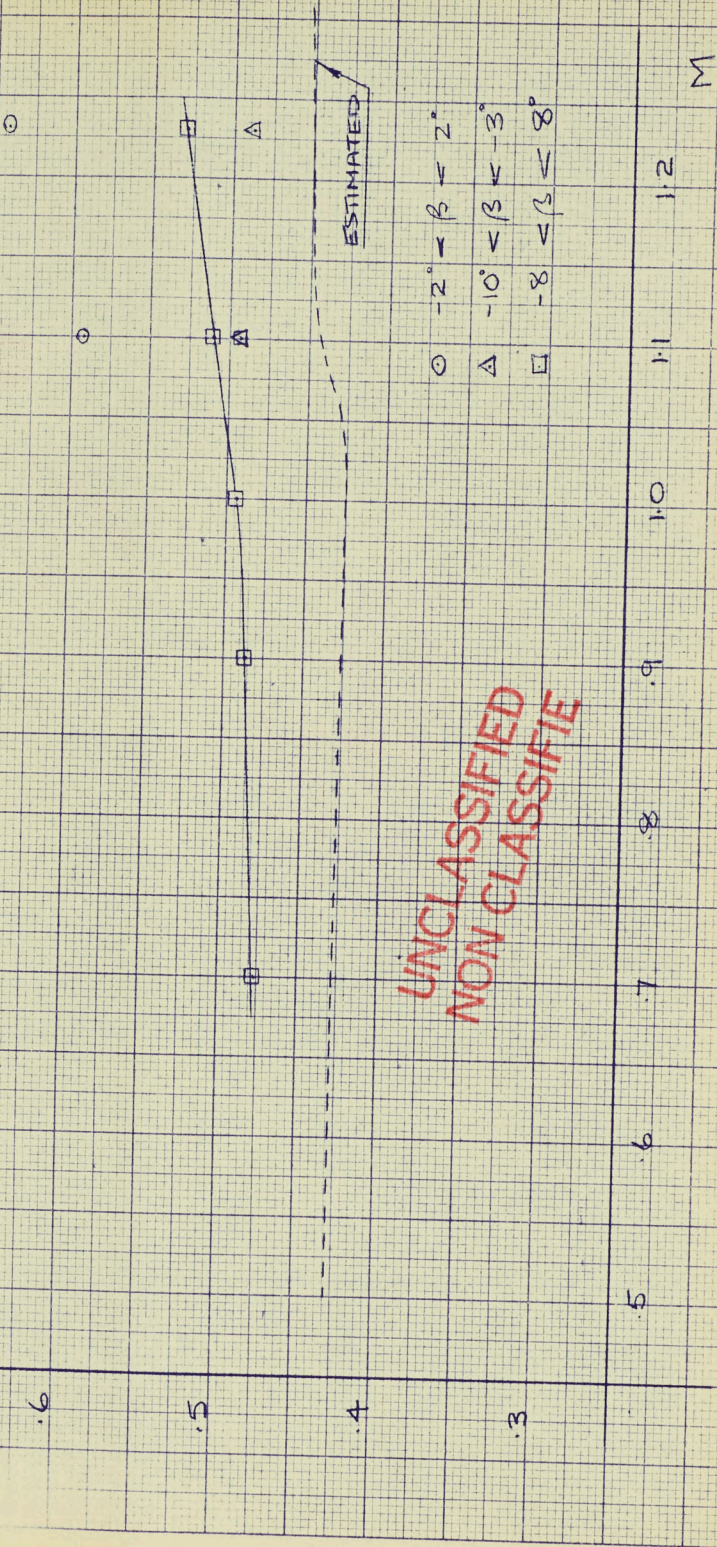
C-105

S.A.L. WIND TUNNEL TESTS

SPANWISE CENTRE OF PRESSURE ~ FIN & RUDDER

$\alpha = 6^\circ$

η
(cp.
(FRACTION
OF
SPAN).



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NON CLASSIFIE

$\circ - 2^\circ < \beta < 2^\circ$
 $\Delta - 10^\circ < \beta < -3^\circ$
 $\square - 8^\circ < \beta < 8^\circ$

ESTIMATED

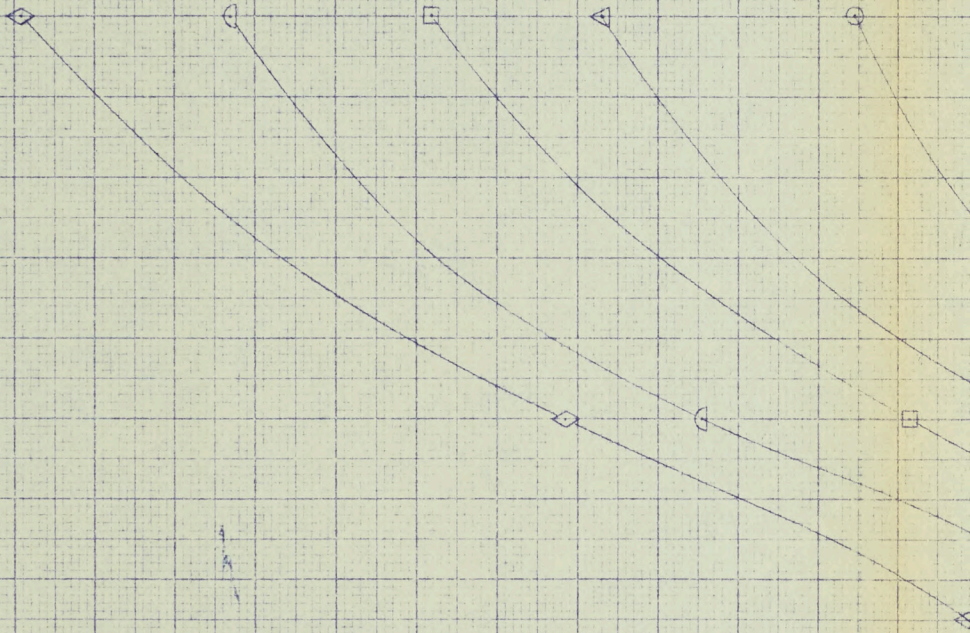
C-105

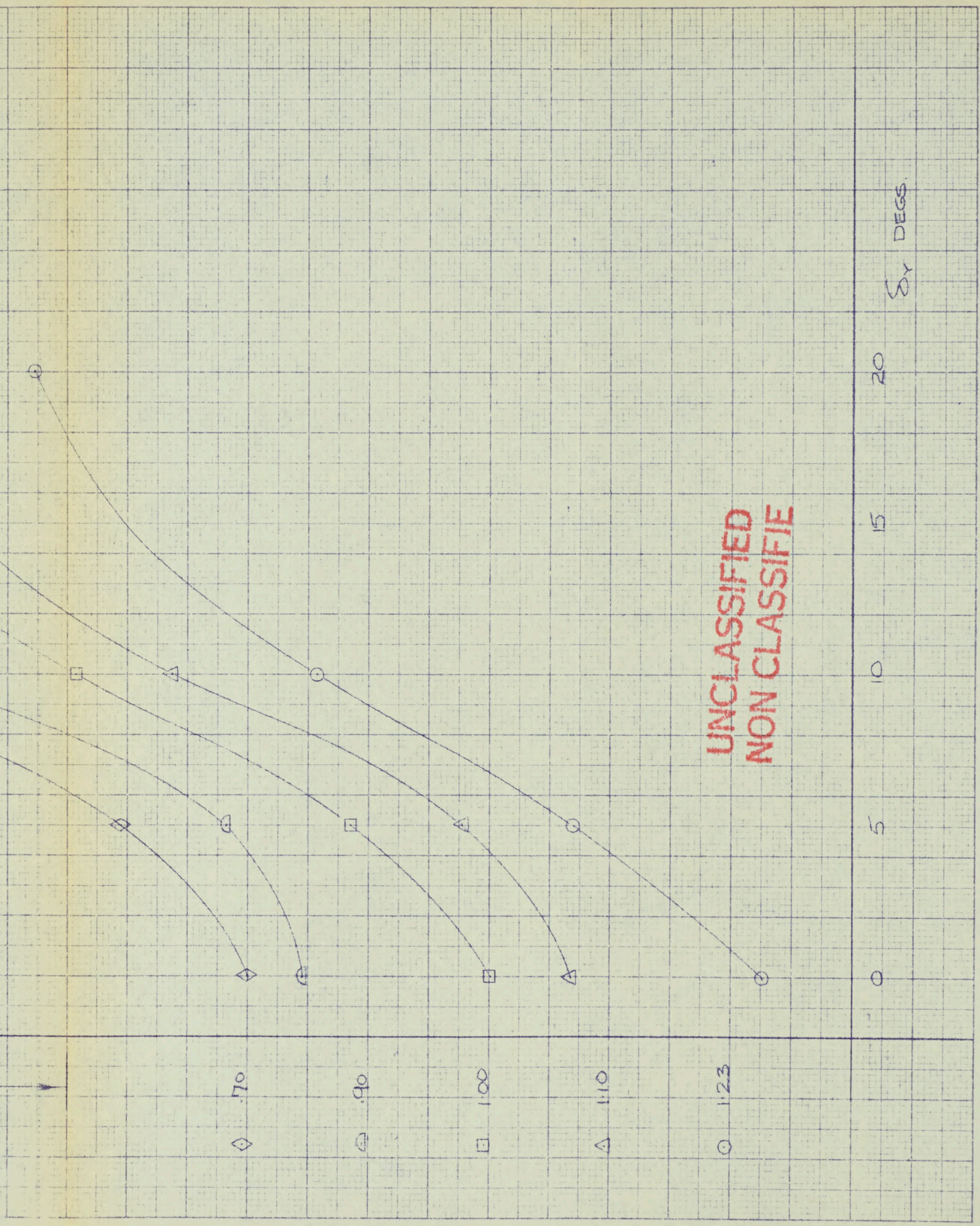
C_{Nf} vs δr

$\alpha = -2^\circ$ $\psi = 0^\circ$

C_{Nf}

SCALE OF
 C_{Nf} .10
(ORIGIN AT
M)





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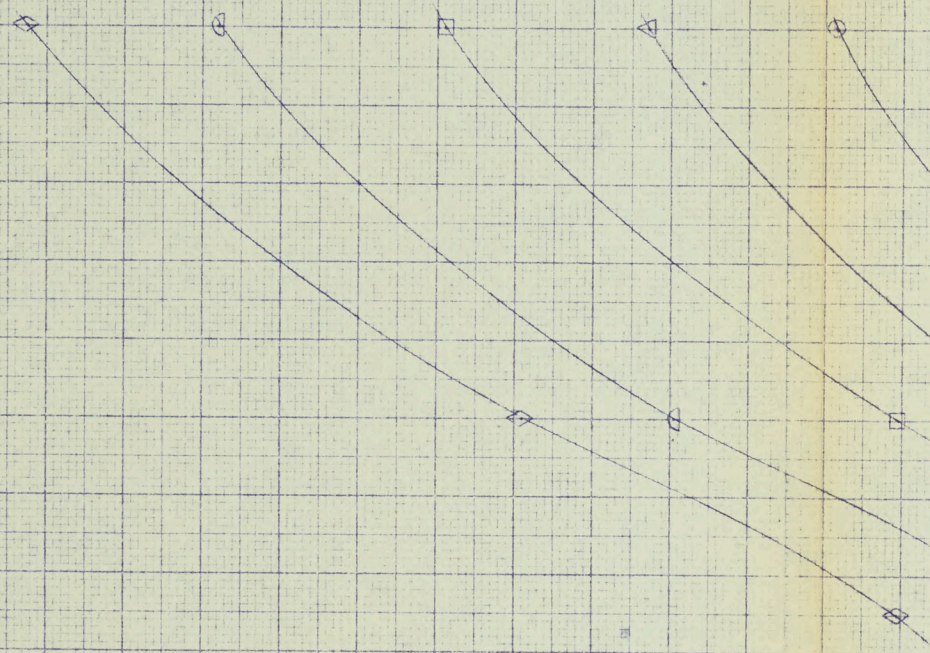
C-105

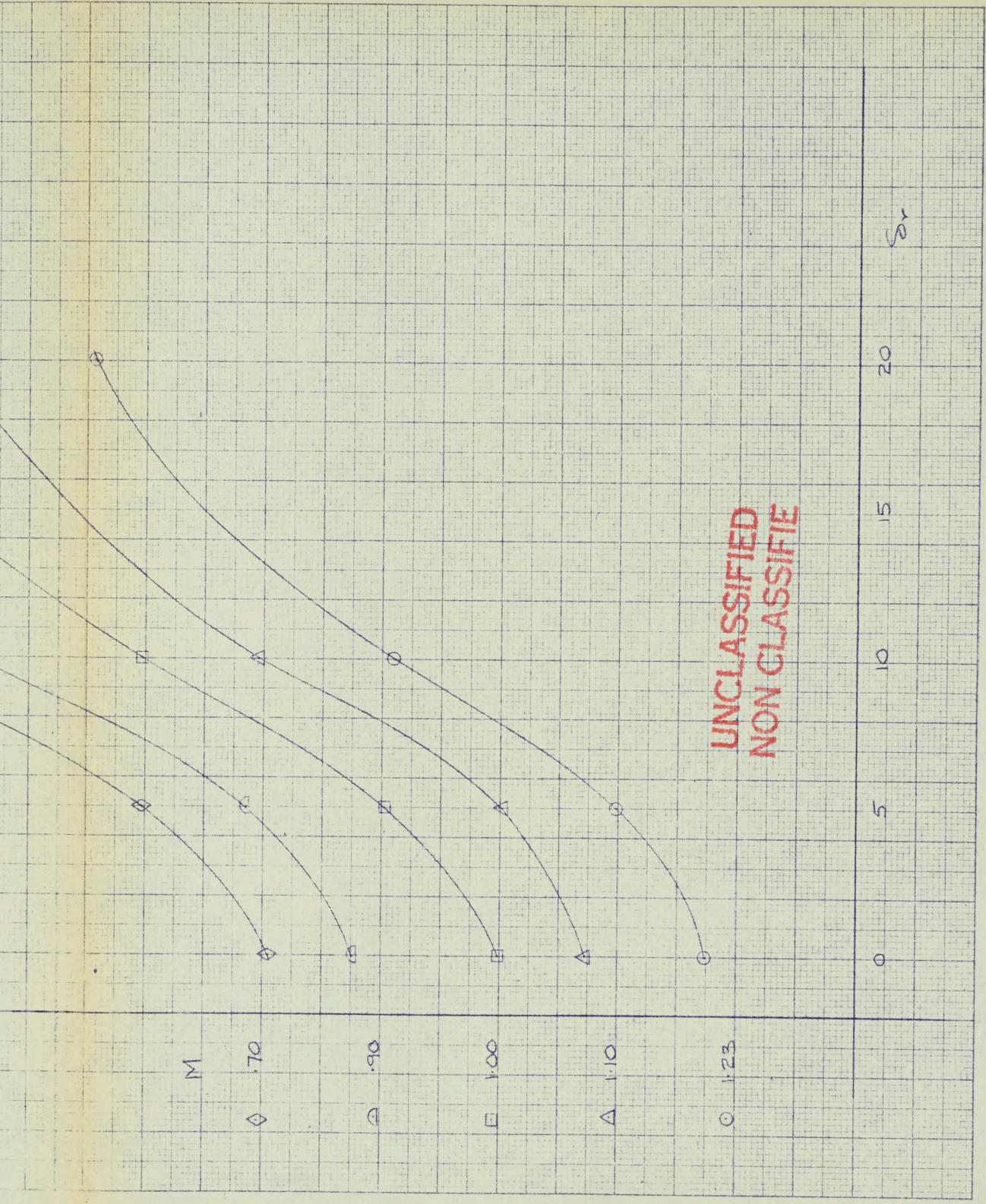
C_{NF} vs S_r

$\alpha = 0^\circ$ $\psi = 0^\circ$

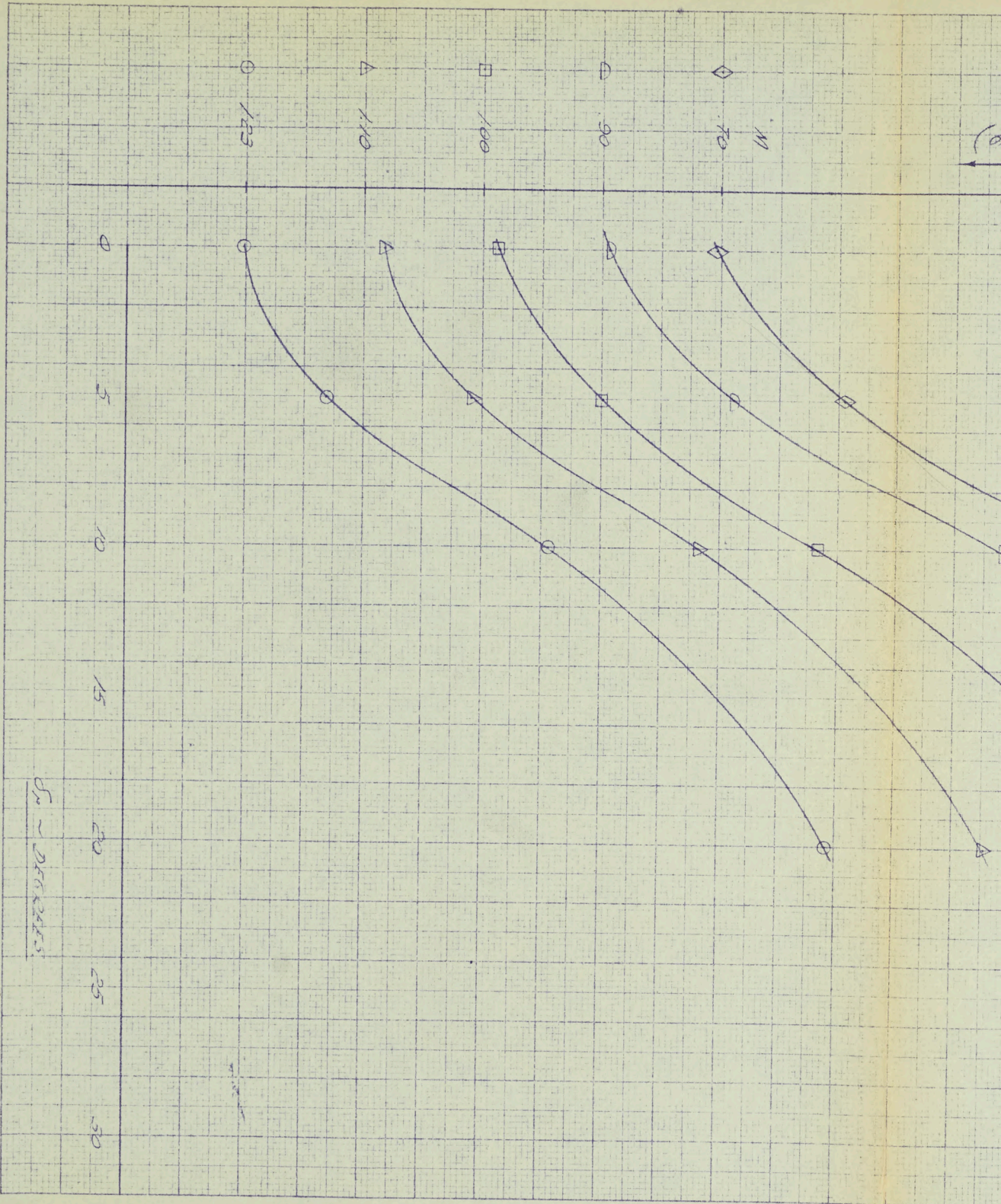
C_{NF}

SCALE OF
 C_{NF} .10
(ORIGIN AT
M)





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NON CLASSIFIE



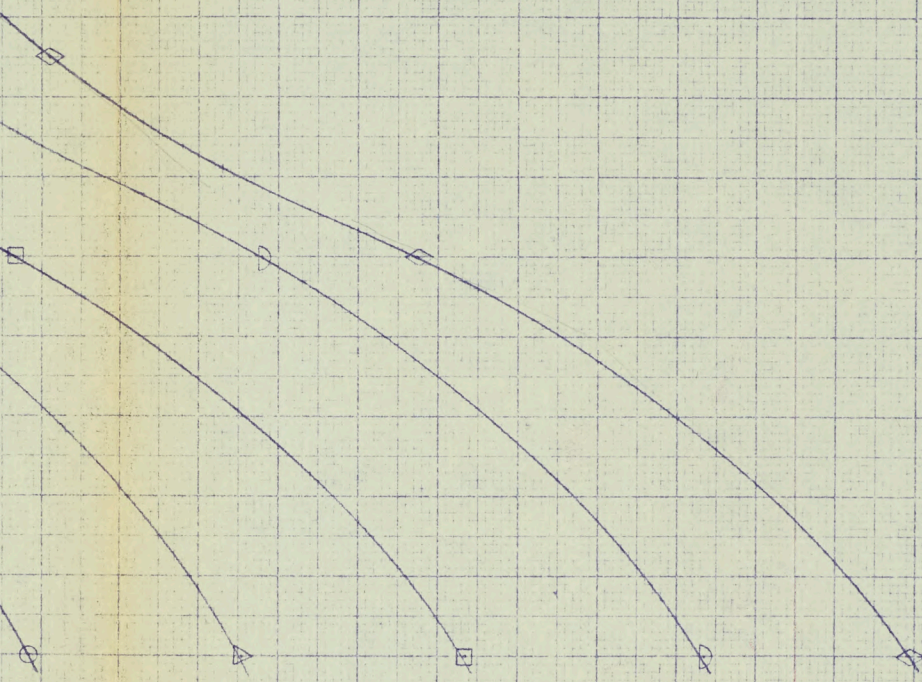
Sum - 25000000

1.4.3.
MAY 54.

P/N.T./20
CLARK.

(ORIGIN @ MATH NO.)
10.

21



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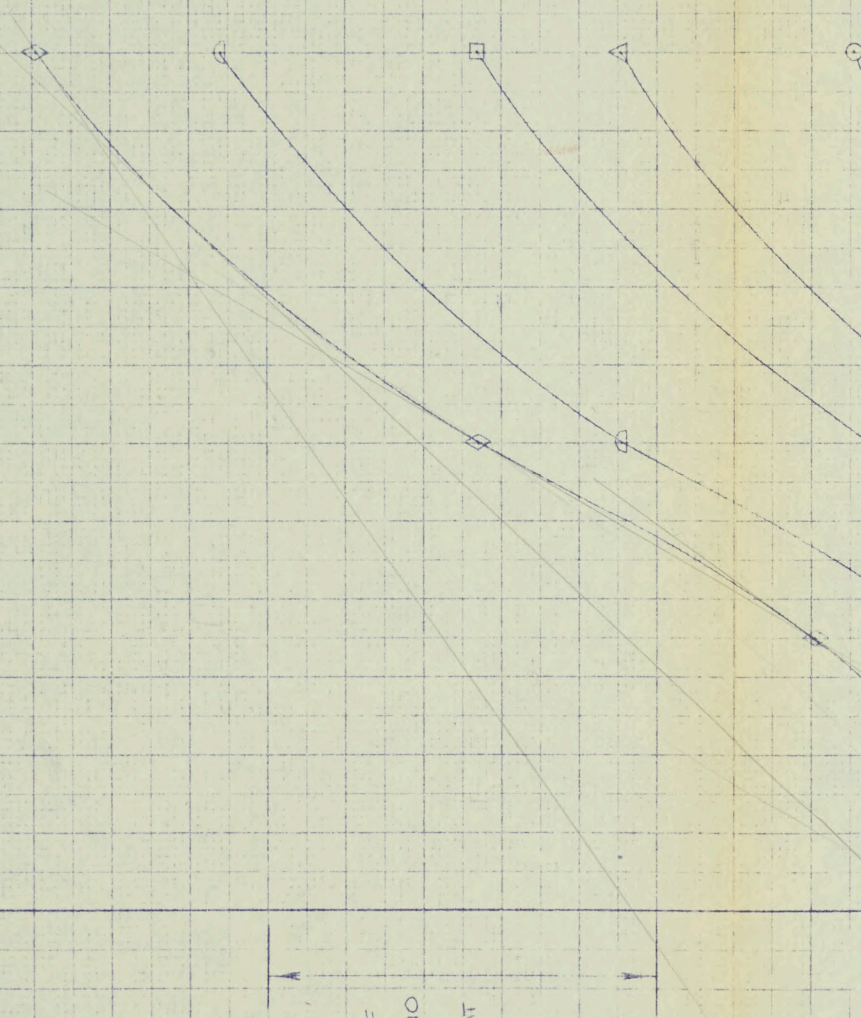
21.05
21.15 58
21.20 21.00

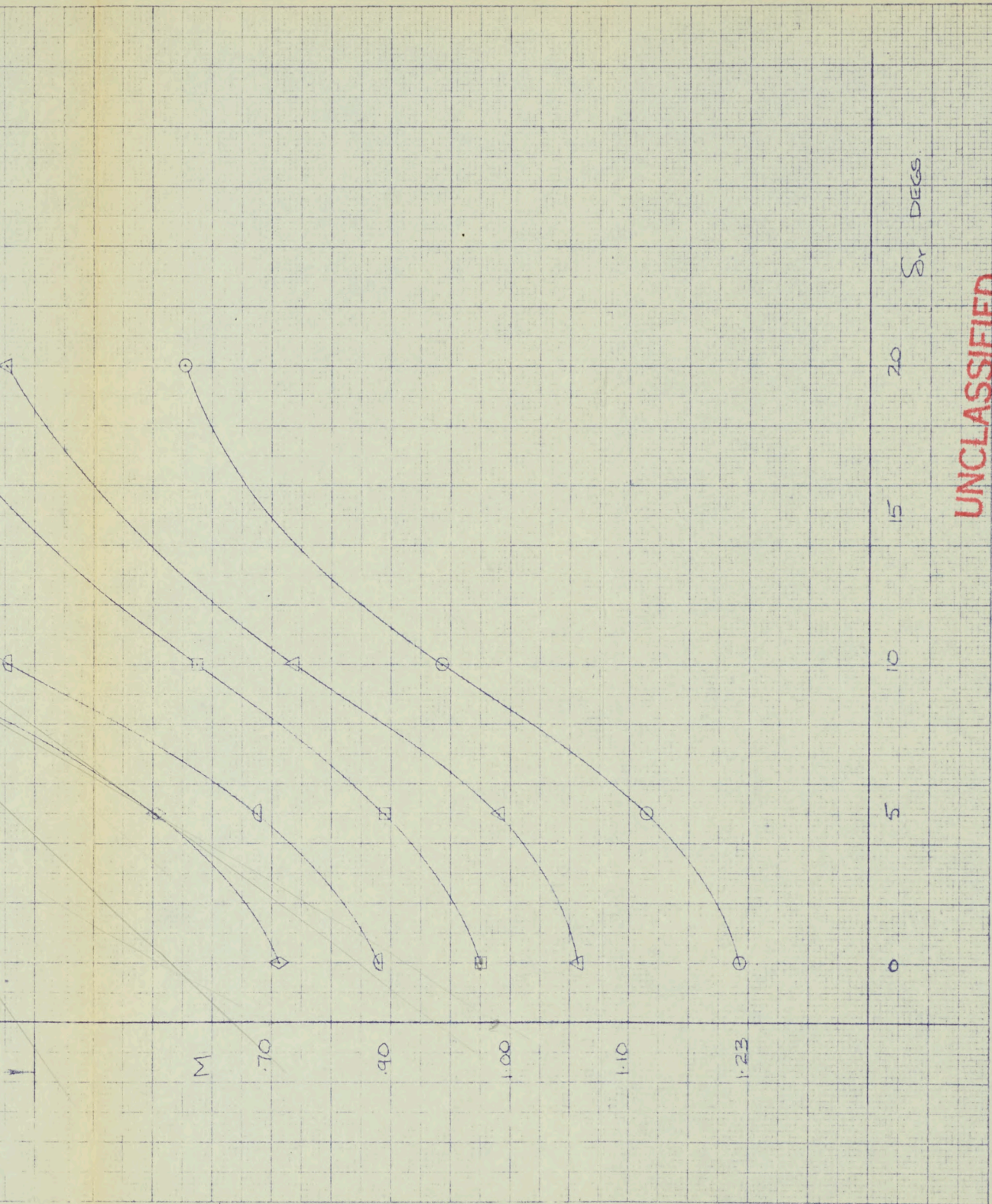
C-105

$C_M = 1.0$ vs δ
 $\alpha = 6^\circ$ $\psi = 0^\circ$

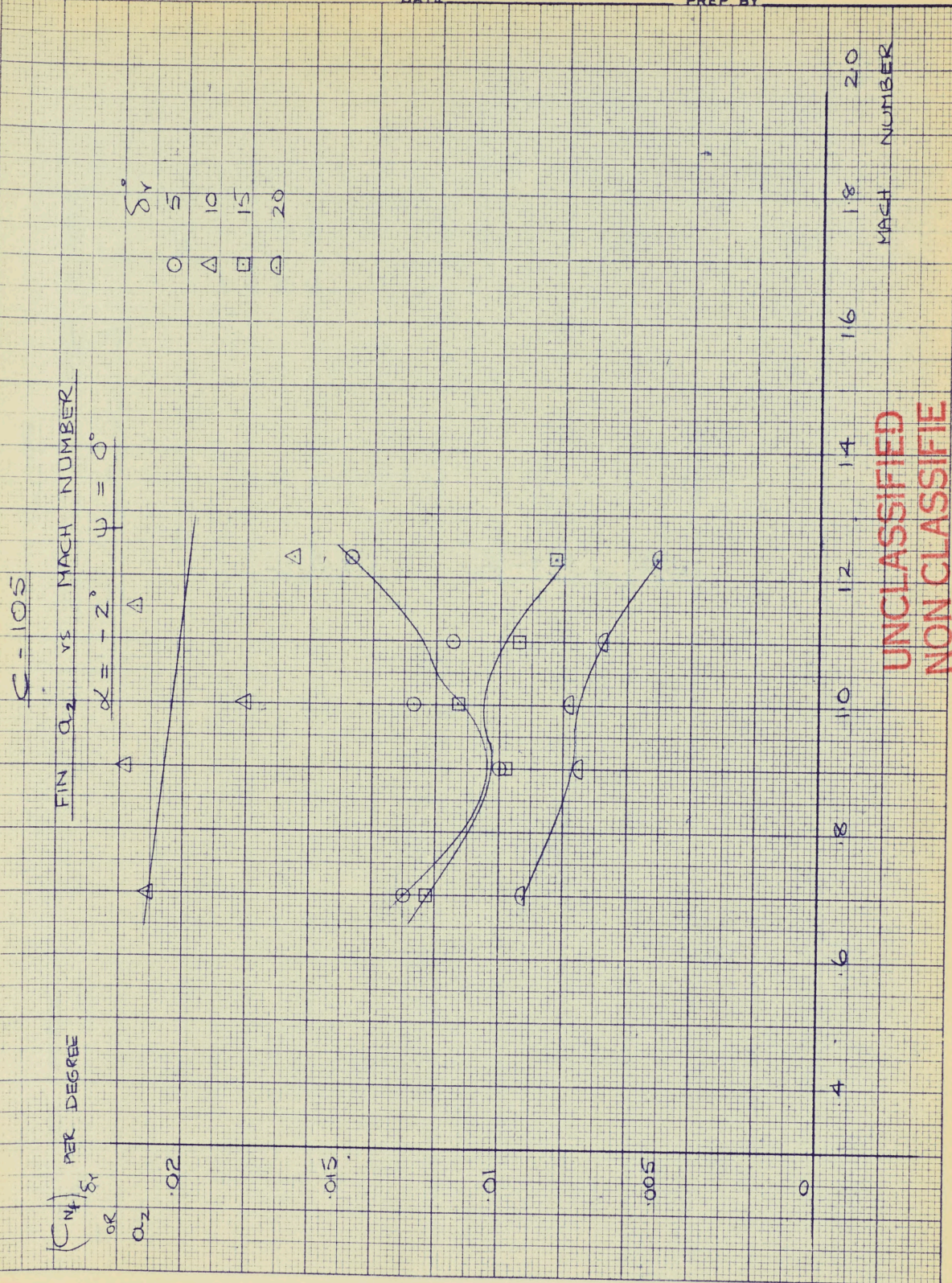
C_M

SCALE OF
 $C_M = .10$
(ORIGIN AT
M)





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15-412 - REVISED 9-55-60
 10 - 10 TO REV. 2, 1961; SEE FIGS ASSUMED
 MADE IN U.S.A.

C-105
FIN α_2 vs MACH NUMBER

$\alpha = 0^\circ$ $\gamma = 0^\circ$

- α_2
 \circ 5°
 Δ 10°
 \square 15°
 \square 20°

PER DEGREE

$(C_{M+})_{\alpha_2}$

α_2

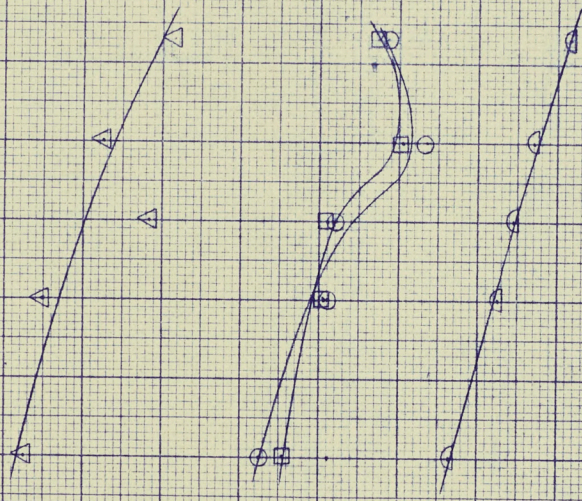
.02

.015

.01

.005

0



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313 KEUFER, LESSER CO.
107 10th St. New York, N.Y.
MADE IN U.S.A.

C-105
FIN α_2 VS MACH NUMBER
 $\alpha = 2^\circ$ $\psi = 0^\circ$

Δ \circ \square \square
5° 10° 15° 20°

(C_{Mx}) PER DEGREE

α_2

.020

.015

.010

.005

.0

.4

.6

.8

1.0

1.2

1.4

1.6

1.8

2.0

MACH NUMBER

UNCLASSIFIED
NON CLASSIFIED

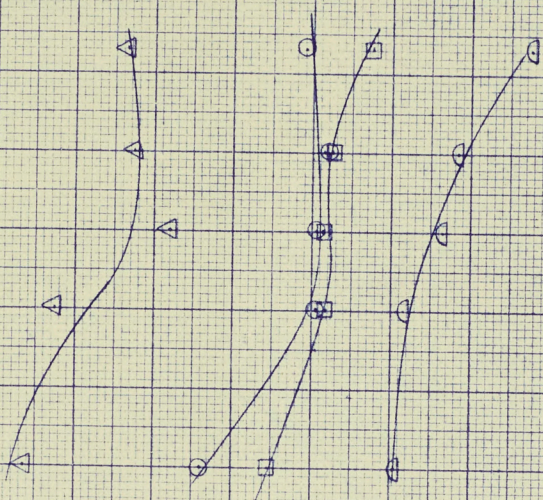
489-12 KEUFFEL & ESSER CO.
10 x 10 to the 13 inch 50 lines accurate
MADE IN U.S.A.

C-105
FIN Q_2 VS MACH NUMBER
 $\alpha = 6^\circ$
 $\gamma = 0^\circ$

Sr.
6°
10°
15°
20°

○ △ □ ◇

$(C_{mf})_{\delta}$ PER DEGREE
OR
 Q_2 .020



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MACH NUMBER

16

14

12

10

8

6

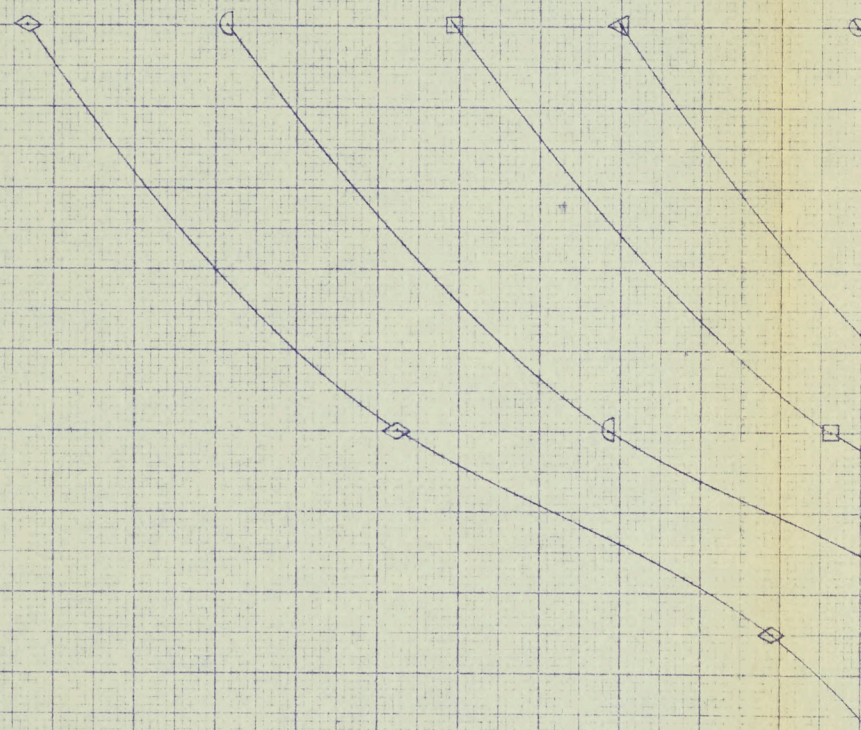
4

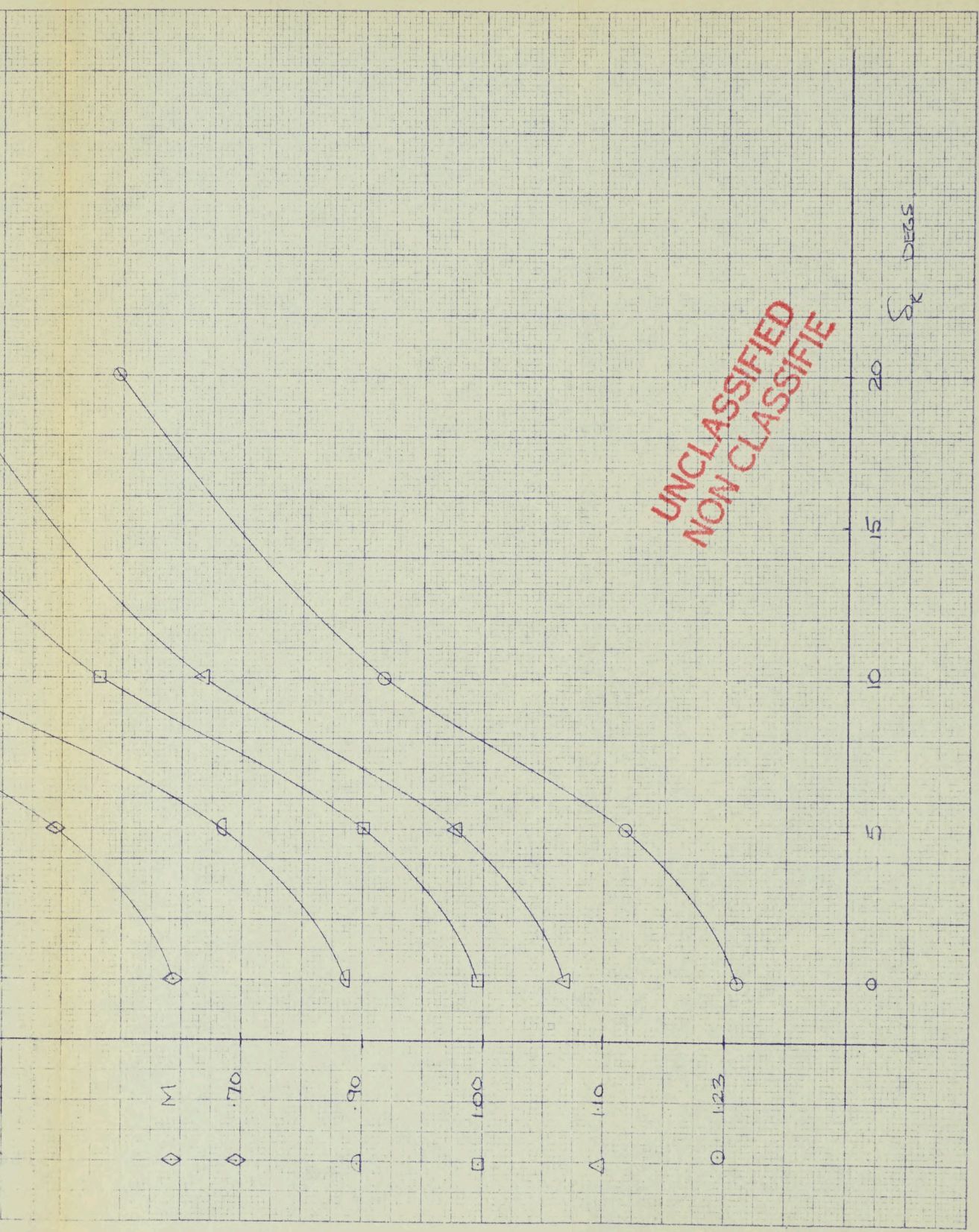
0

C-105
 C_{MFR} vs δY
 $\alpha = -2^\circ$ $\psi = 0^\circ$

C_{MFR}

SCALE OF
 $C_{MFR} \cdot 02$
(ORIGIN AT
M)





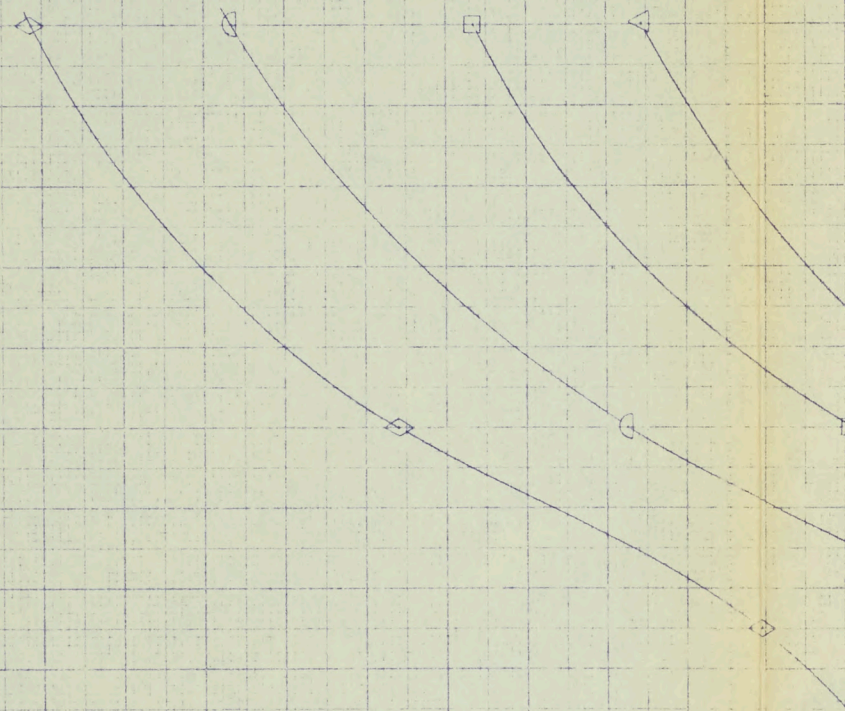
C-105

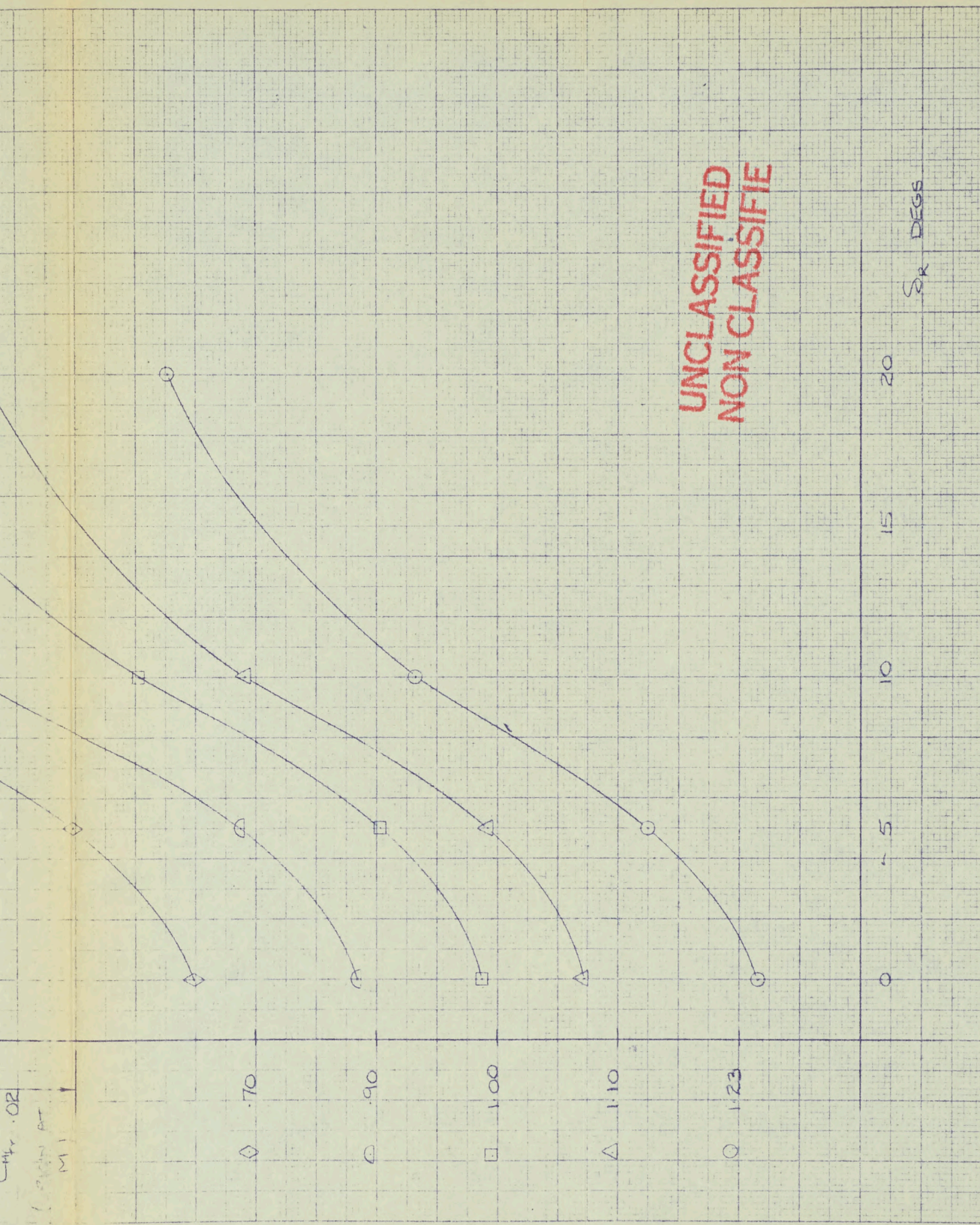
$C_{MFR} \text{ vs } S_R$

$\alpha = 0^\circ \quad \psi = 0^\circ$

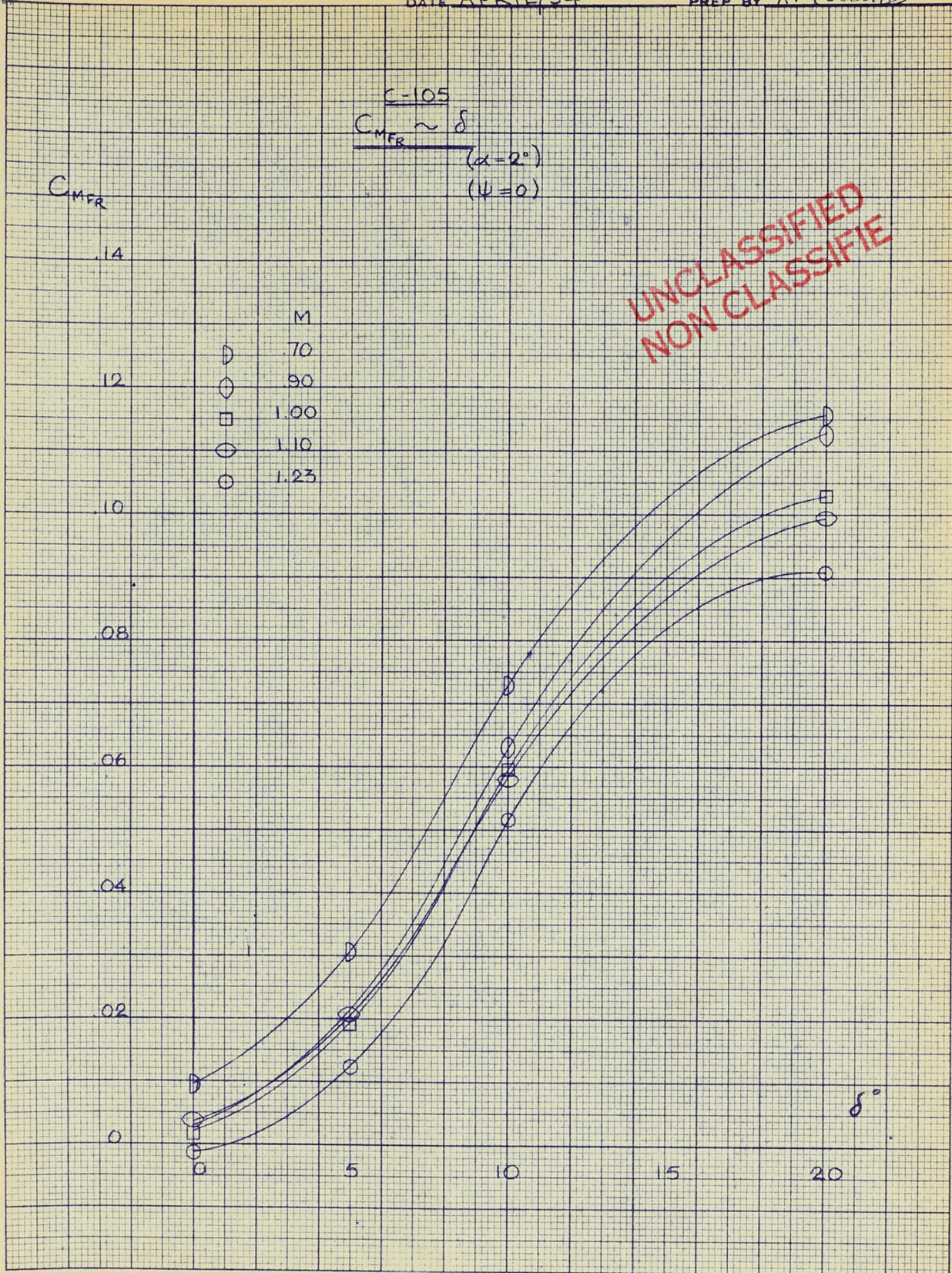
C_{MFR}

SCALE OF
 $C_{MFR} \cdot 0.2$
1 centimeter
= 1 M





$\frac{1}{M1} = .02$
 (0.02) at
 M1



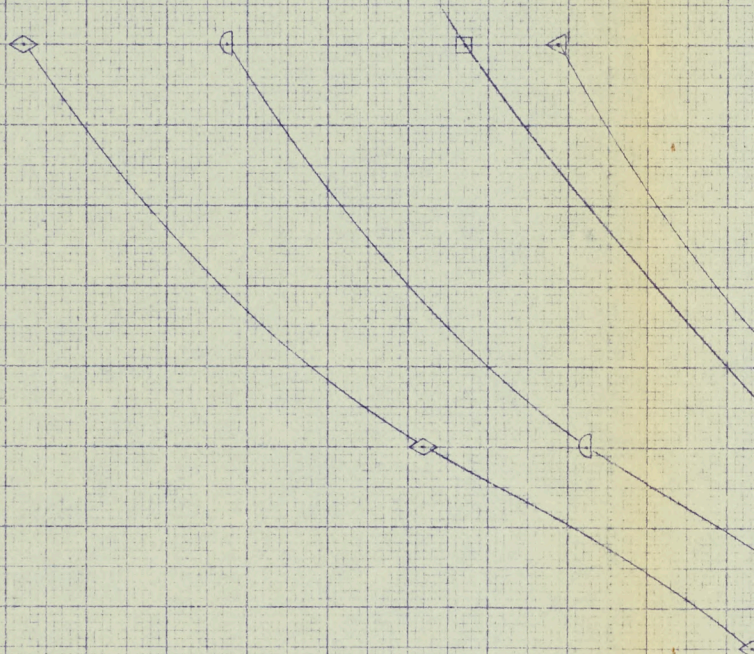
S = 105

C_{MFR} VS S_R

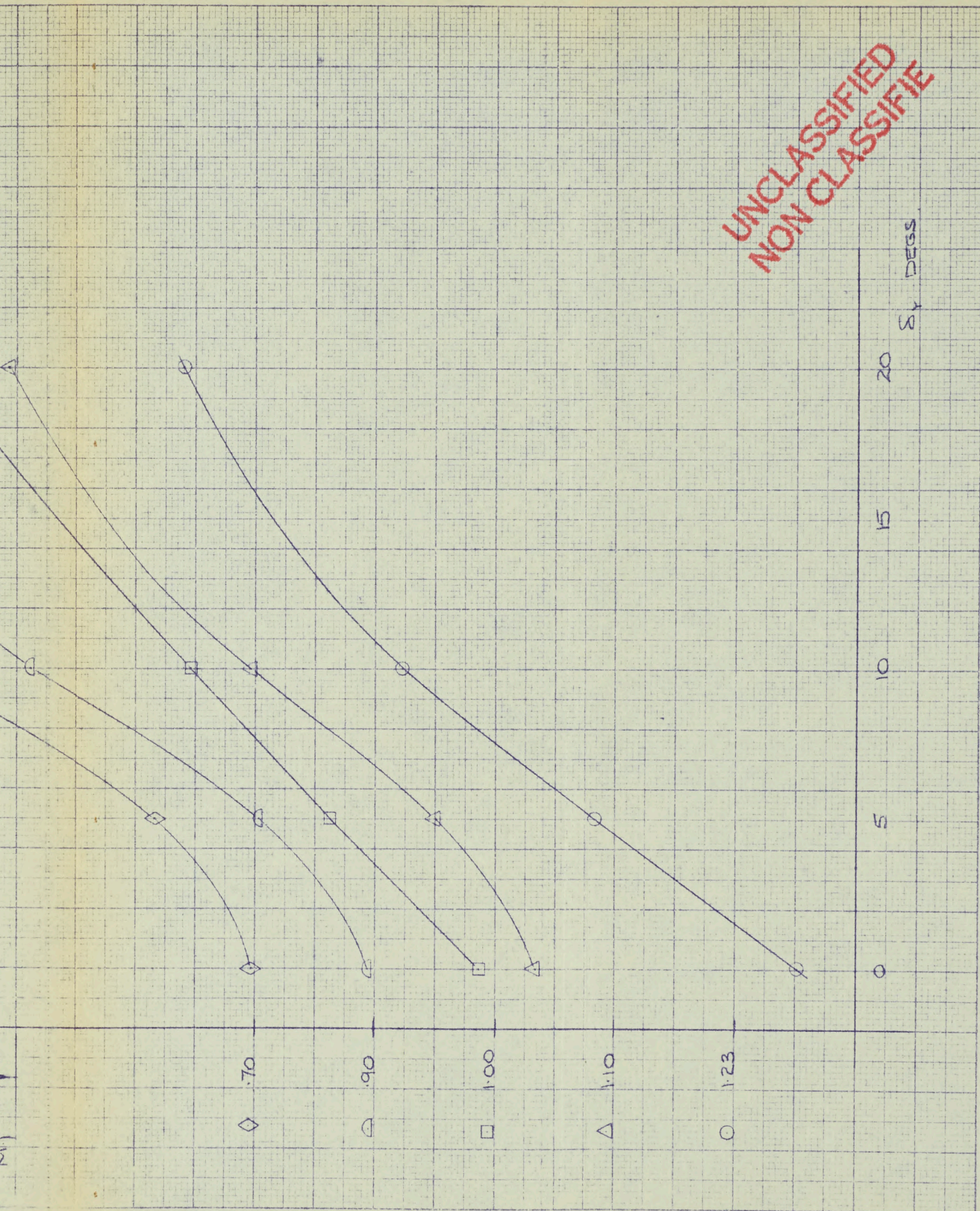
$\alpha = 6^\circ$ $\psi = 0^\circ$

C_{MFR}

SCALE OF
 C_{MFR} .02
(ORIGIN AT
M)



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C105
CHORDWISE CP POSITION

RUDDER LOAD

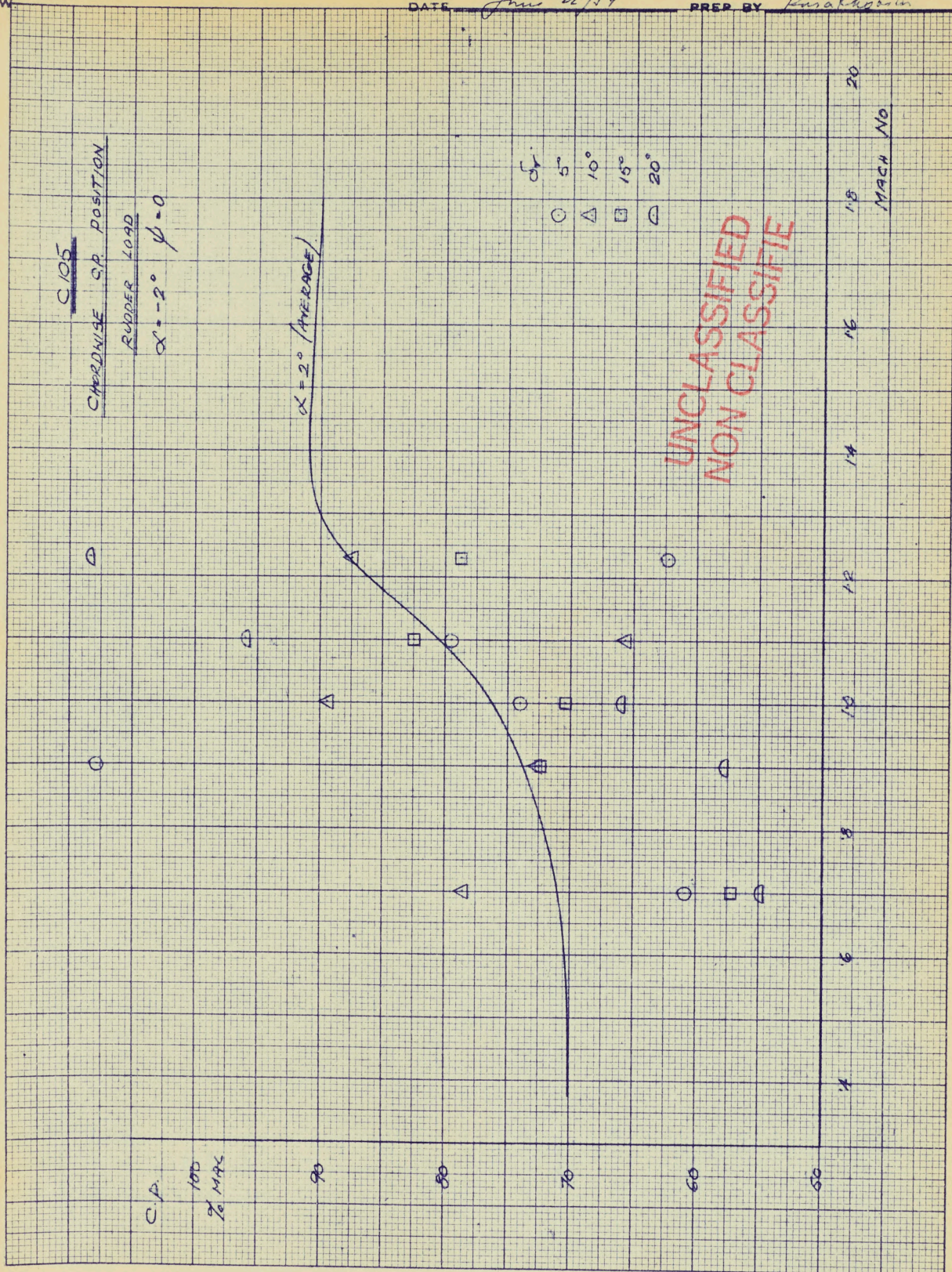
$\alpha = -2^\circ$ $\psi = 0$

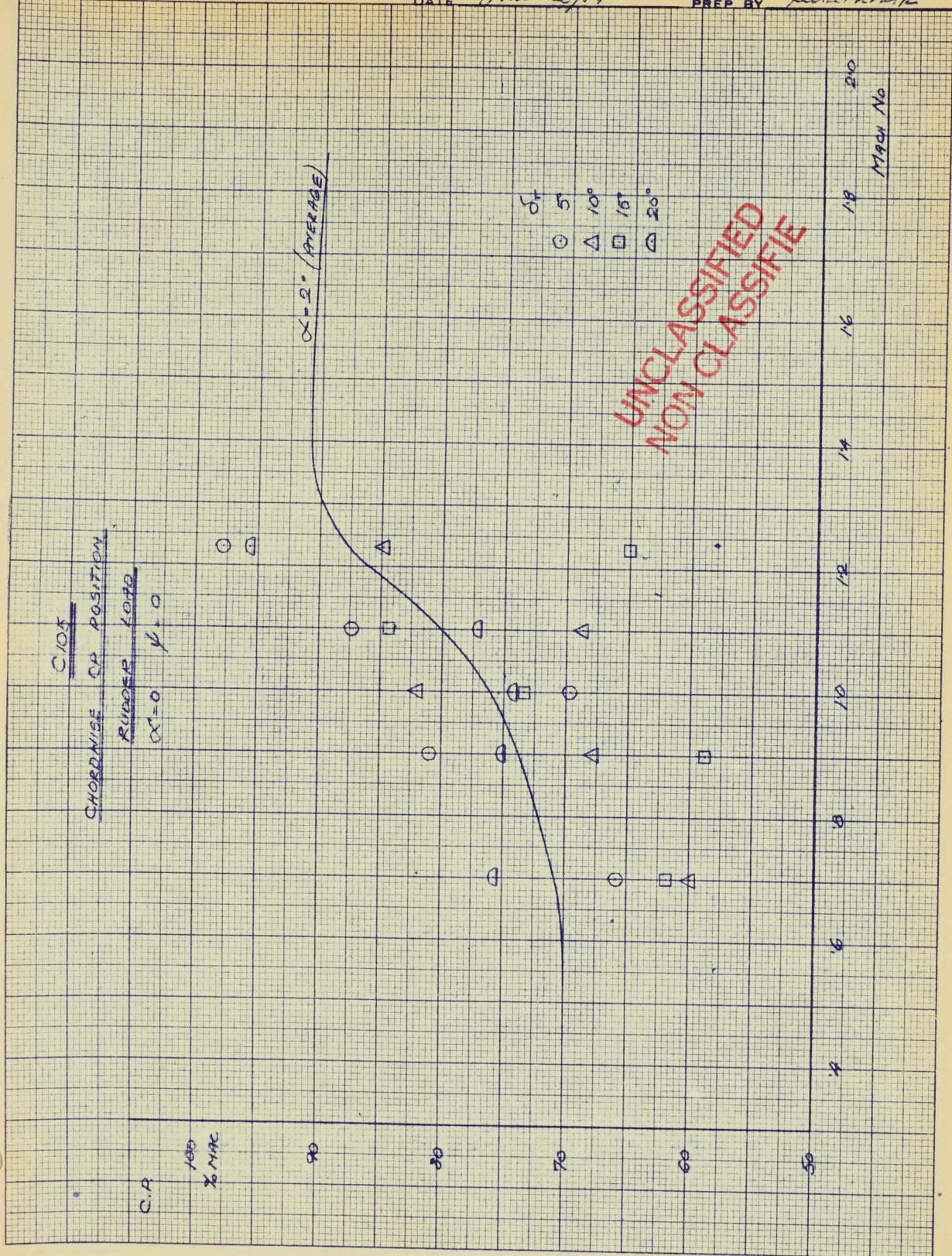
$\alpha = 2^\circ$ (AVERAGE)

α :
5° 10°
15° 20°

○ △ □ ◐

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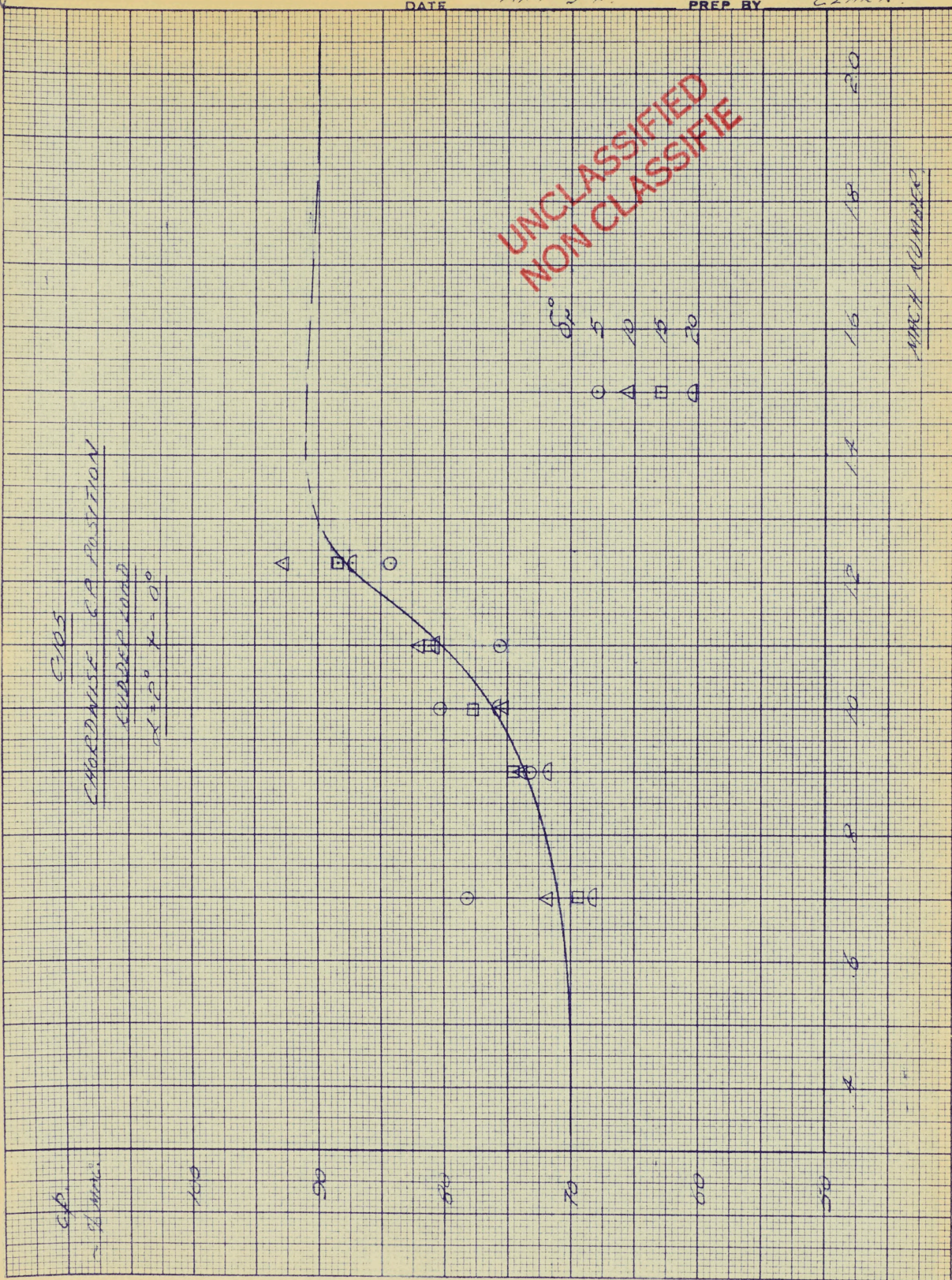




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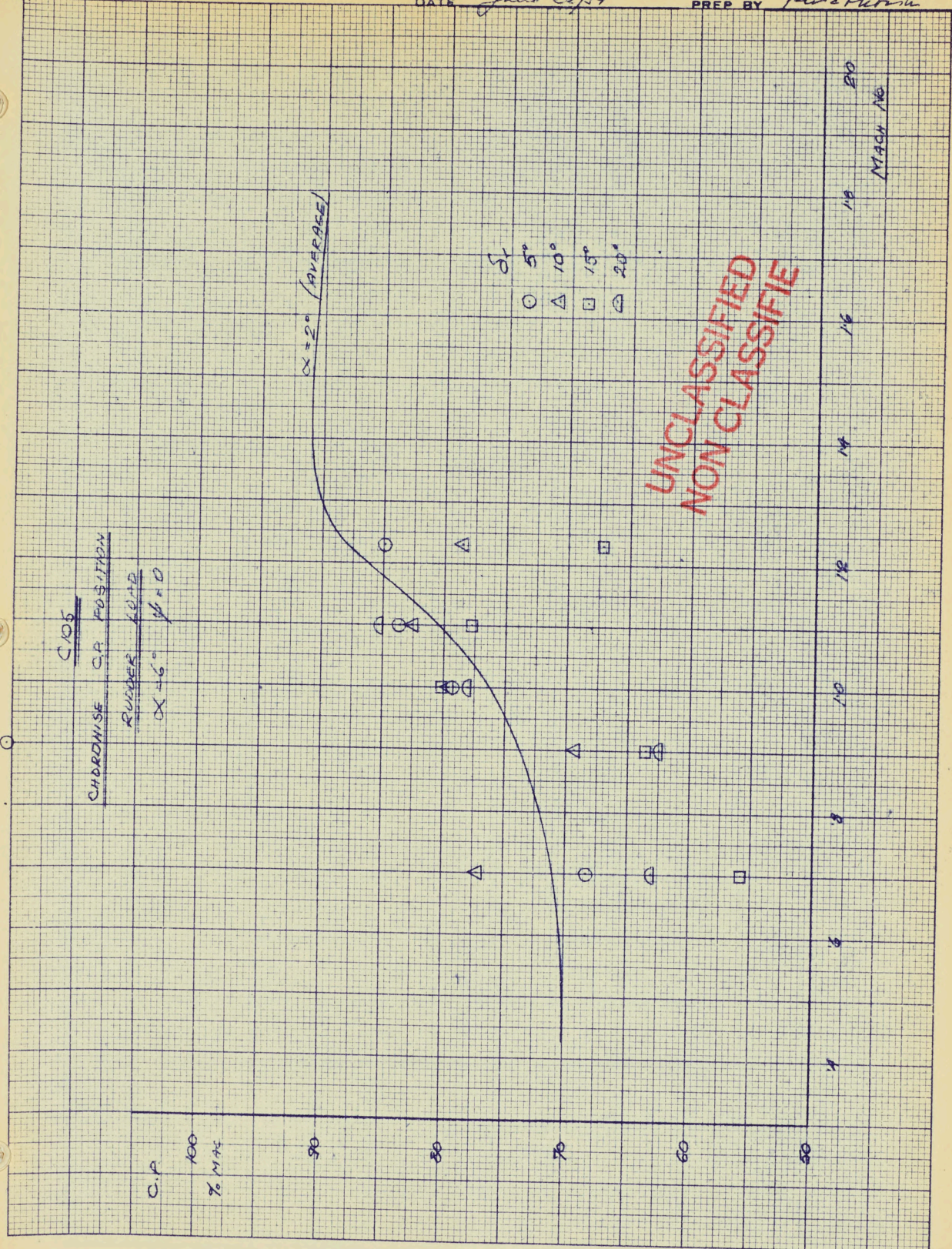
159-12 KEUFFEL & ESSER CO.
10 x 10 to the 1/2 inch. 5th lines accounted.
MADE IN U.S.A.

459-12 REUFEL & LESSER CO.
10 x 10 to the 1/2 inch, 50 lines uncut
MADE IN U.S.A.



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MARCH NUMBER



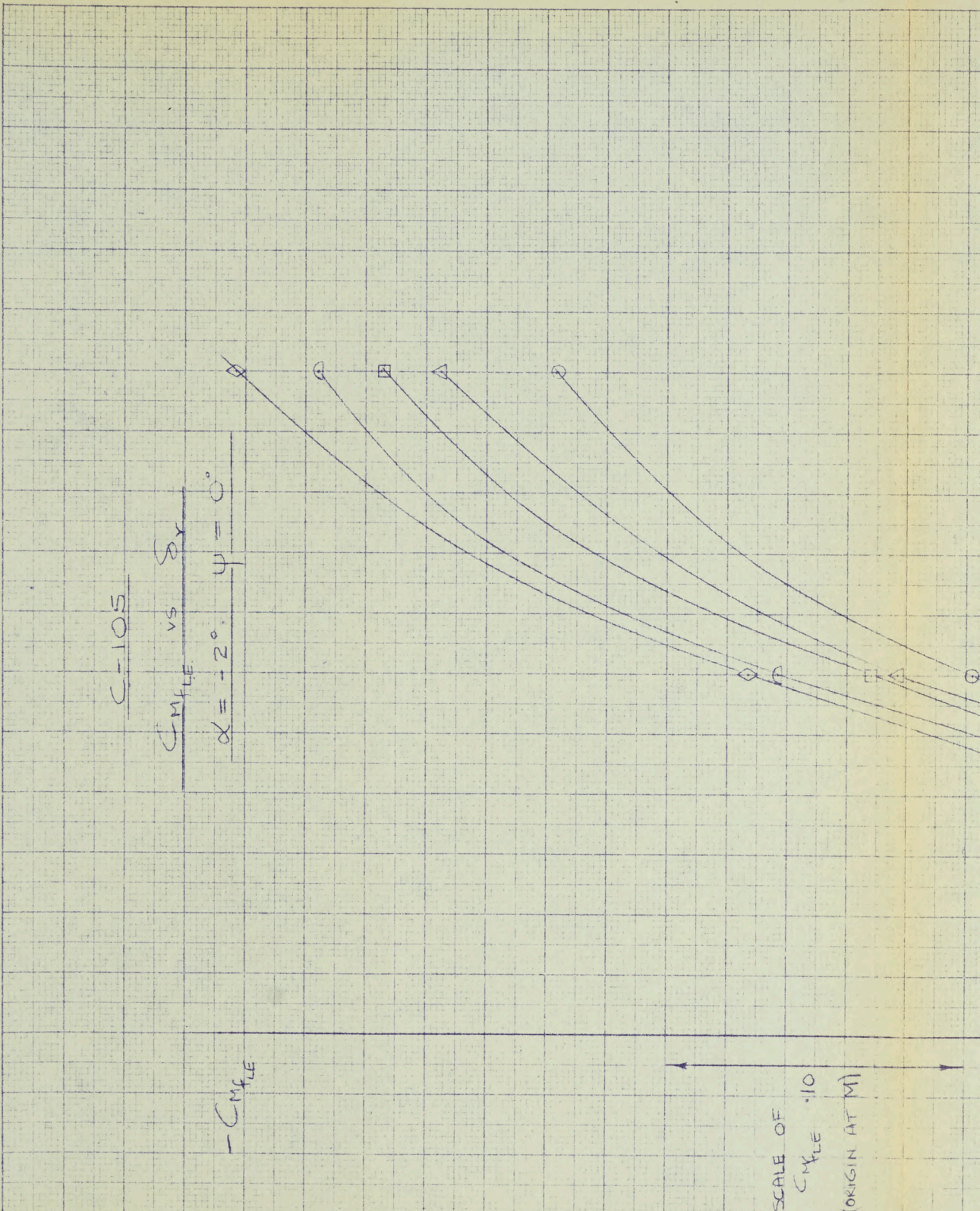
C-105

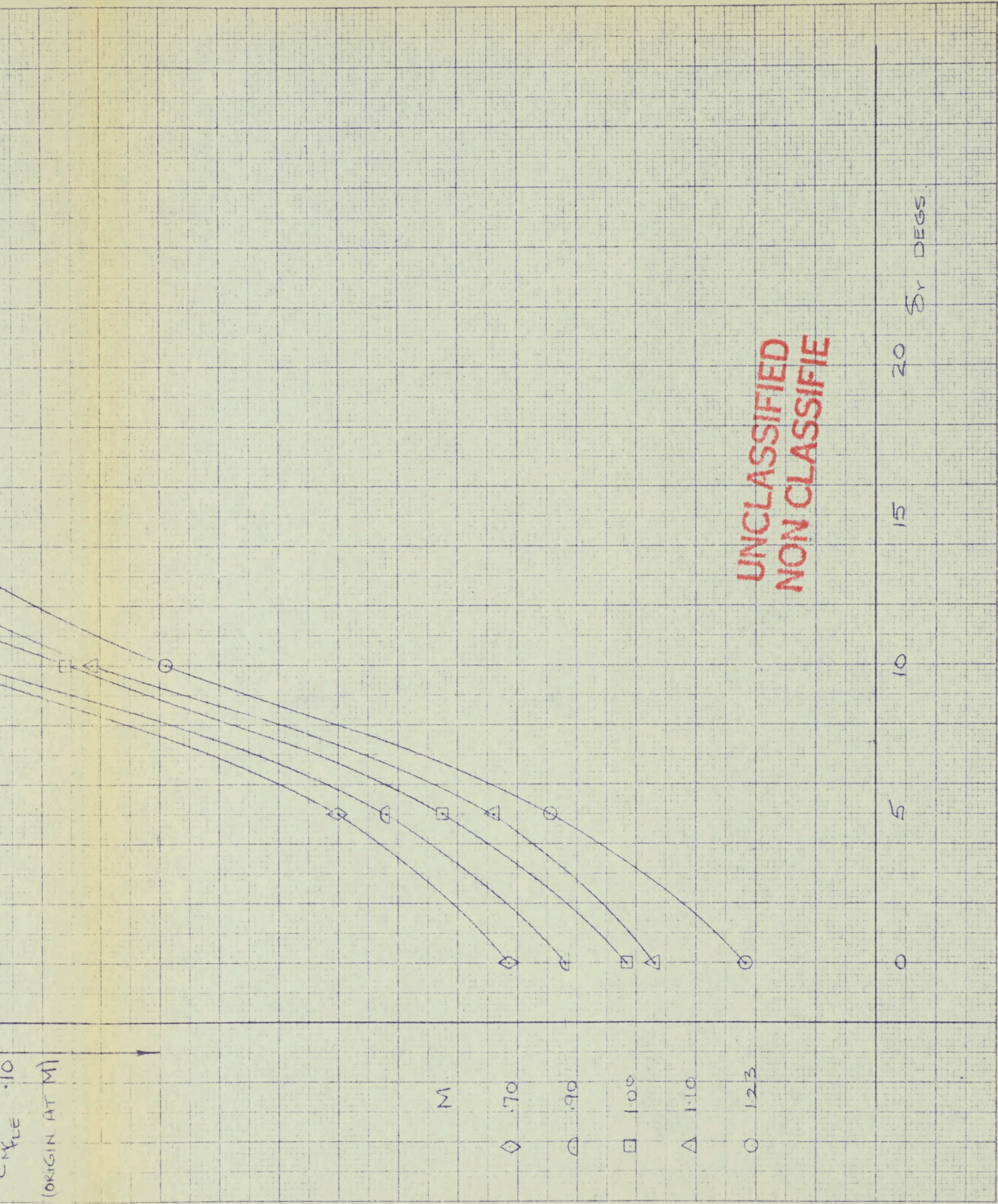
$C_{MFL E}$ vs δy

$\alpha = -2^\circ$ $\psi = 0^\circ$

$-C_{MFL E}$

SCALE OF
 $C_{MFL E} \cdot 10$
(ORIGIN AT M)

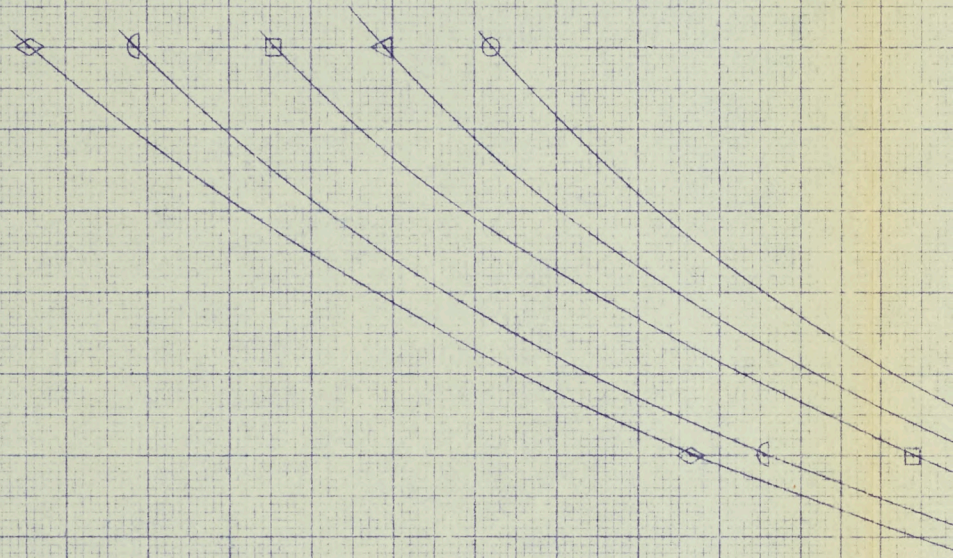




C-105

C_{MfLE} vs δ_x

$\alpha = 0^\circ$ $\psi = 0^\circ$

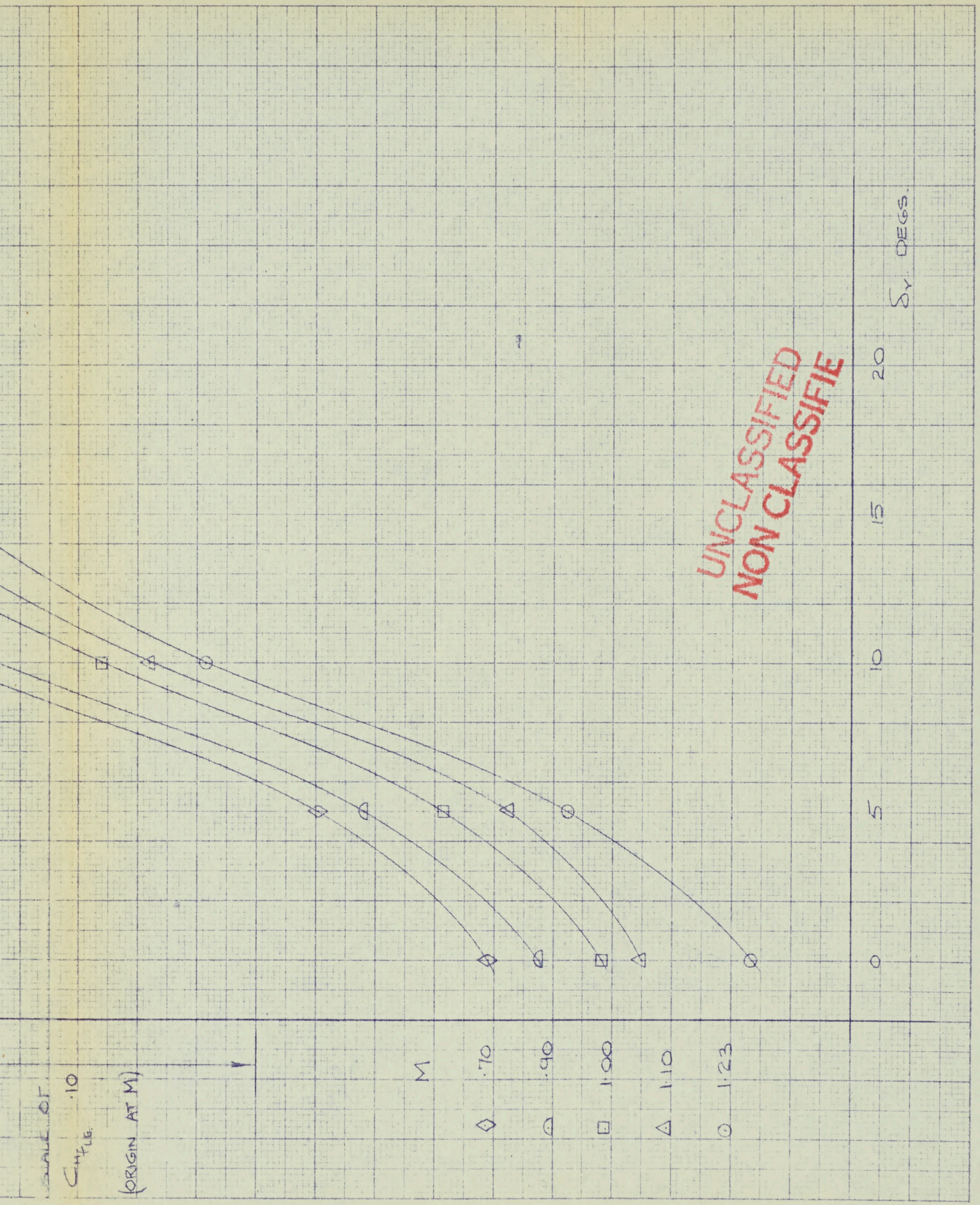


$-C_{MfLE}$

number of

C_{MfLE} 10

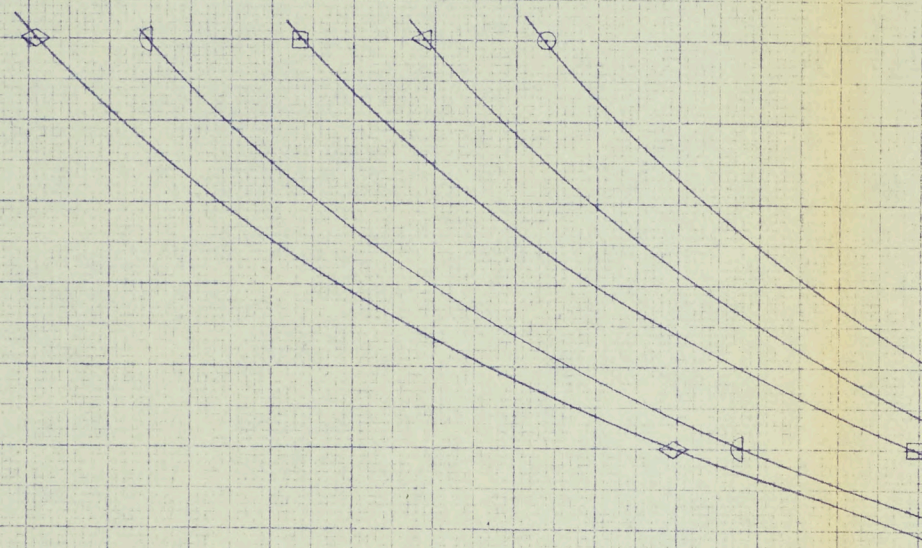
height of fin



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- SAMPLE

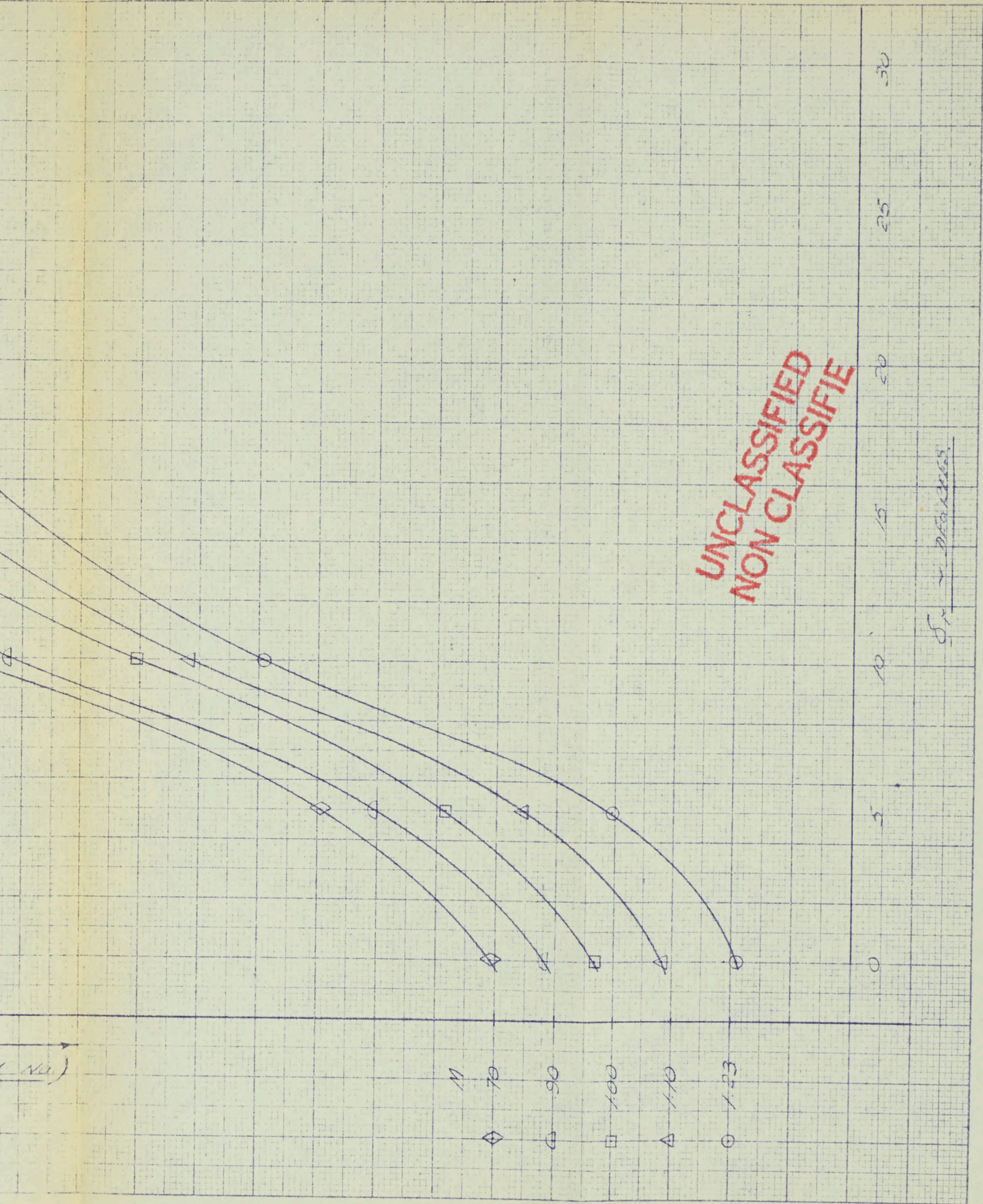
$\frac{0.02}{\text{SAMPLE}} \frac{15}{\text{K}} \frac{50}{\text{K}}$
 $K = 2^\circ \quad K = 0$



.10
(ORIGIN @ MACH NO.)

16.3
NY 54

P/W-T/20
LARR

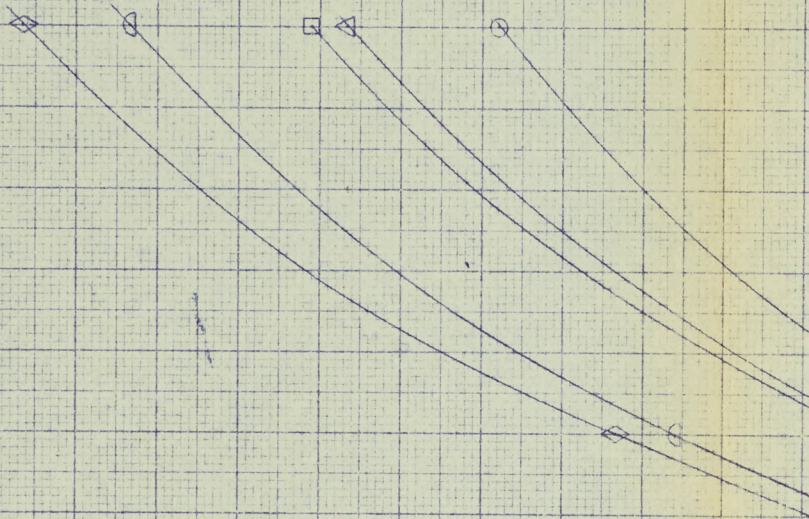


C-105

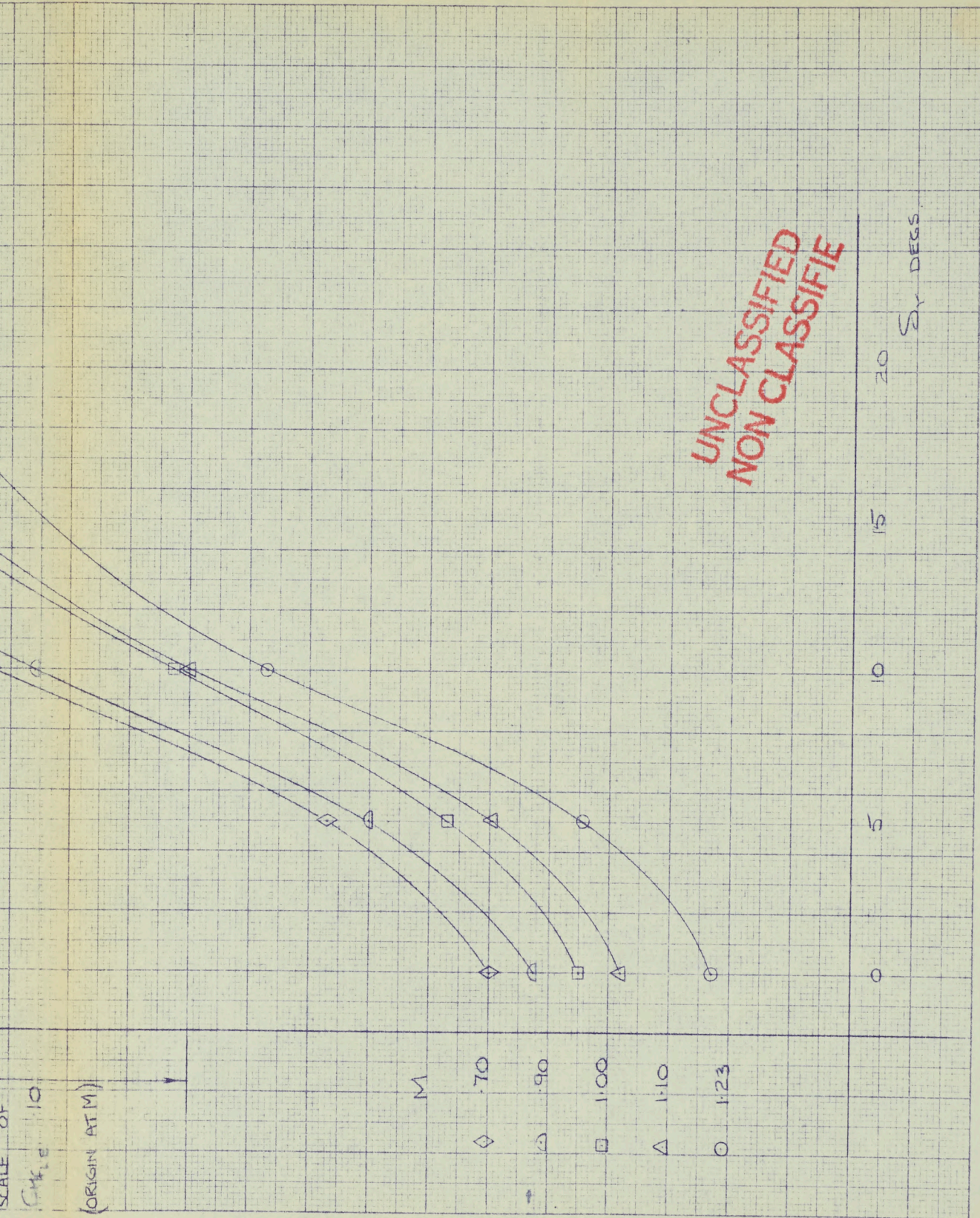
C_{MFL} vs δ_x

$\alpha = -6^\circ$ $\psi = 0^\circ$

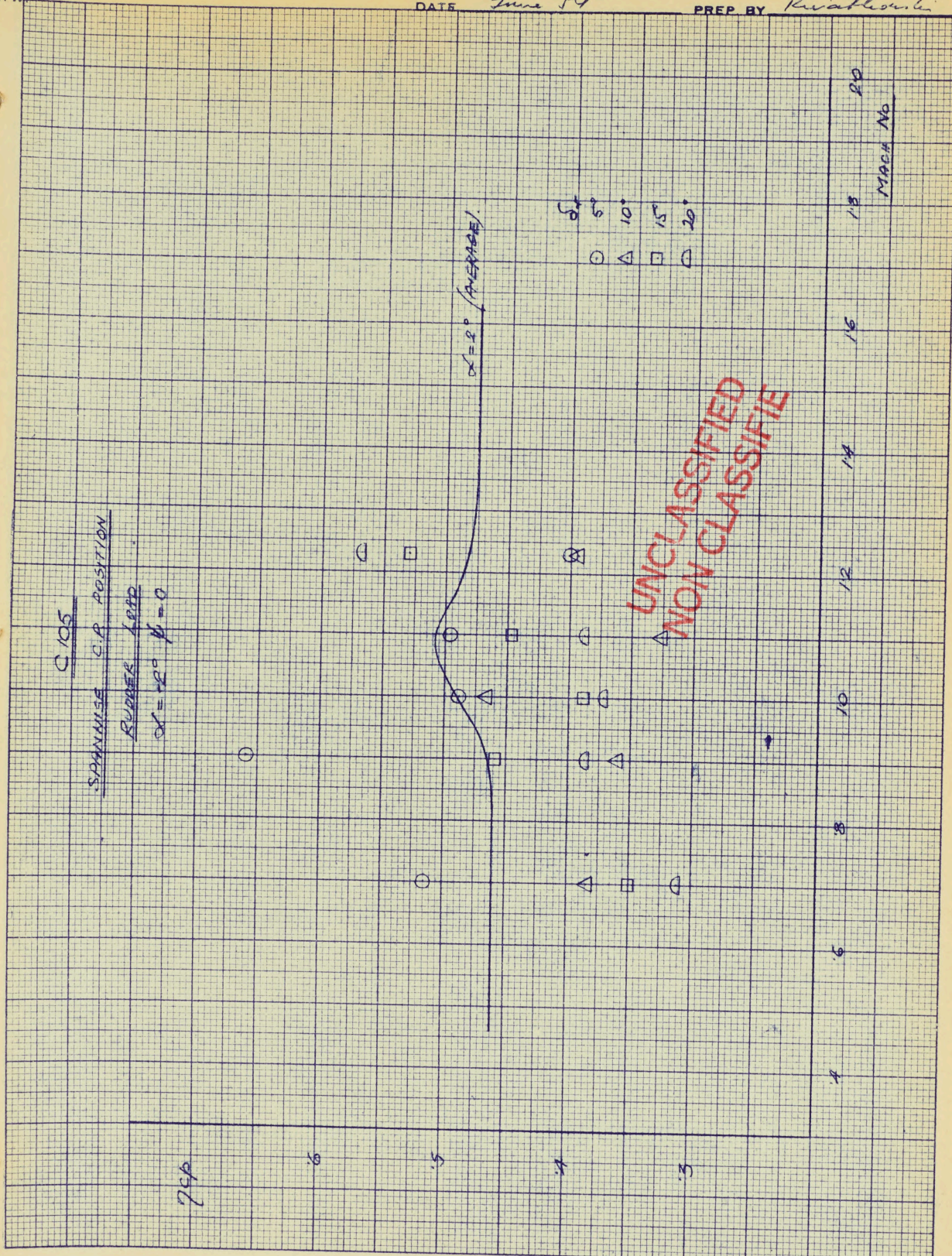
-SAMPLE

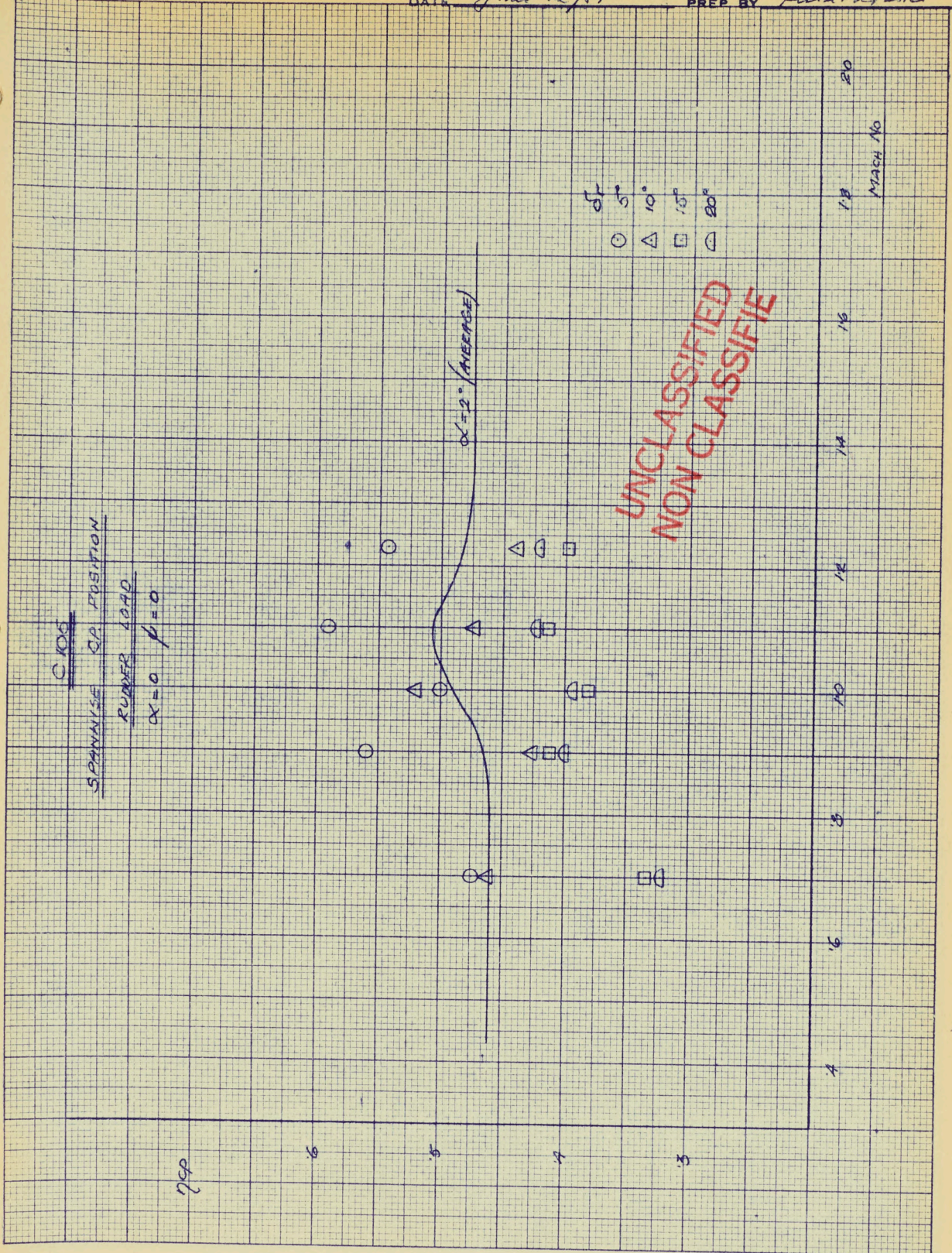


SCALE OF
 C_{MFL} 10
(ORIGIN ATM)



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3-10-5
SPYALMISE C.A. POSITION
CRABER WAD.
0120 X=0

764

7

6

5

4

3

2

1

0

8

10

12

14

16

18

20

0°
5
10
15
20

○ △ □ ◐

MAP NUMBER

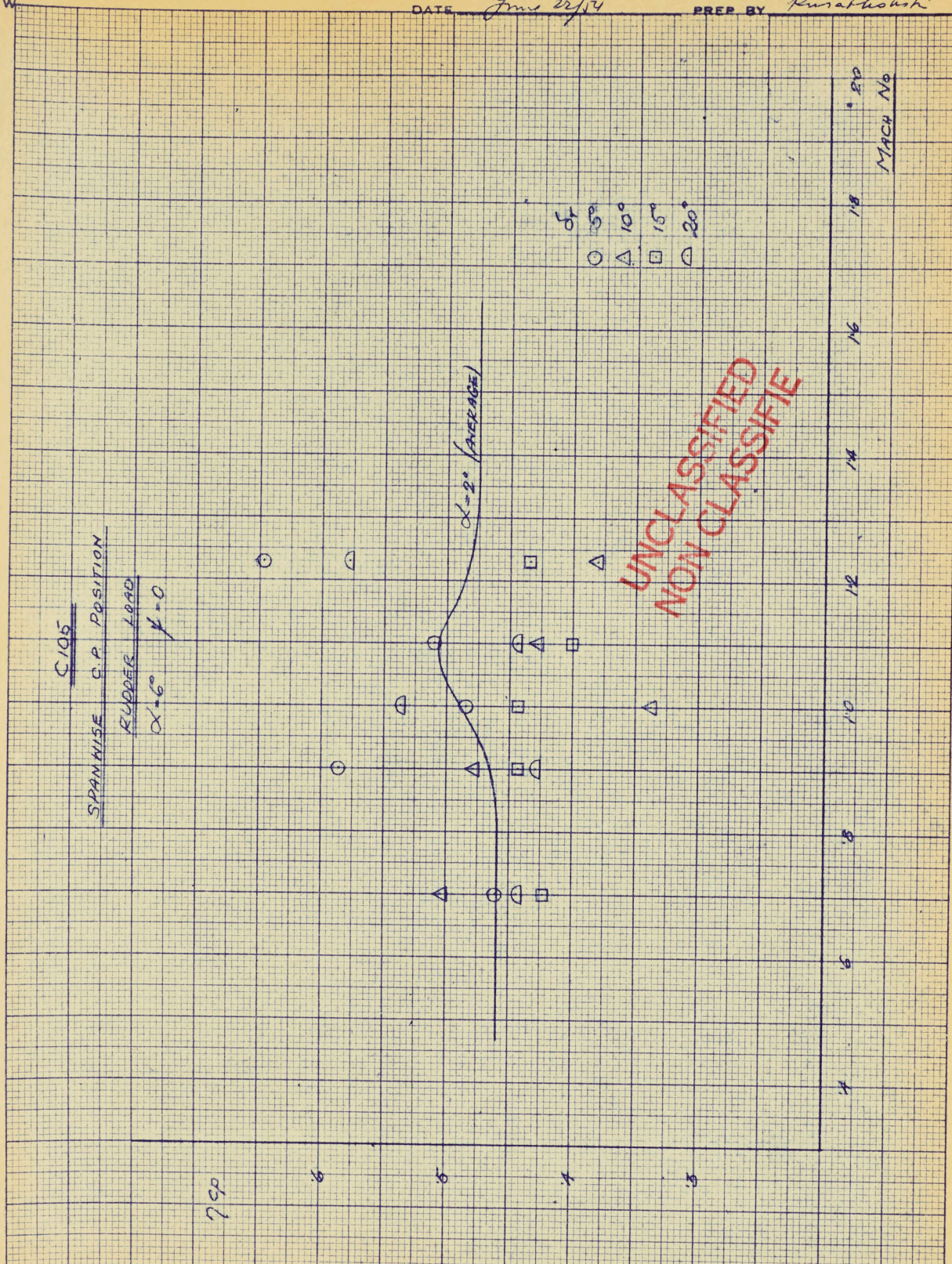
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AIRCRAFT C105
A. U. W.

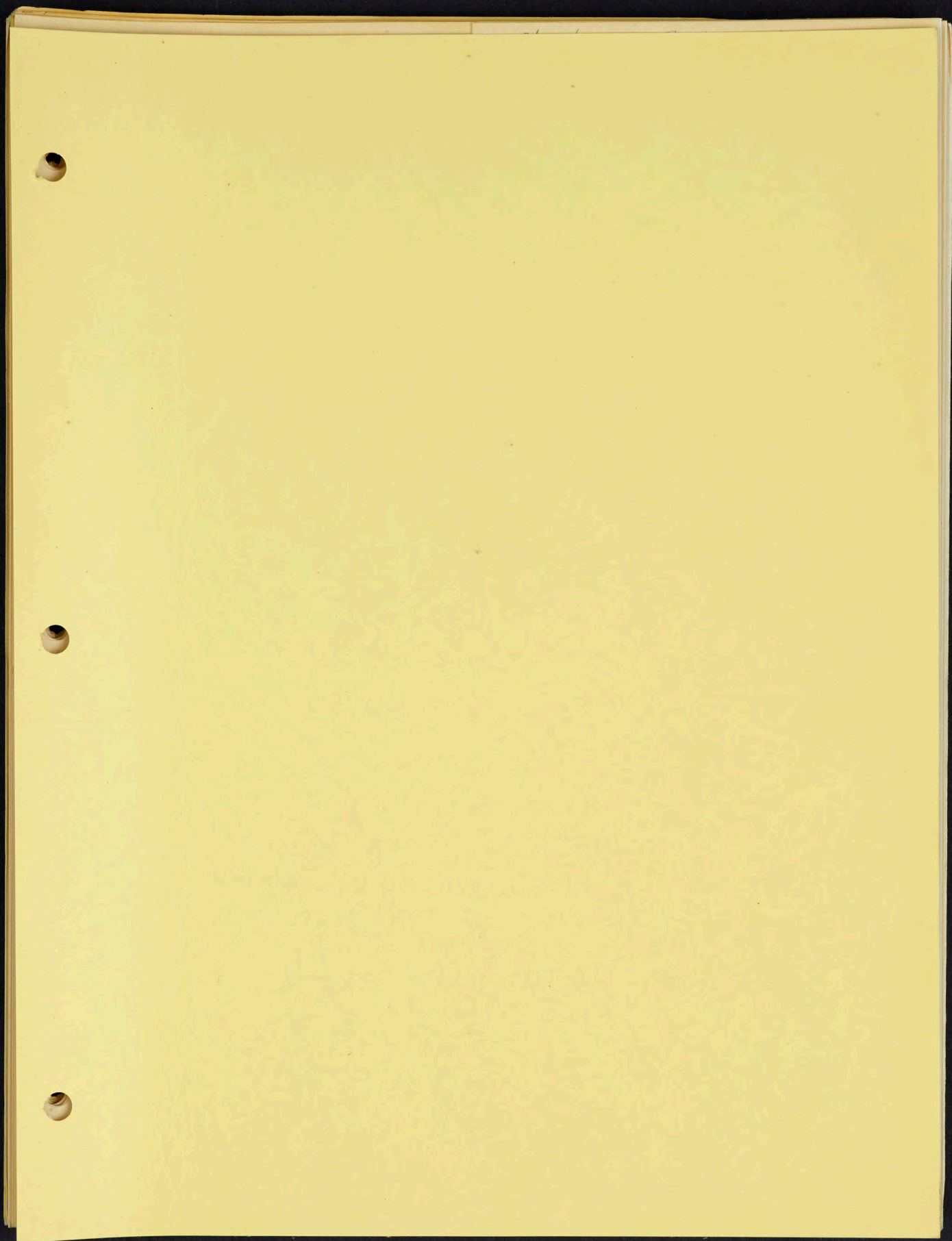
COMPONENT

SHEET No. 1.6.9
DATE June 22/54

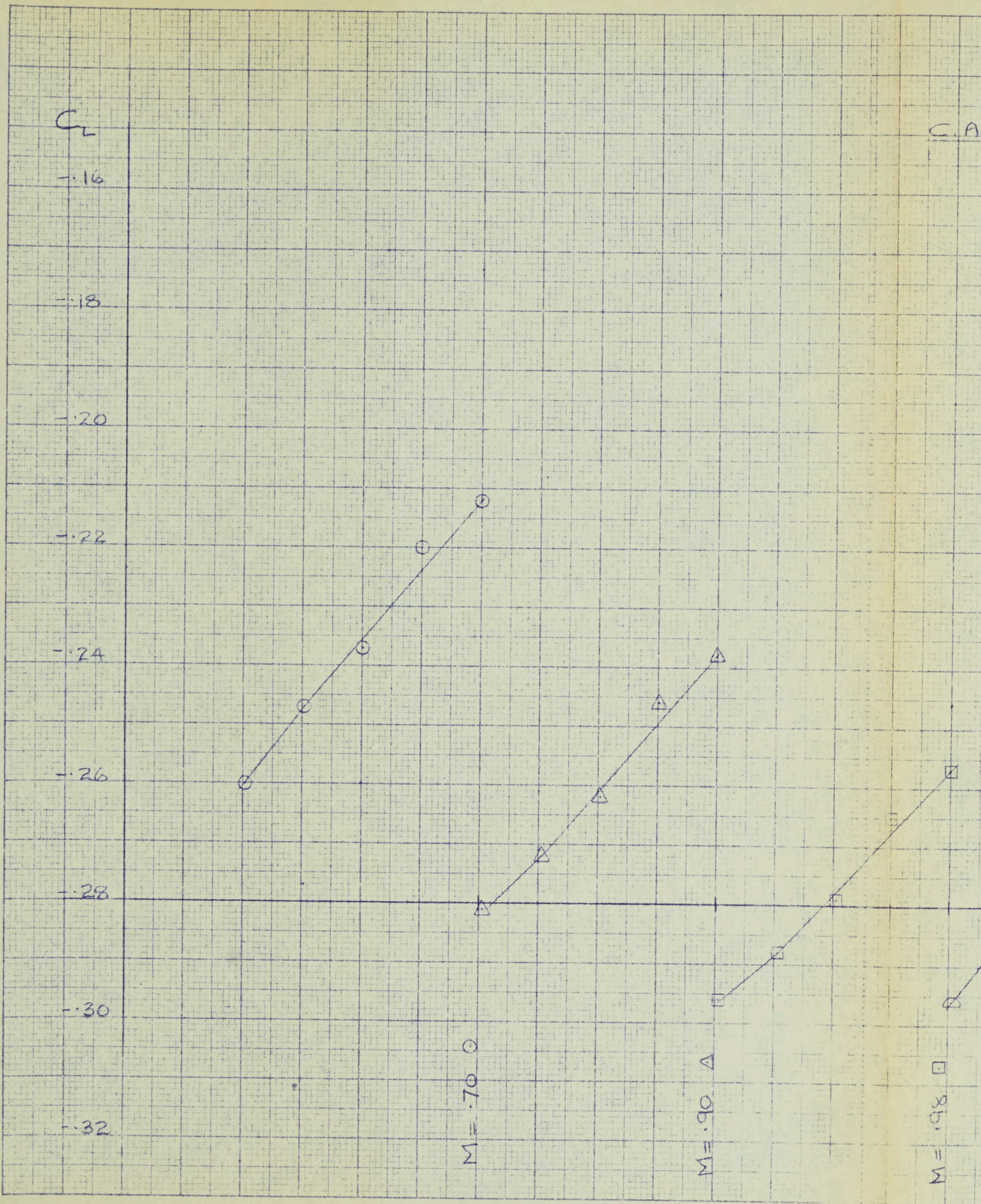
REPORT No. P/W.T./20
PREP BY Kurakhovsk



159-12 KEUFFEL & ESSER CO.
10 x 10 to the 1/2 inch, 5th lines accented.
MADE IN U.S.A.



358-111 KEUFFEL & ESSER CO.
10 x 10 to the 1/2 inch, all lines accepted.
445 08 0 1 4



C-105

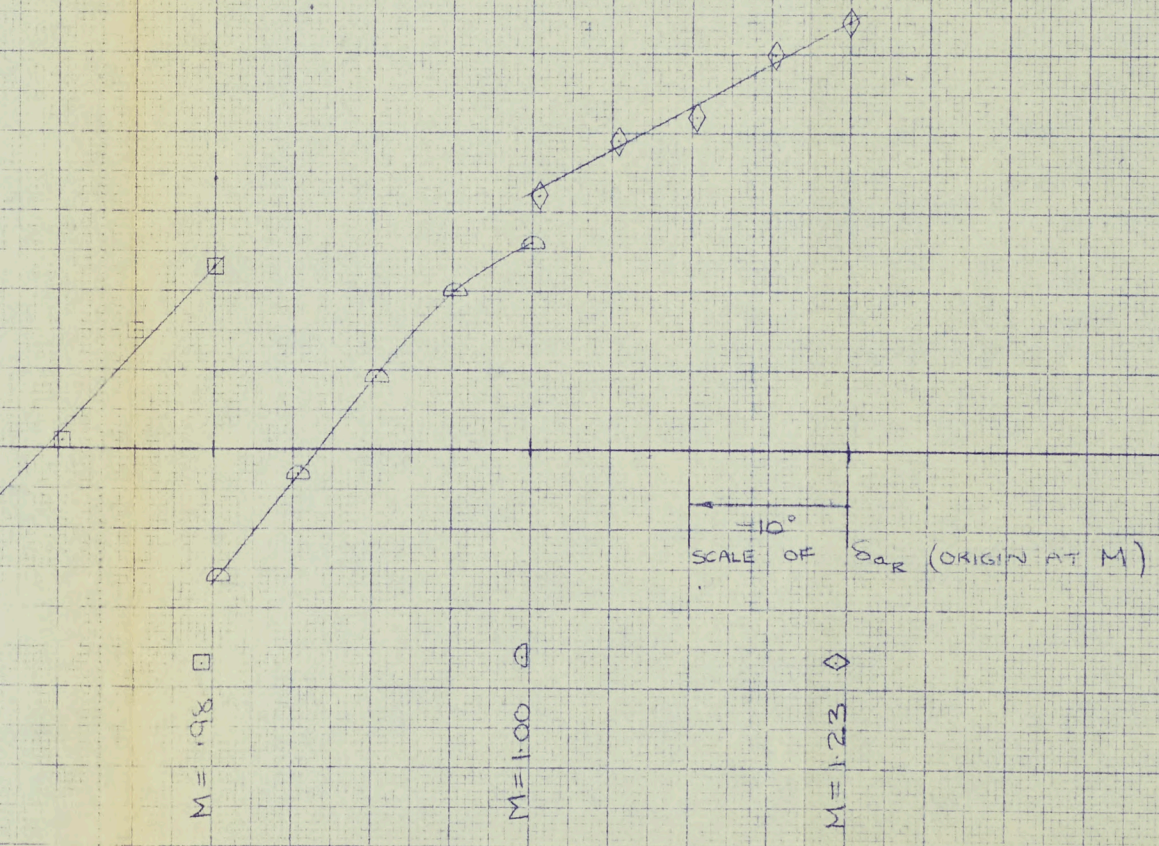
C.A.L. WIND TUNNEL TESTS

C_L vs. δ_{or}

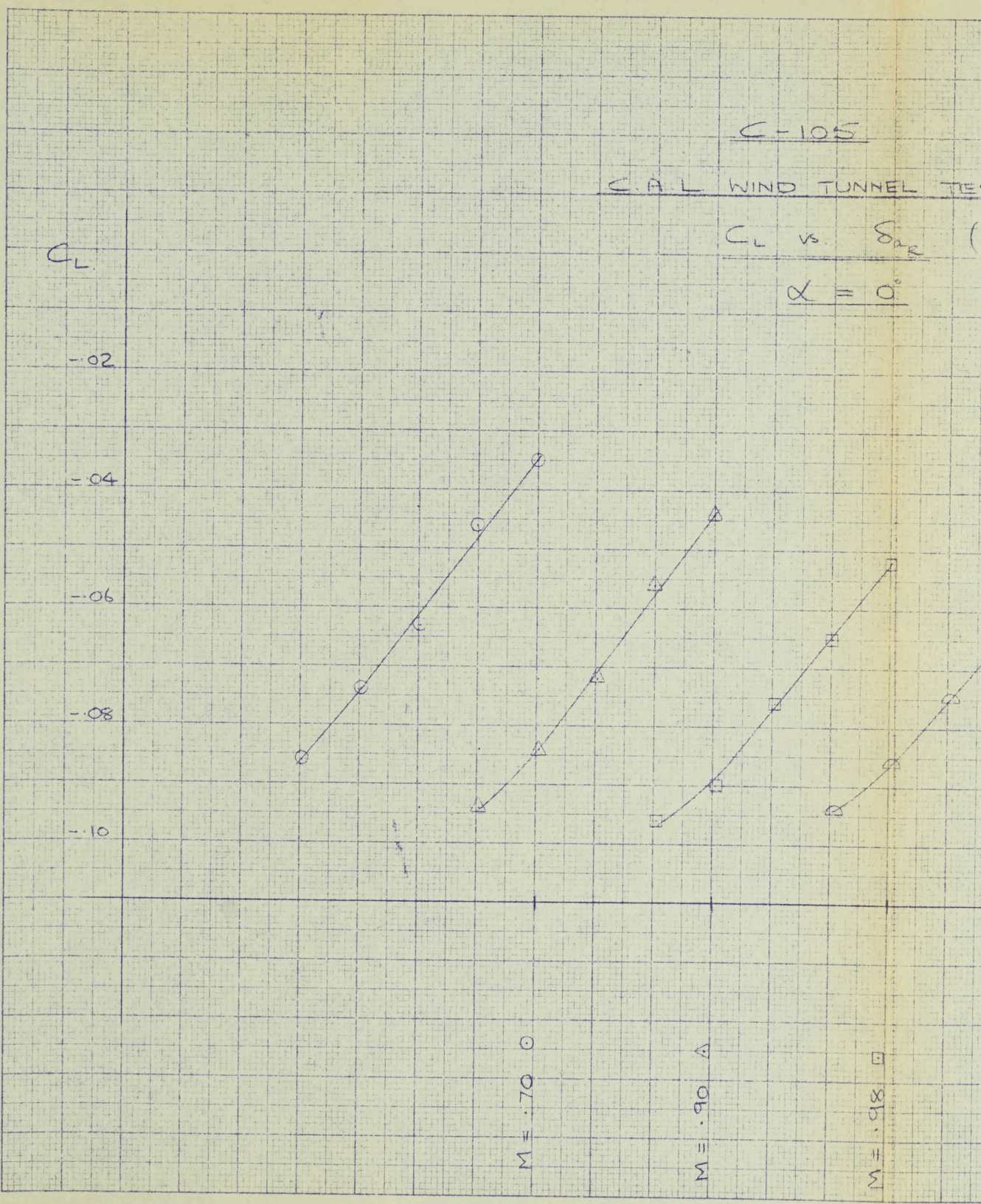
($\delta_{or} = 0^\circ$)

$\alpha = -4^\circ$

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 NON CLASSIFIED



359-111 KEUFFEL & ESSER CO.
10 x 10 1/2 inch grid paper
MADE IN U.S.A.

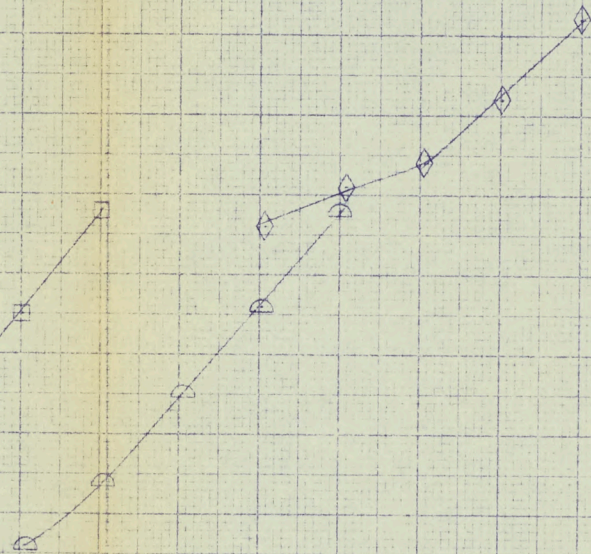


05

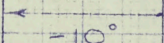
TUNNEL TESTS.

δ_{aR} ($\delta_{aL} = 0^\circ$)

$= 0^\circ$



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SCALE OF δ_{aR} (ORIGIN AT M)

M = 0.98 □

M = 1.00 □

M = 1.23 ◇

C-105

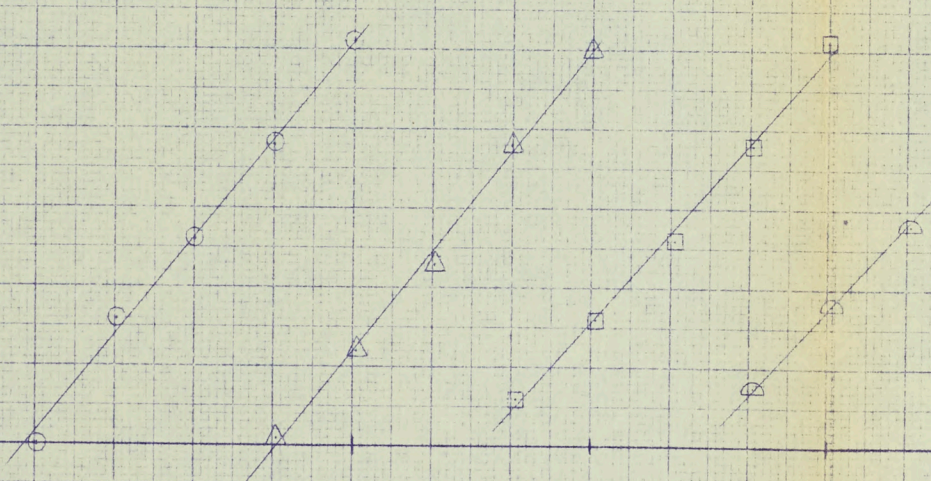
C. A. L. WIND TUNNEL TESTS

C_L vs δ_{aR} ($\delta_{aL} = 0^\circ$)

$\alpha = 2^\circ$

C_L

0
.02
.04
.06
.08



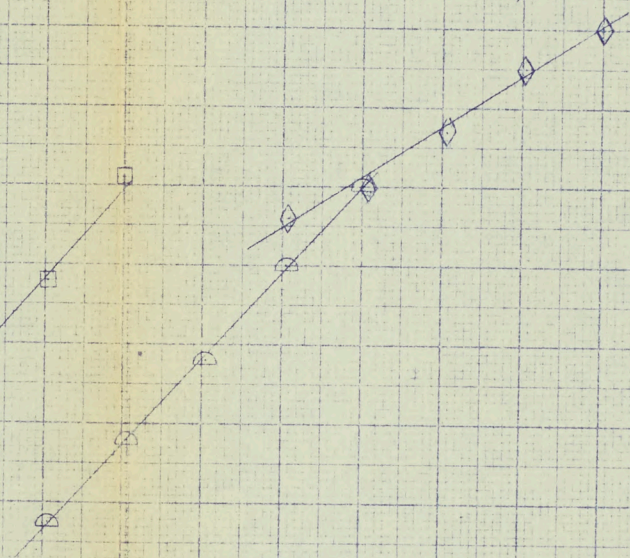
$M = .70$ ○

$M = .90$ △

$M = .98$ □

= 0°)

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10°

SCALE OF σ_{aR} (ORIGINS AT M)
+ve TO RIGHT.

M = .98 □

M = 1.00 ◊

M = 1.23 ◊

C-105

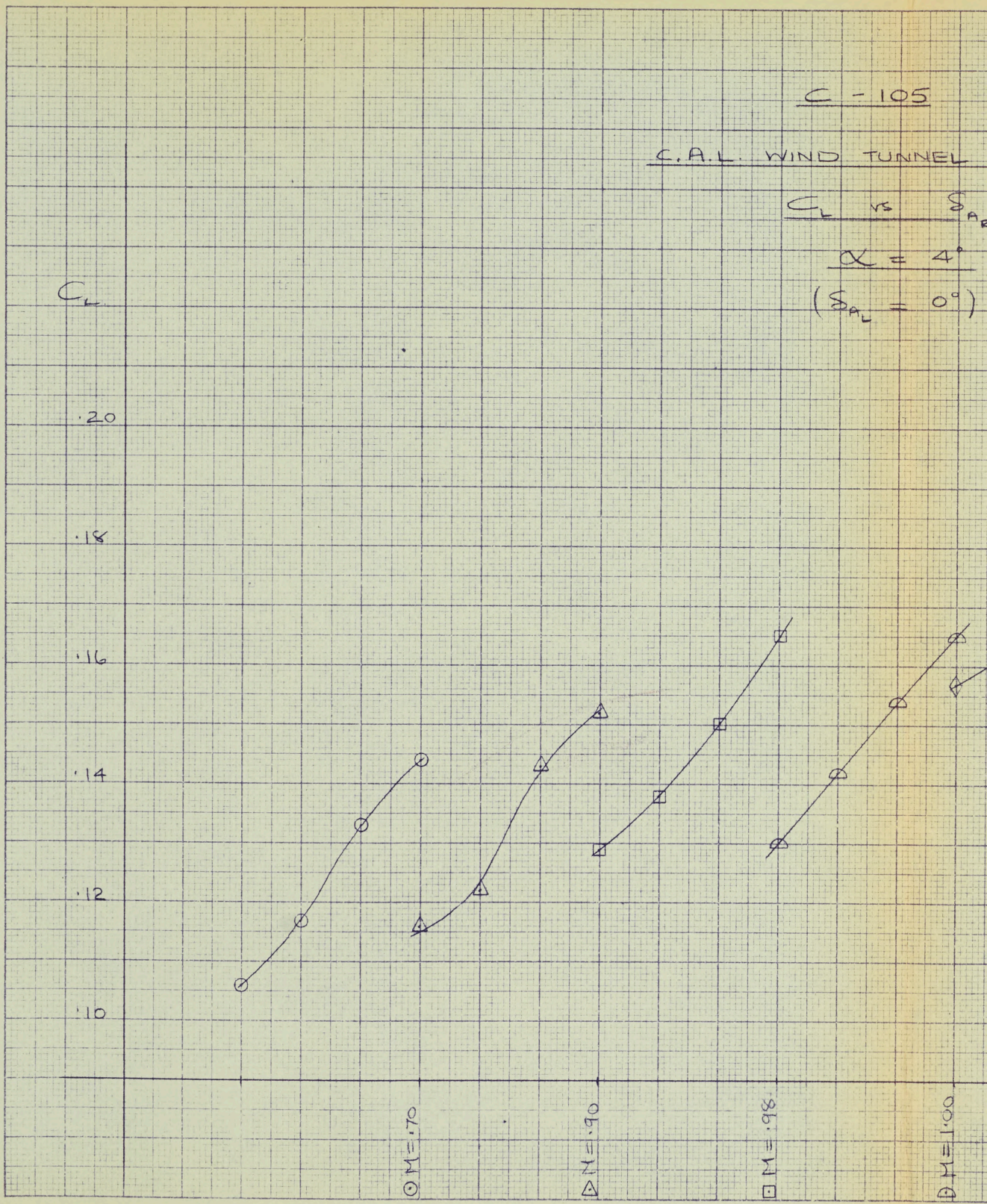
C.A.L. WIND TUNNEL

C_L vs S_{AR}

$\alpha = 4^\circ$

($S_{AR} = 0^\circ$)

C_L



- 105

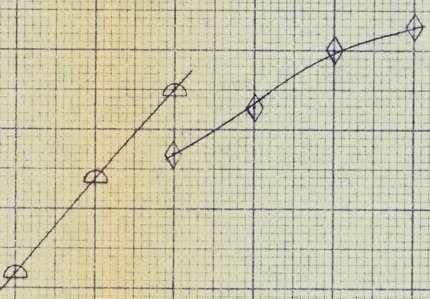
TUNNEL TESTS APRIL 54.

vs σ_{AR}

$\alpha = 4^\circ$

$\sigma_{AL} = 0^\circ$

NOTE: σ_{AR} UNCORRECTED FOR MEASURED VALUE OR ELASTICITY.



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$\circ M=100$

$\diamond M=123$

5° SCALE OF σ_{AR}
 (ORIGIN AT M)

C-105

C.A.L. WIND TUNNEL TESTS.

C_L

C_L VS δ_{AR}

$(\delta_{AL} = 0^\circ)$

$\alpha = 6^\circ$

.30

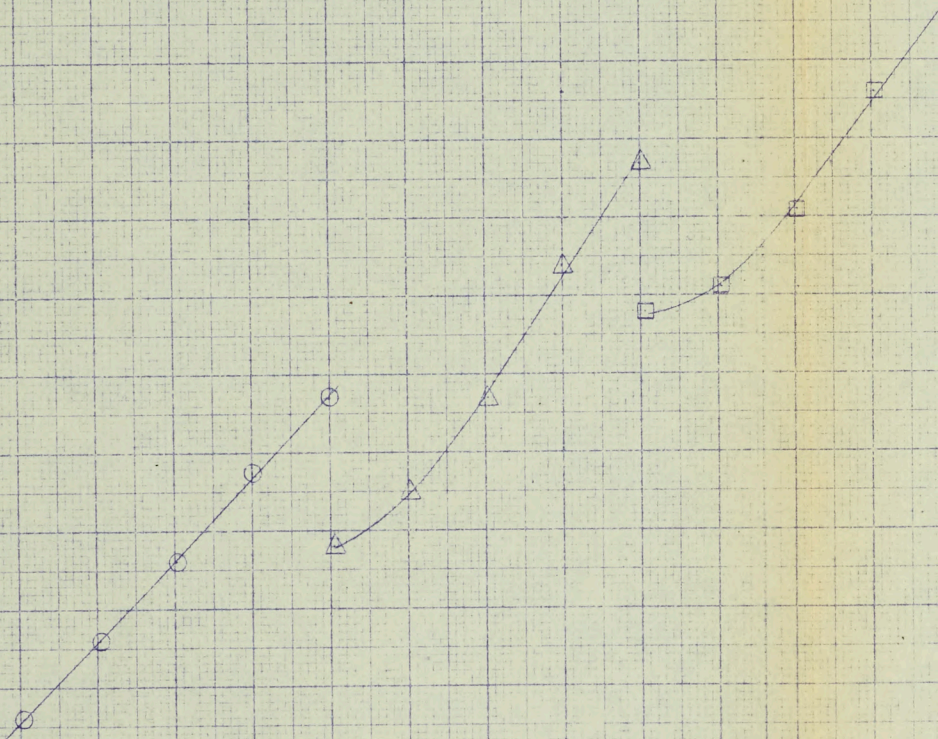
.28

.26

.24

.22

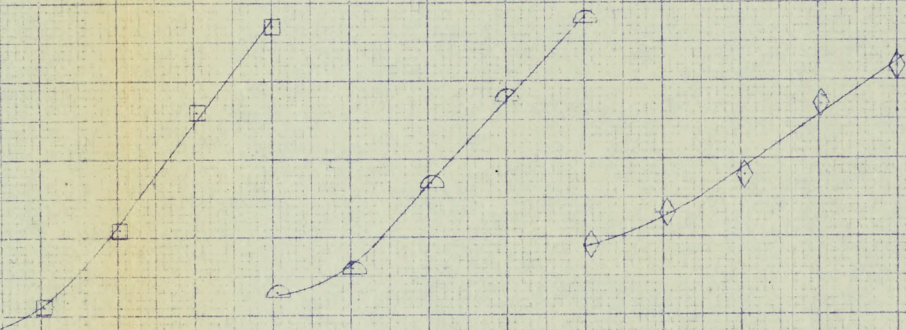
.20



SCALE OF δ_{AR}
ORIGIN AT M.

$M = .70$ ○

$M = .90$ △

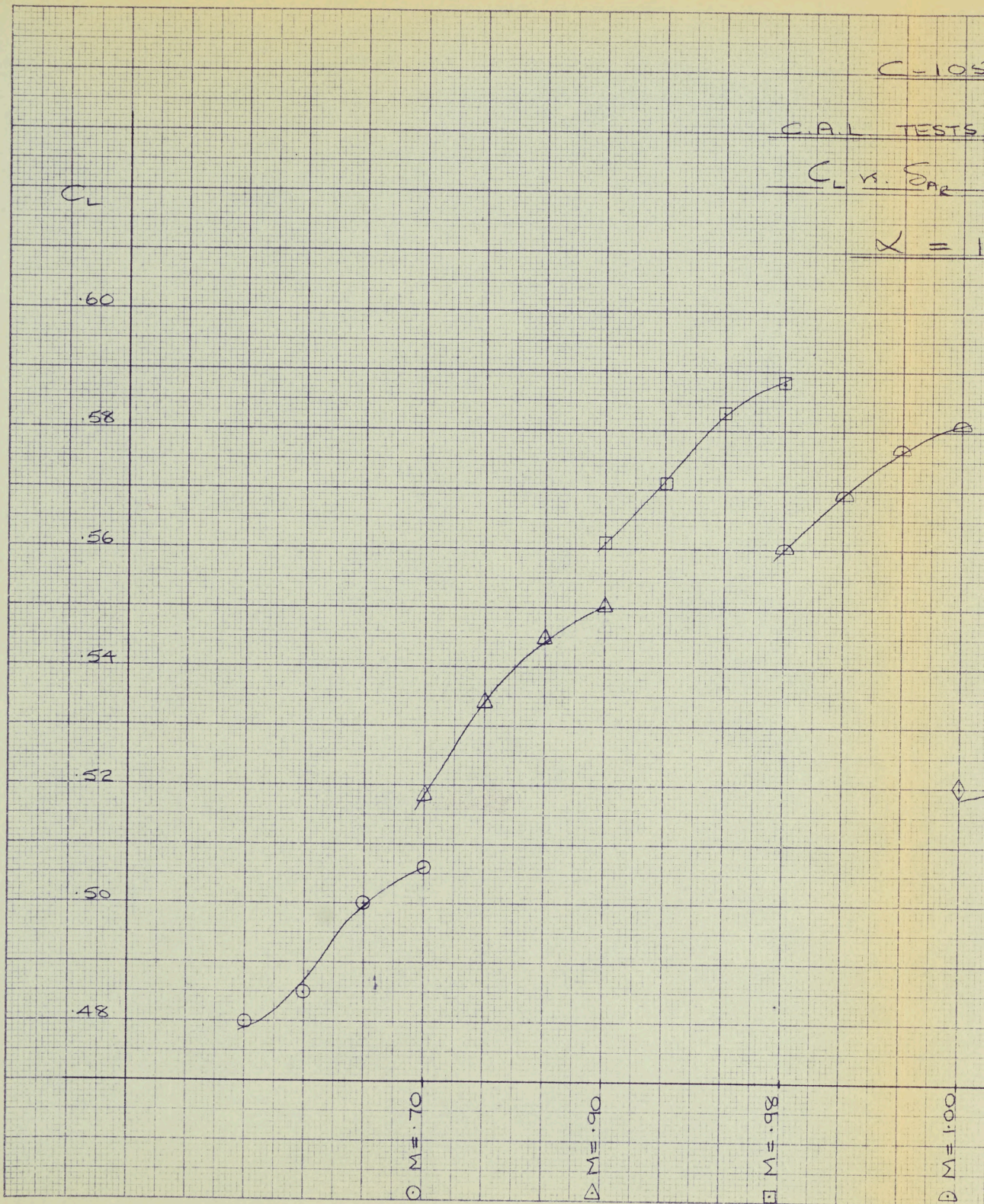


M = .98 □

M = 1.00 ○

M = 1.23 ◇

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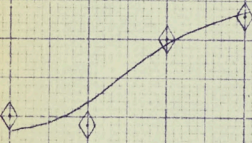
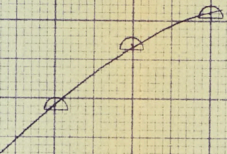
C-105

A.L. TESTS APRIL '54

C.L.V. δ_{AR} ($\delta_{AL} = 0^\circ$)

$\alpha = 11^\circ$

NOTE: δ_{AR} UNCORRECTED FOR MEASURED VALUE OR ELASTICITY

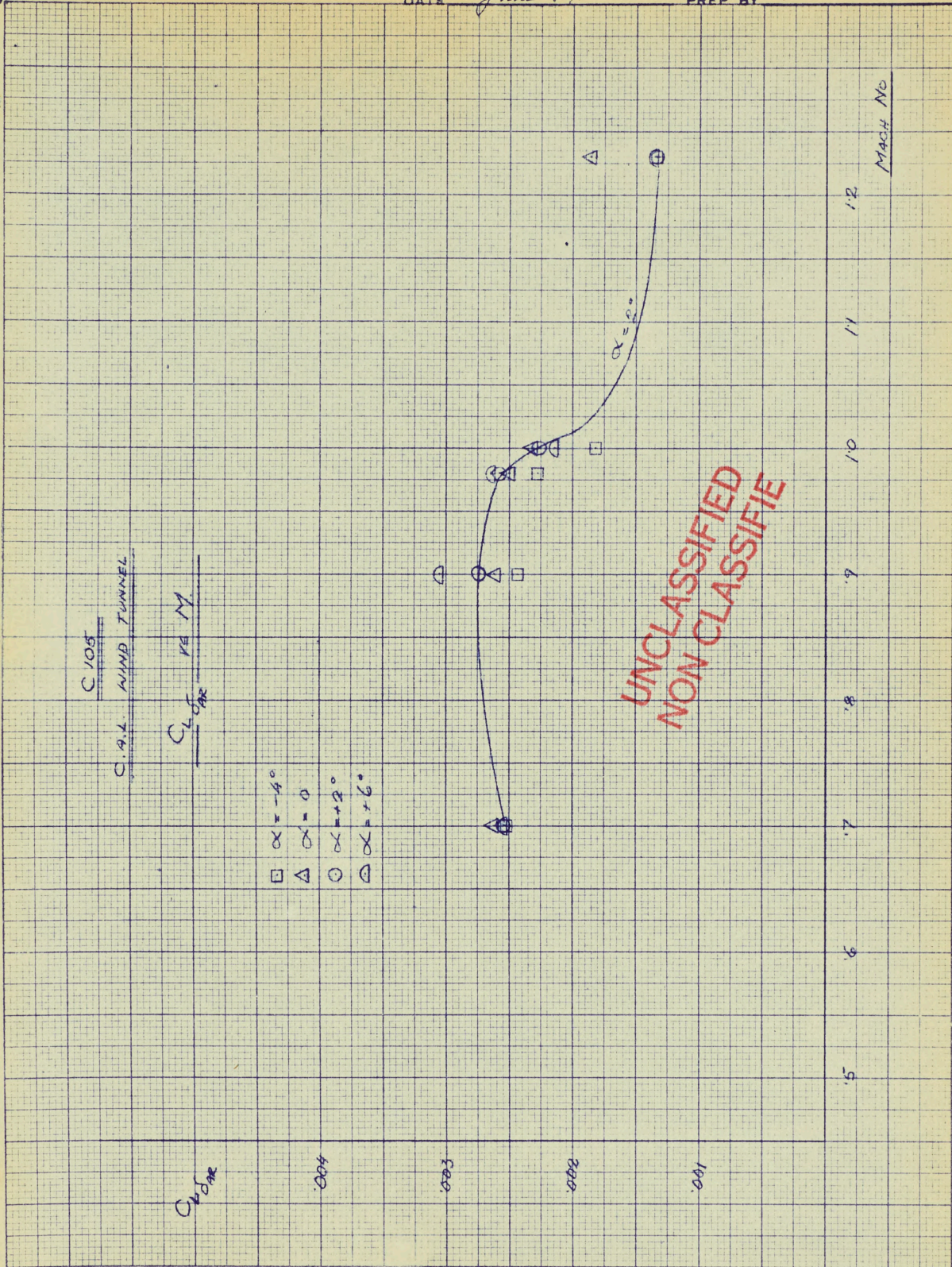


$\diamond M = 1.00$

$\diamond M = 1.23$

5° SCALE OF δ_{AR}
(ORIGIN AT M)

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959-12 KEUFFEL & ESSER CO.
10 x 10 to the 1/2 inch. 5th lines accounted.
MADE IN U.S.A.

359 III. KIEFEL & ESSER CO.
10 x 10 to the 1/2 inch, 2 1/2 inch increments.
MADE IN U.S.A.

C-105

C.A.L. WIND TUNNEL TESTS

C_L vs S_{AR}
($S_{AL} = 0$)
 $\alpha = -4^\circ$

C_L

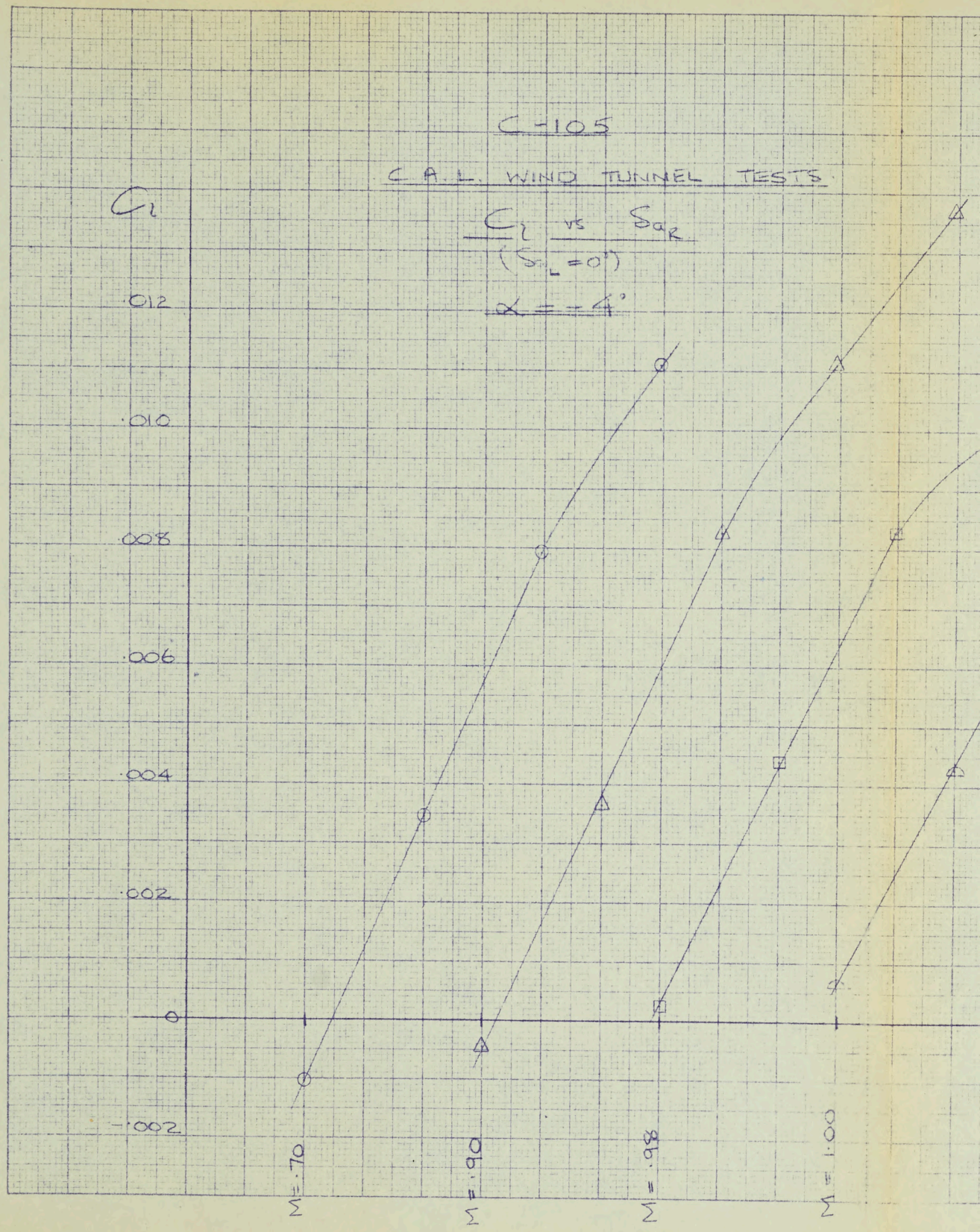
0.12
0.10
0.08
0.06
0.04
0.02
0
-0.02

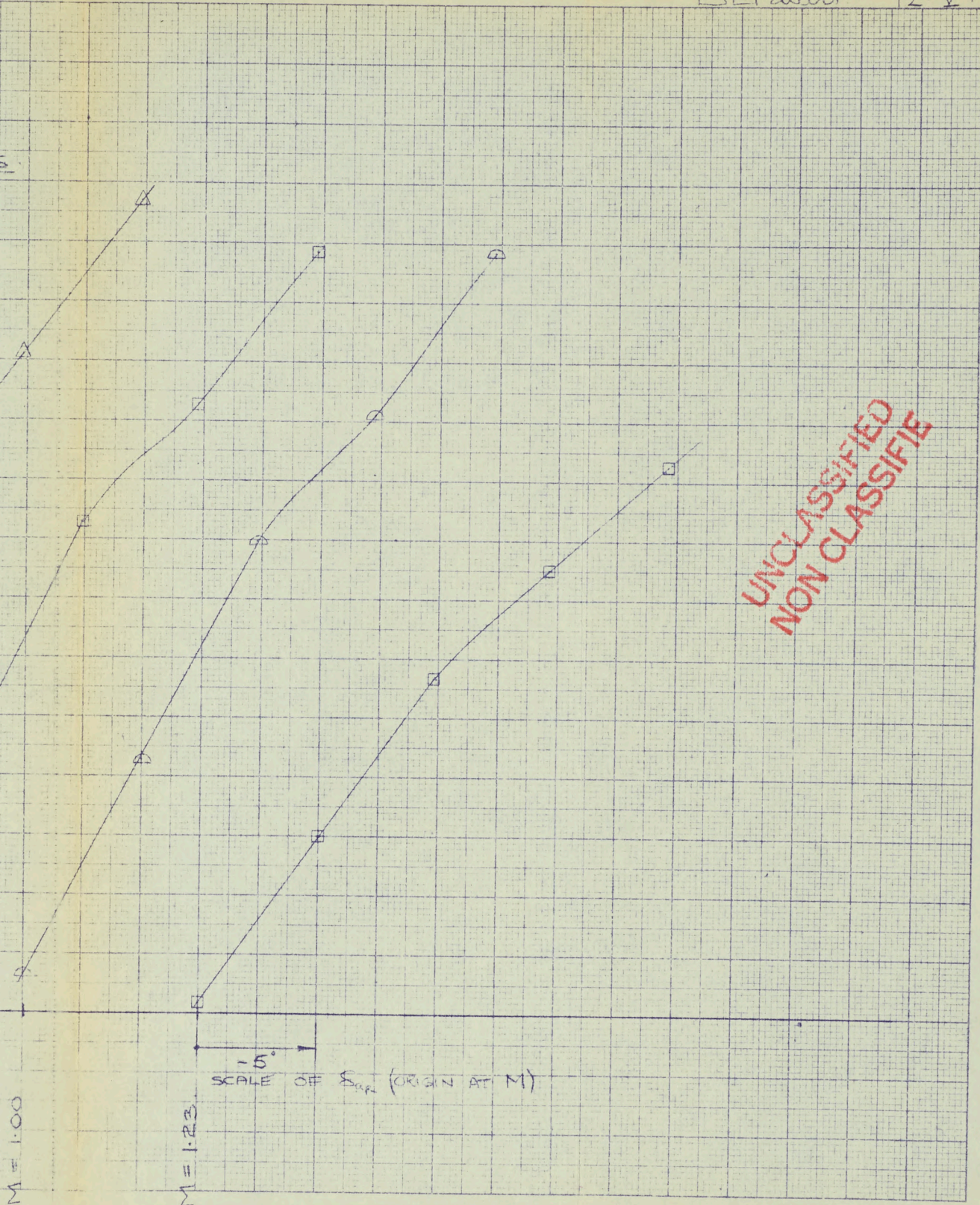
$M = .70$

$M = .90$

$M = .98$

$M = 1.00$





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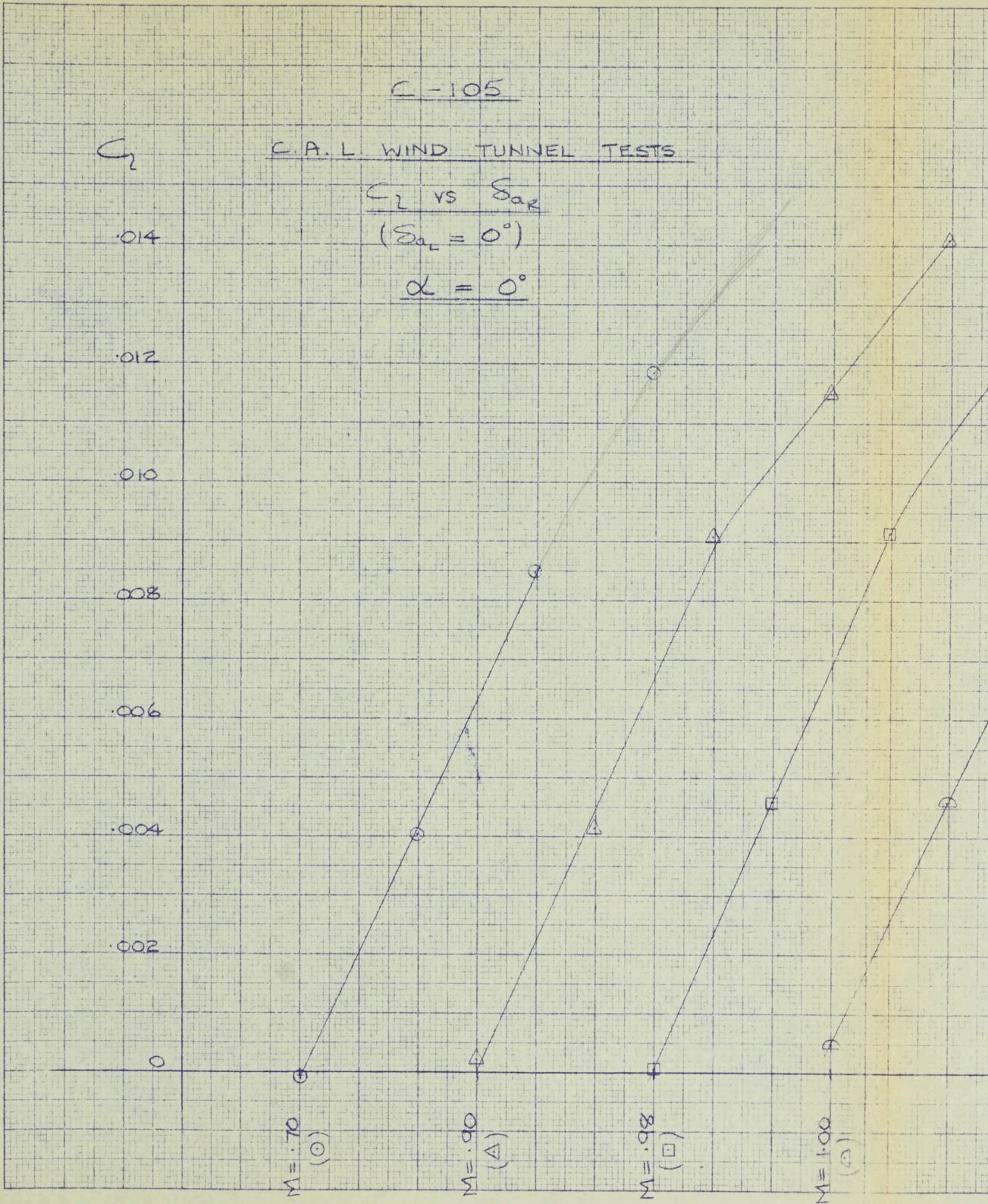
C-105

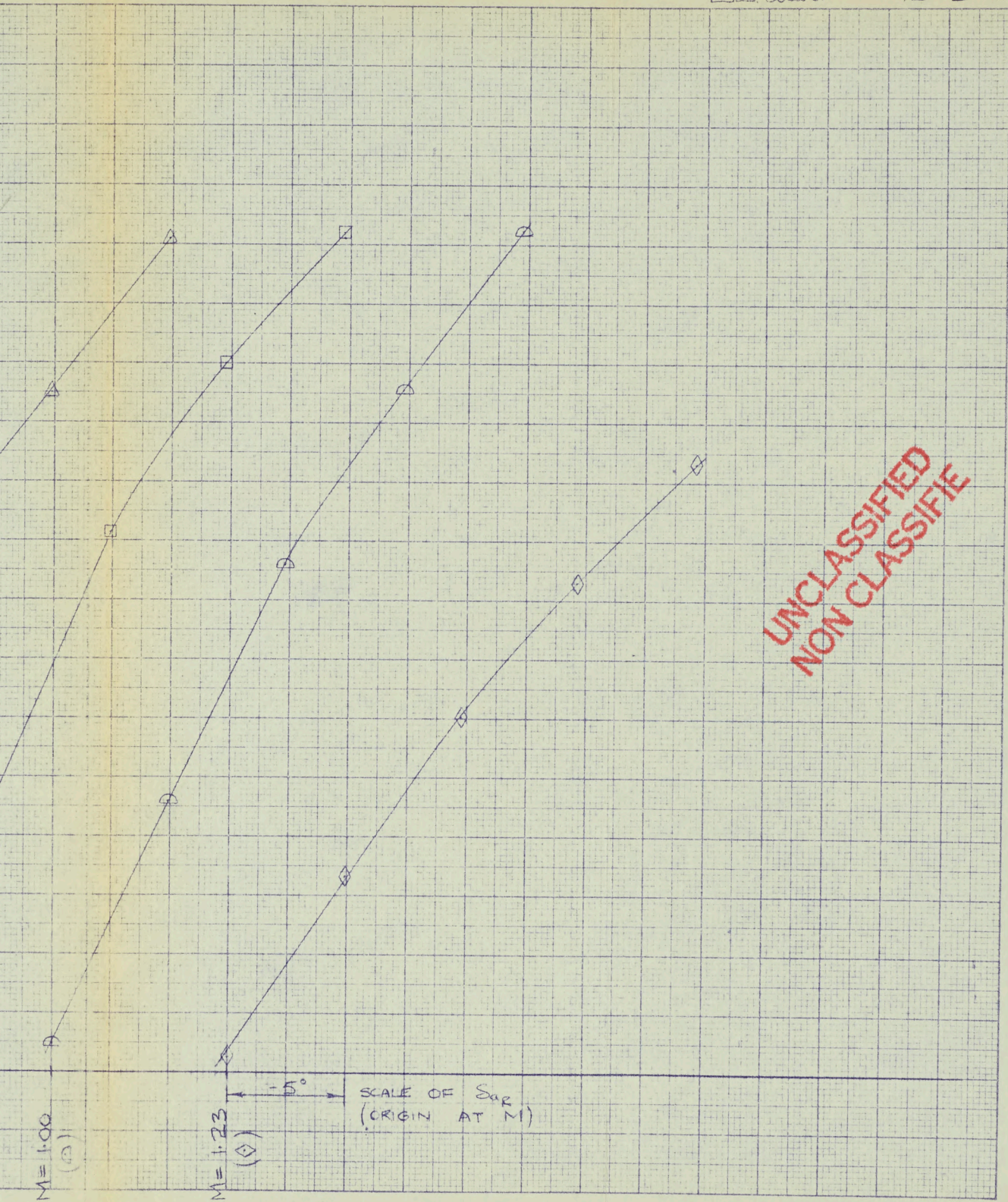
C.A.L. WIND TUNNEL TESTS

C_L vs δ_{aL}

$(\delta_{aL} = 0^\circ)$

$\alpha = 0^\circ$





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C-105

C.A.L. WIND TUNNEL TESTS

C_L vs δ_{aR}

($\delta_{aL} = 0^\circ$)

$\alpha = 2^\circ$

C_L

.014

.012

.010

.008

.006

.004

.002

0

M = .70
(O)

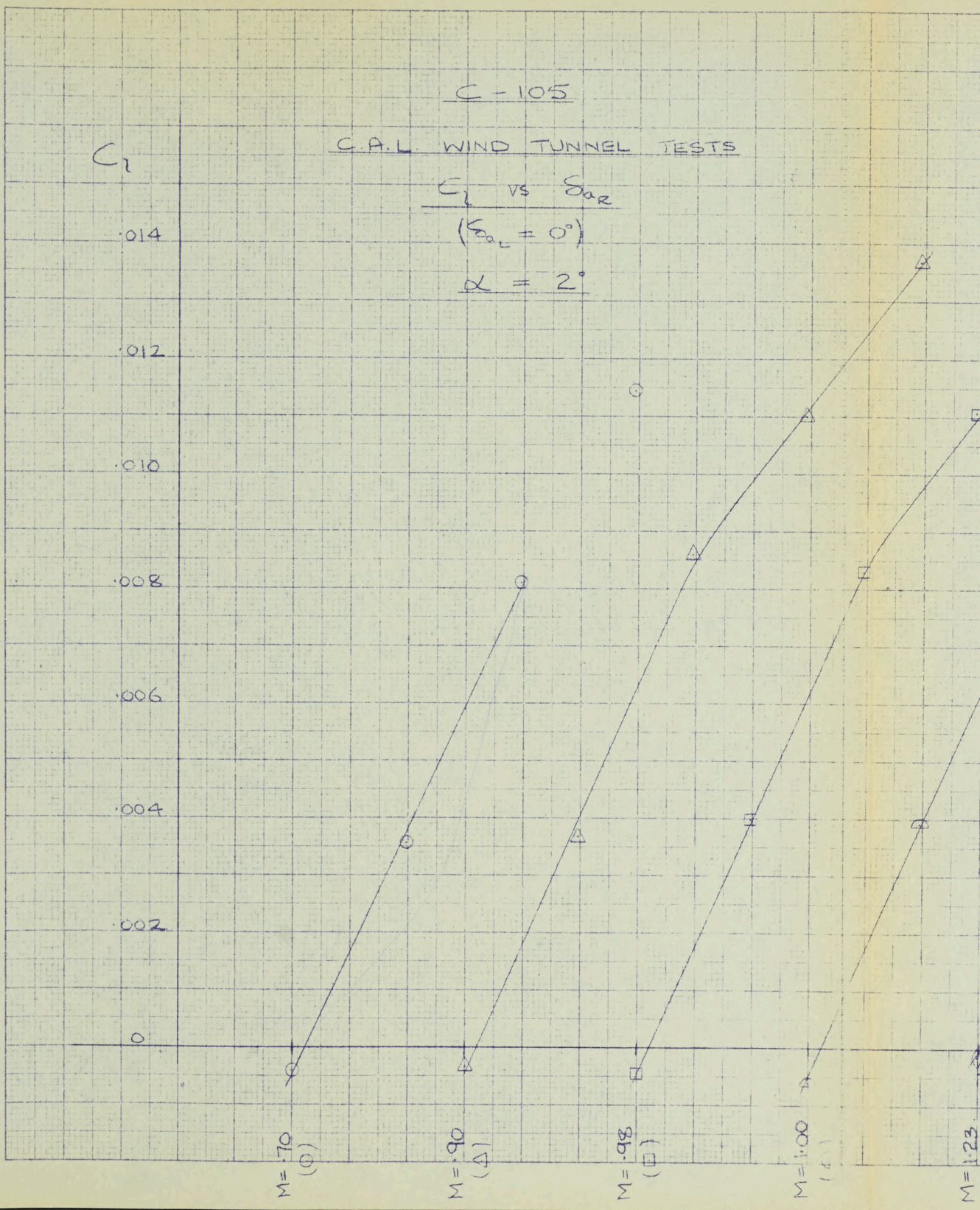
M = .90
(Δ)

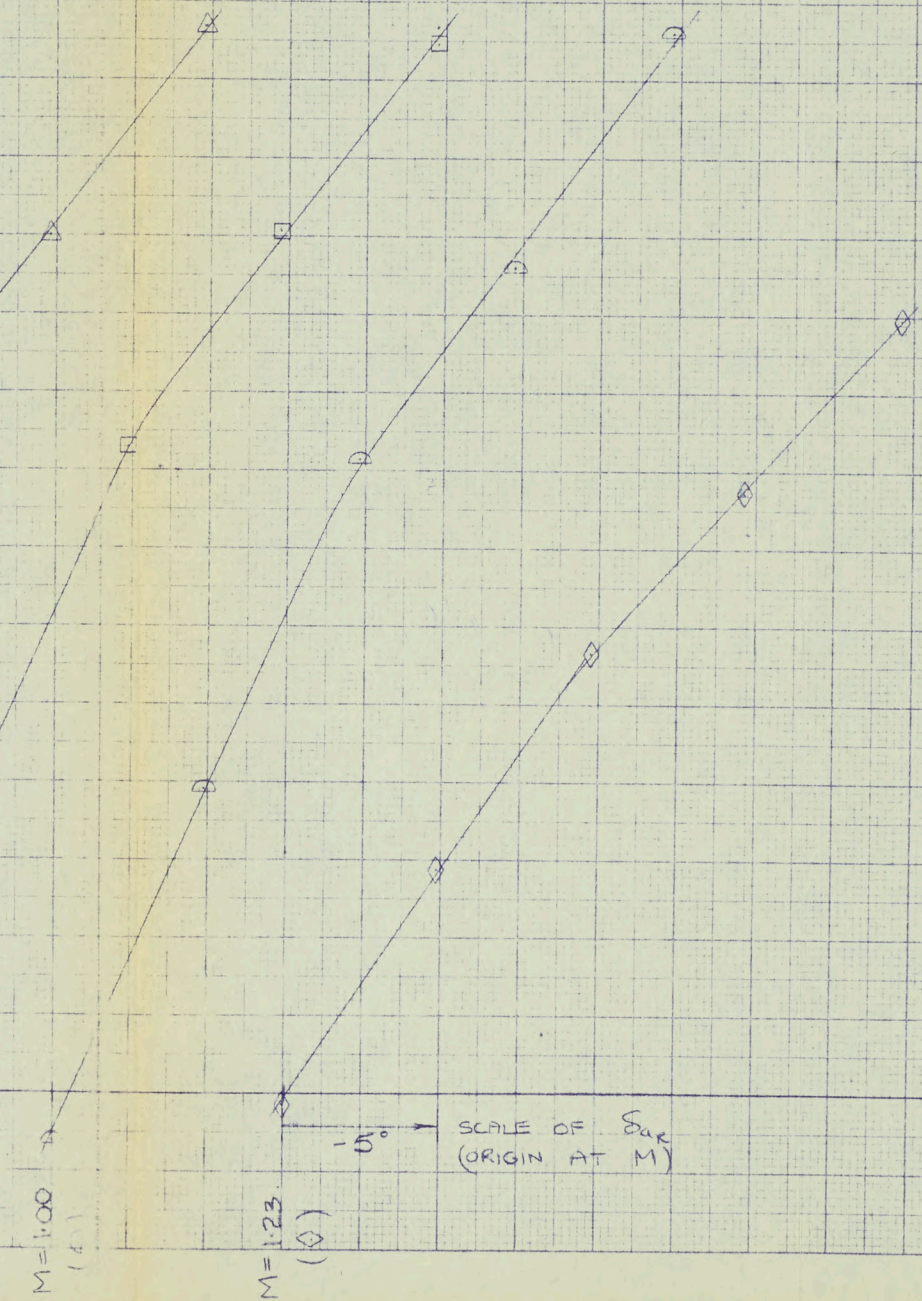
M = .98
(□)

M = 1.00
(△)

M = 1.23
(△)

358-111 KEUFFEL & ESSER CO.
P.O. BOX 1000, ST. LOUIS, MO. 63101
MADE IN U.S.A.





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C-105

CAL WIND TUNNEL TESTS

C_L vs δ_{AR}

($\delta_{AL} = 0^\circ$)

$\alpha = 6^\circ$

C_L

.012

.010

.008

.006

.004

.002

-.002

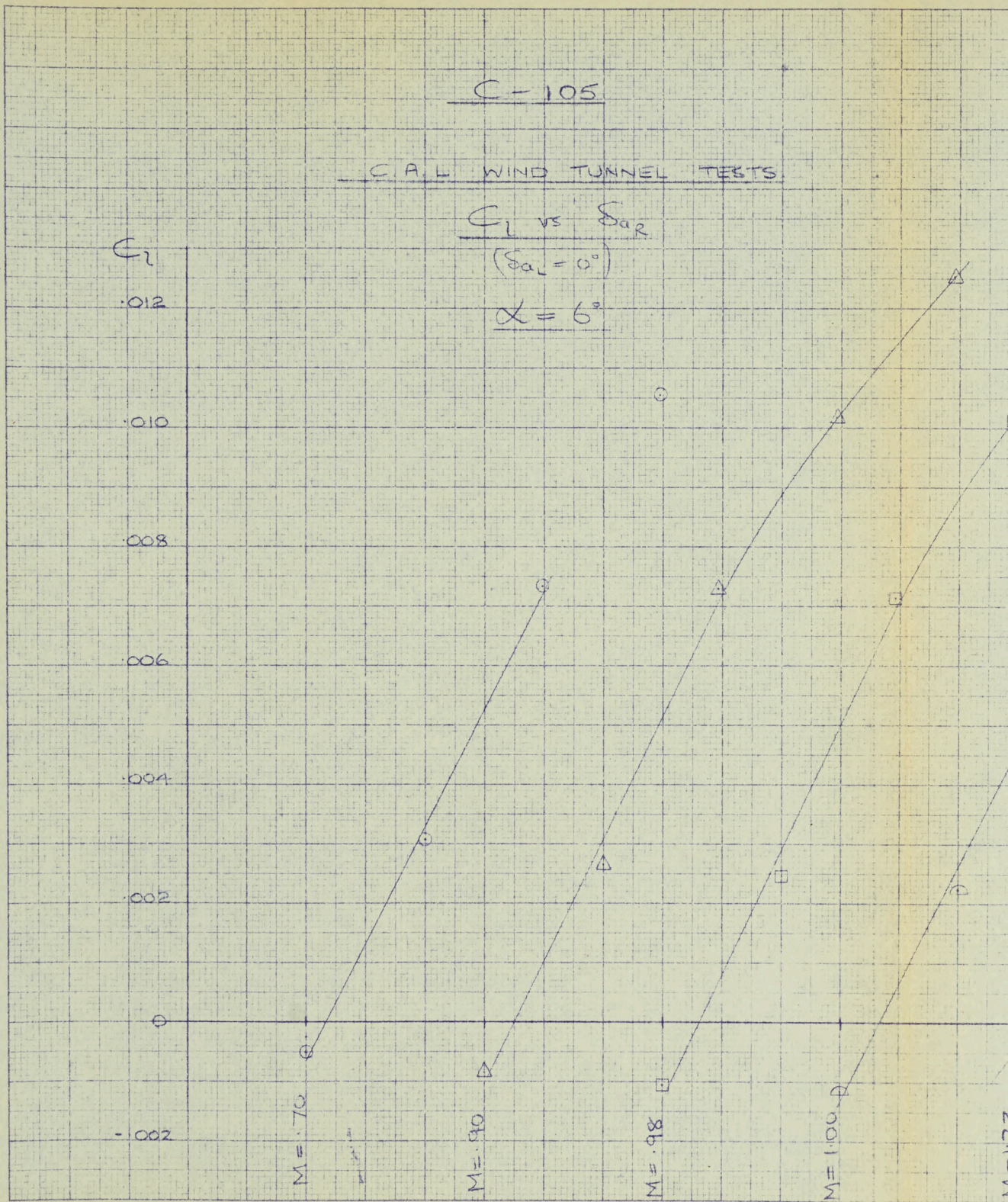
M = .79

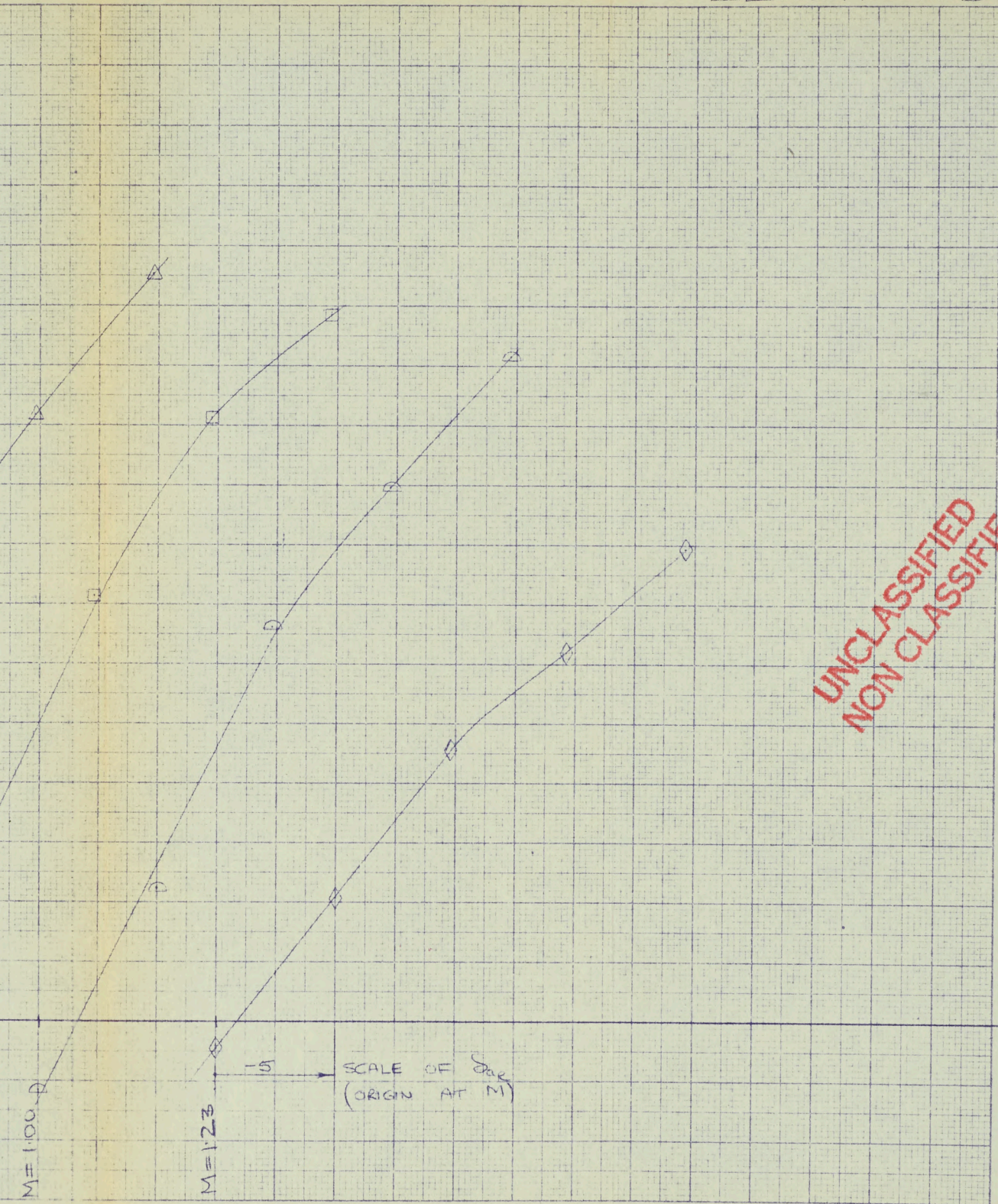
M = .90

M = .98

M = 1.00

450-116 KEUFFEL & ESSER CO.
107-10 Columbia Blvd., 5th Floor, Philadelphia, Pa. 19104

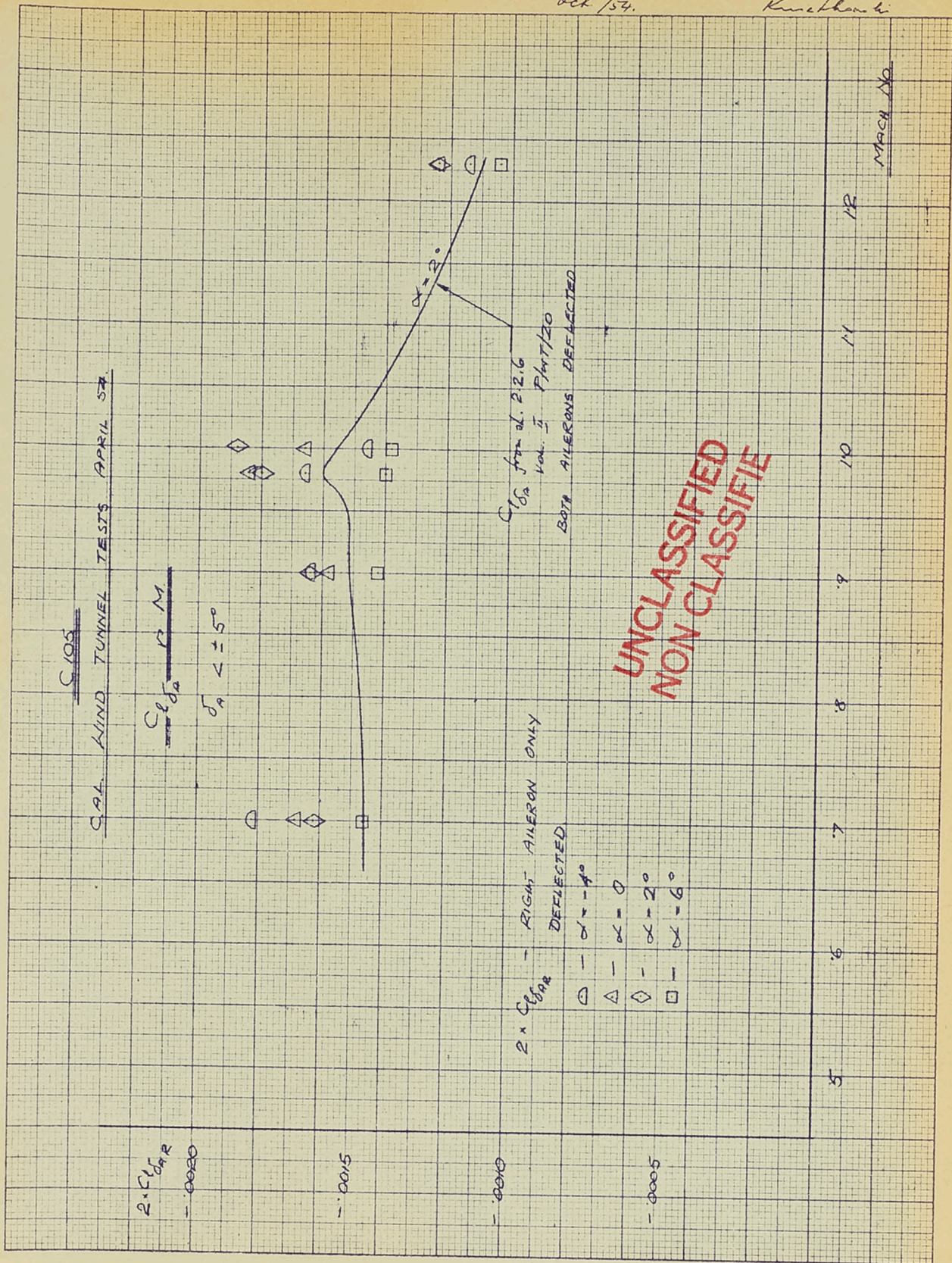




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NON CLASSIFIE

2.1.12.
6ck/54.

P/WT/20 15.
Knechtke



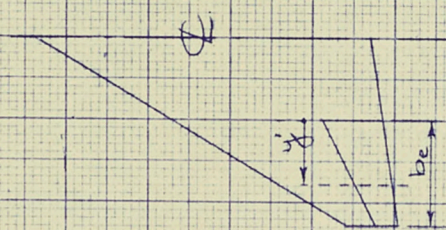
C-105

S.A.L. WIND TUNNEL TESTS
SPANWISE POSITION OF AILERON LOADS
AS FRACTION OF AILERON SPAN

C.P. POSITION
(FRACTION OF
AILERON SPAN
~ FROM
INBOARD END
OF AILERON)

α
-4° 0° 2° 6°

◇ ○ △ □



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0.6
0.5
0.4
0.3
0.2
0.1
0
-0.1
-0.2

0.7 0.8 0.9 1.0 1.1 1.2 1.3 M

C-105

C.A.L. WIND TUNNEL TESTS

C_M

C_M vs δ_{AR}

($\delta_{AL} = 0^\circ$)

$\alpha = -4^\circ$

.08

.07

.06

.05

.04

.03

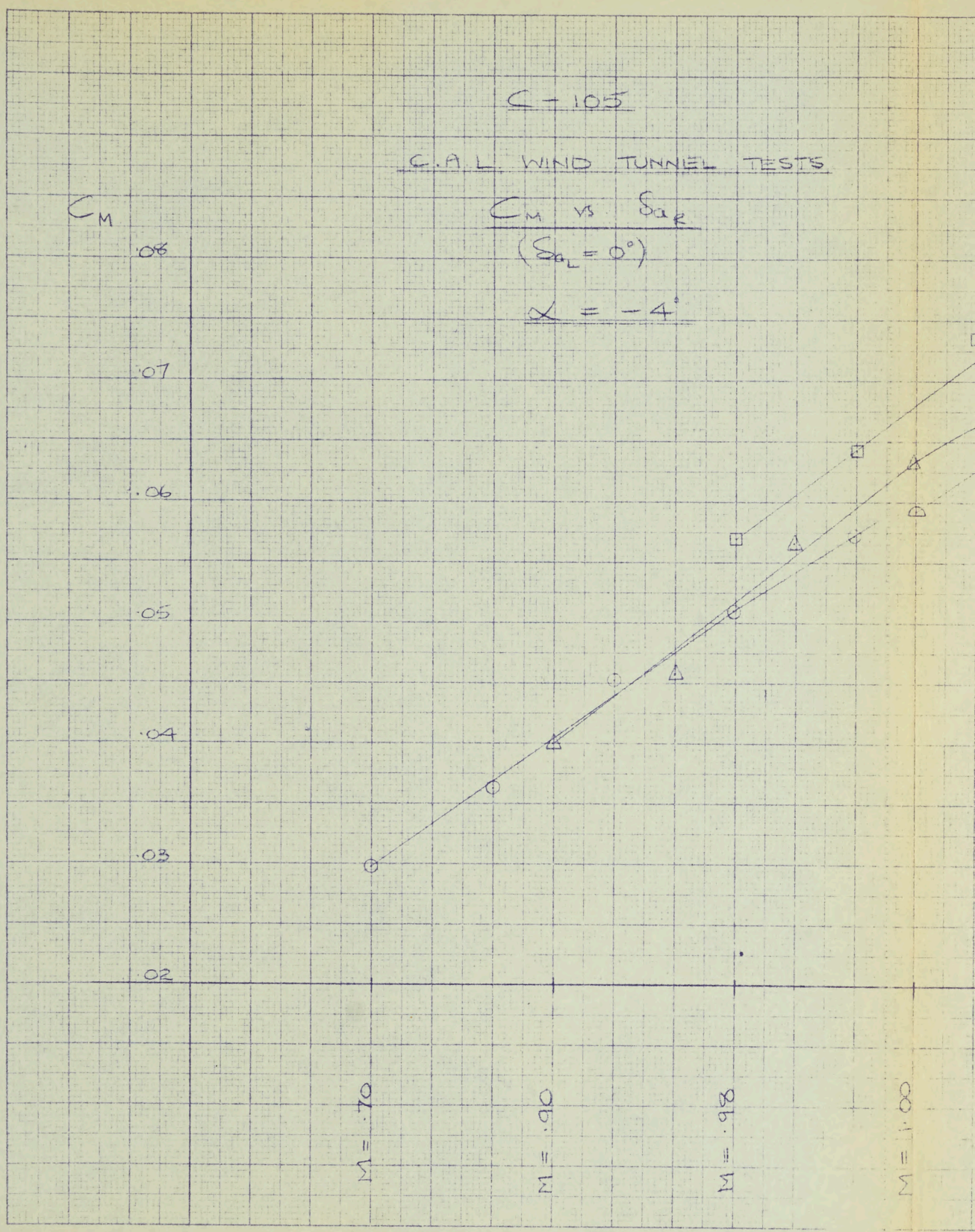
.02

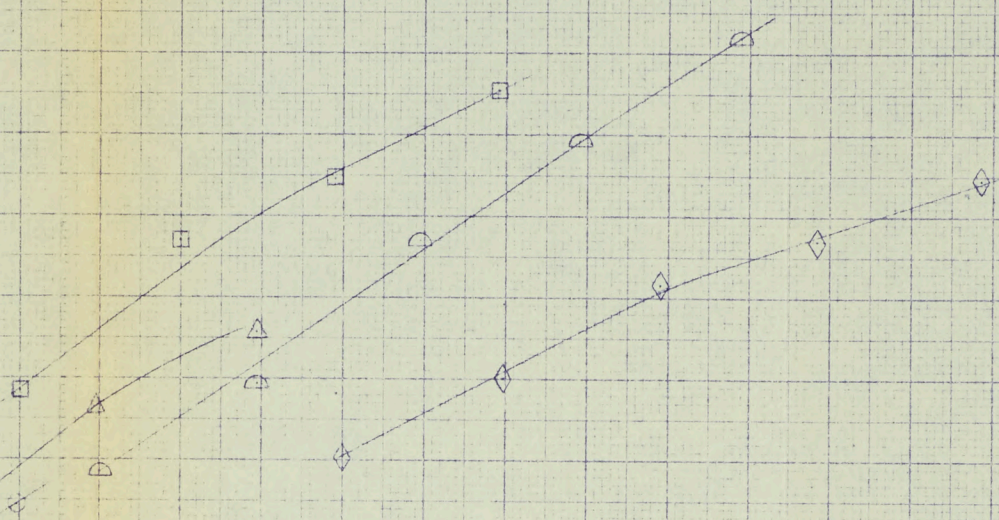
$M = .70$

$M = .90$

$M = .98$

$M = 1.00$





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M = 1.00

M = 1.23

SCALE OF δ_{ar} (ORIGIN AT M)

-5°

C-105

C.A.L. WIND TUNNEL

C_M vs. δ_{air}

$\alpha = 0^\circ$

C_M

.05

.04

.03

.02

.01

0

$M = .70$ ○

$M = .90$ △

$M = .98$ □

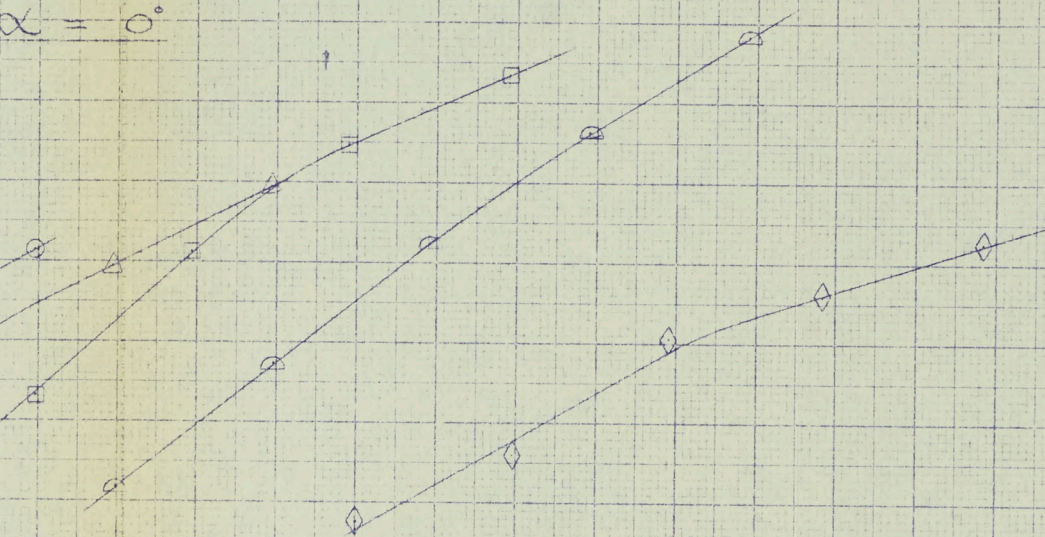
$M = 1.00$ ⊙

105

TUNNEL TESTS.

vs. S_{aR} ($S_{aL} = 0^\circ$)

$\alpha = 0^\circ$



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-5°
SCALE OF S_{aR} (ORIGIN AT M)

M = 1.00

M = 1.23

C-105

C.A.L. WIND TUNNEL

C_M vs. δ_{AR}

$\alpha = 2^\circ$

C_M

.04

.03

.02

.01

$M = .70$ ○

$M = .90$ △

$M = .98$ □

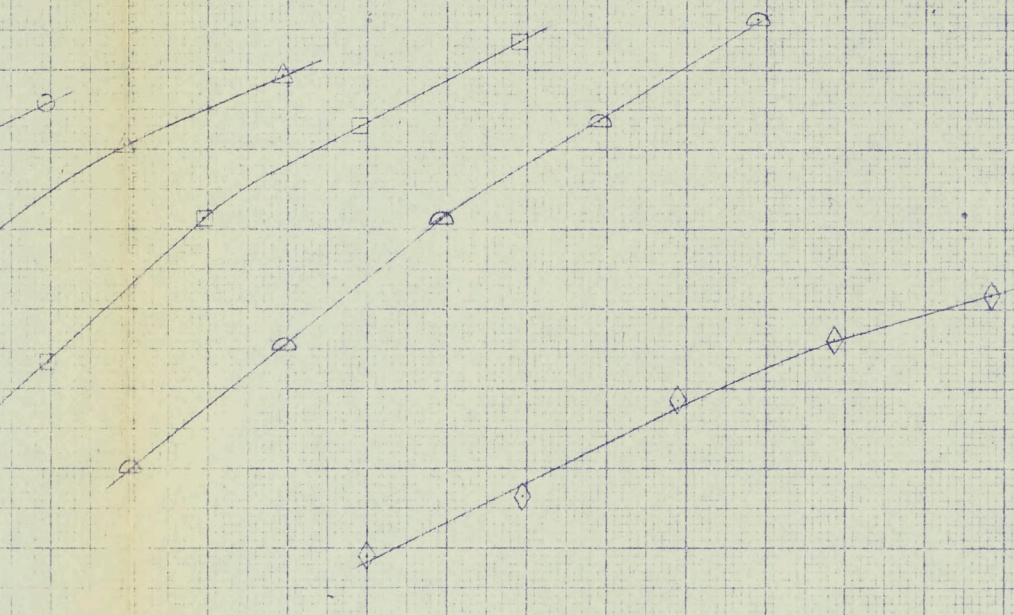
$M = 1.00$ ◇

- 105

TUNNEL TESTS

vs. ϵ_{aR} ($\epsilon_{aL} = 0^\circ$)

$L = 2'$



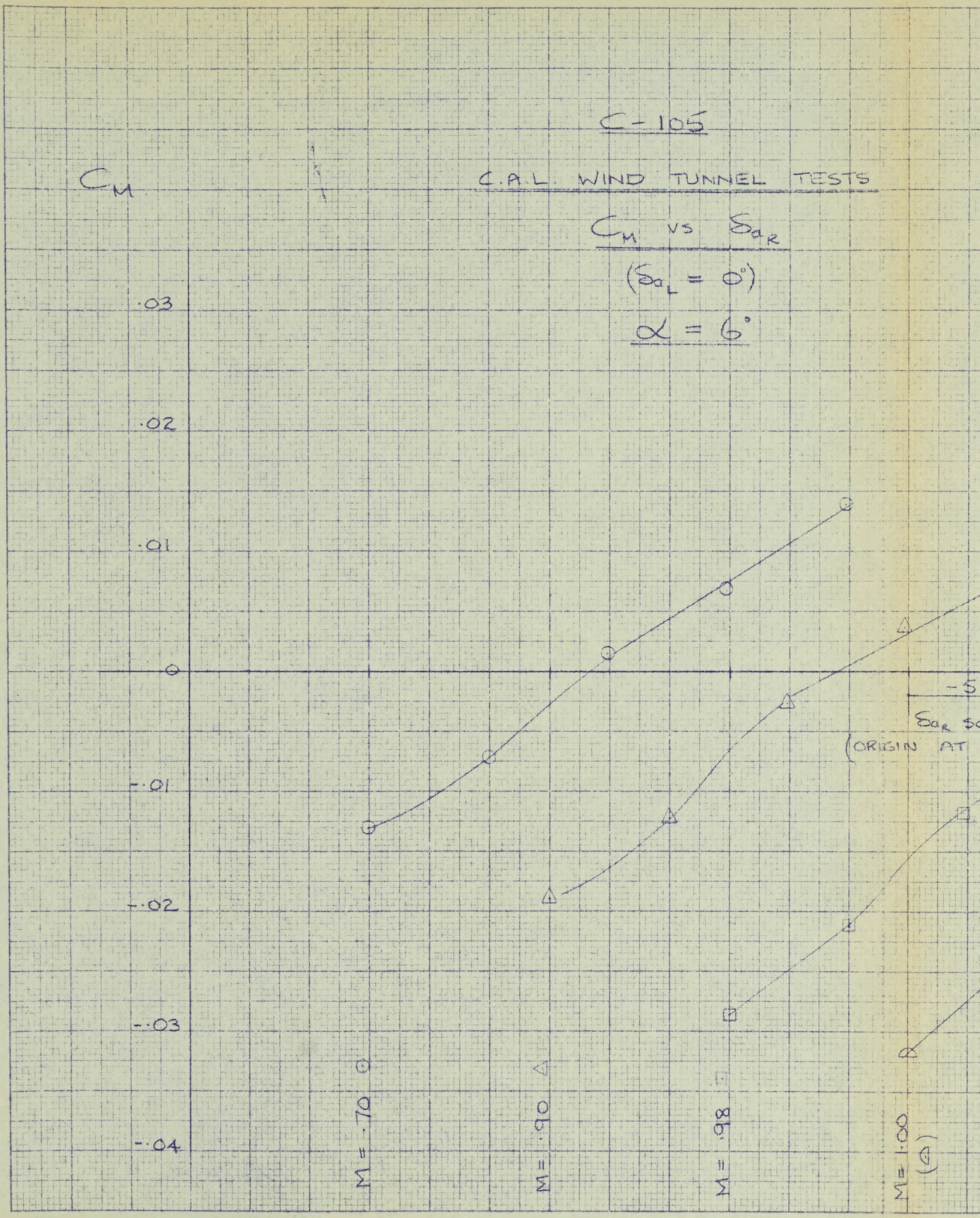
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-5°
SCALE OF ϵ_{aR} (ORIGINS AT M)

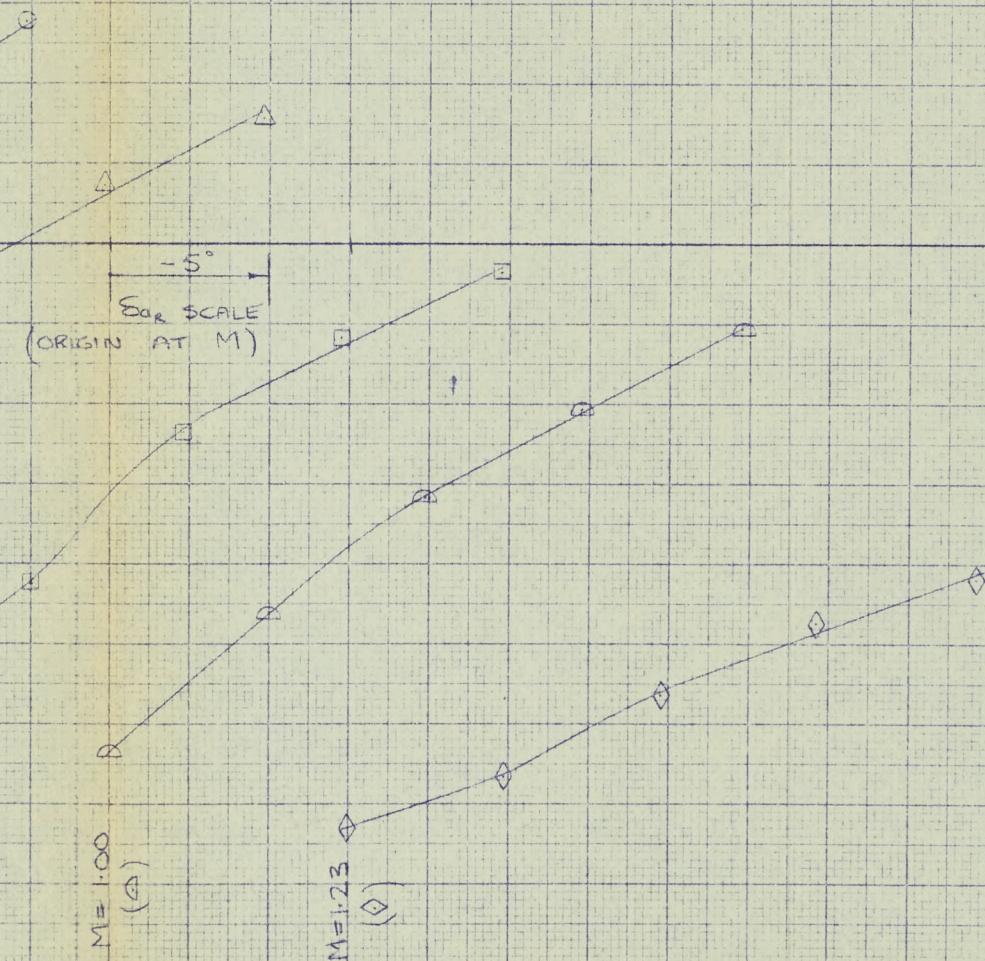
M = 1.00

M = 1.23

350-111 KEUFFEL & ESSER CO.
100 N. 17th St. Philadelphia, Pa. U.S.A.
MADE IN U.S.A.



578



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C105
CAL. A.I.T. TESTS

CM_{drag} vs M
($d_{HL} = 0$)

- $\alpha = -4^\circ$
- △ $\alpha = 0$
- $\alpha = 4^\circ$
- ◇ $\alpha = 6^\circ$

CM_{drag}

0.03

0.02

0.01

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12
MARCH No

11

10

9

8

7

6

5

C-105

C.A.L. WIND TUNNEL TESTS

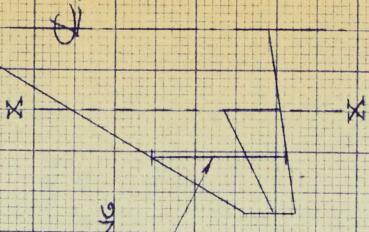
CHORDWISE POSITION OF ALLECON LOADS
AS FRACTION OF M.A.C. OUTER WING

$\alpha = -4^\circ$

C.P. POSITION
(FRACTION M.A.C.
OUTER WING)

1.0
.9
.8
.7
.6
.5
.4
.3

M.A.C. OF WING
OUTBOARD OF
X-X



STARBOARD ALLECON.
AILERON ANGLE $-10^\circ < \delta_{AR} < 0^\circ$
(DEFLECTED DOWN)

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.7 .8 .9 1.0 1.1 1.2 1.3 M

C-105

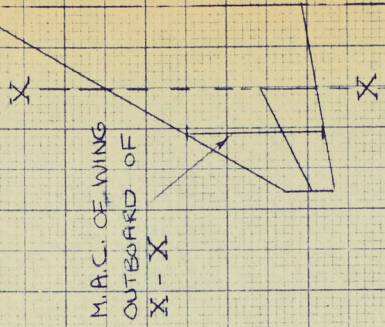
C.A.L. WIND TUNNEL TESTS

CHORDWISE POSITION OF AILERON LOADS
AS FRACTION OF M.A.C. OUTER WING

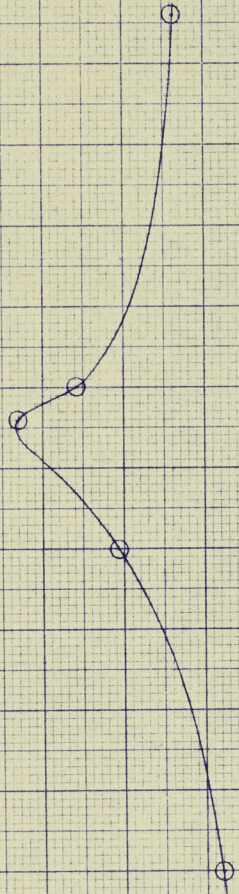
$\alpha = 0^\circ$

C.P. POSITION:
(FRACTION MAC
OUTER WING)

1.0
.9
.8
.7
.6
.5
.4
.3



STARBOARD AILERON
AILERON ANGLE $-10^\circ < \delta_{AK} < 0^\circ$



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7 .8 .9 10 11 12 13 M

C-105

C.A.L. WIND TUNNEL TESTS

CHORDWISE POSITION OF AILERON LOAD

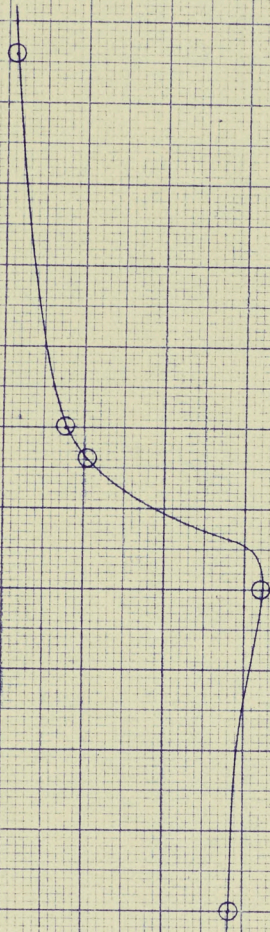
AS FRACTION OF M.A.C. OUTER WING

$\alpha = 2^\circ$

C.P. POSITION
(FRACTION M.A.C.
OUTER WING)

1.0
.9
.8
.7
.6
.5
.4
.3

M.A.C. OF WING
OUTBOARD OF
X-X



STARBOARD AILERON
AILERON RANGE $-10^\circ < \delta_{AR} < 0^\circ$

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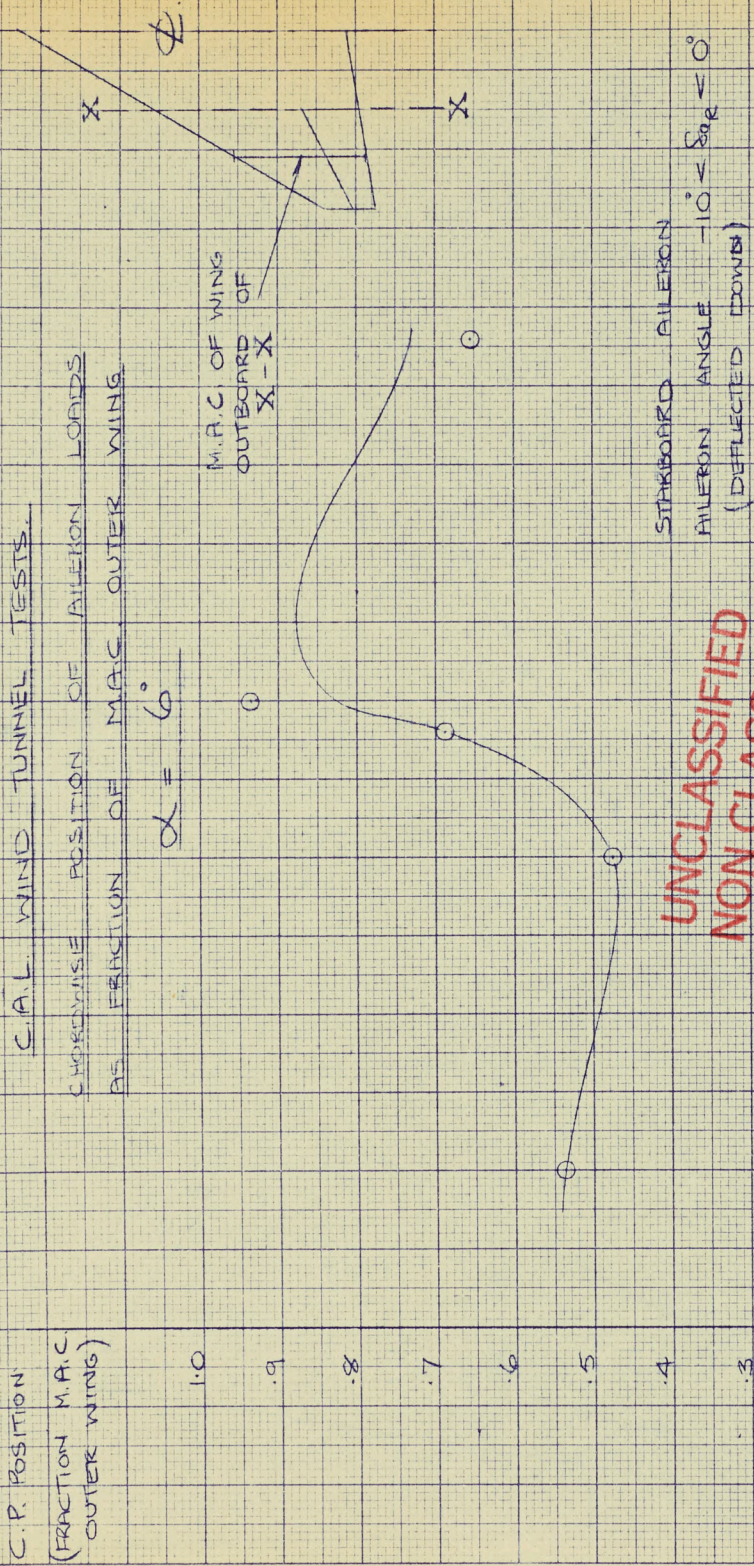
C-105

C.A.L. WIND TUNNEL TESTS.

CHORDWISE POSITION OF AILERON LOADS
AS FRACTION OF MAC OUTER WING

$\alpha = 6^\circ$

M.A.C. OF WING
OUTBOARD OF
X-X



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STARBOARD AILERON
AILERON ANGLE $-10^\circ < \delta_{air} < 0^\circ$
(DEFLECTED DOWN)

0.7 0.8 0.9 1.0 1.1 1.2 1.3 M

C-105

C.A.L. WIND TUNNEL TESTS

AILERON LOAD POSITION

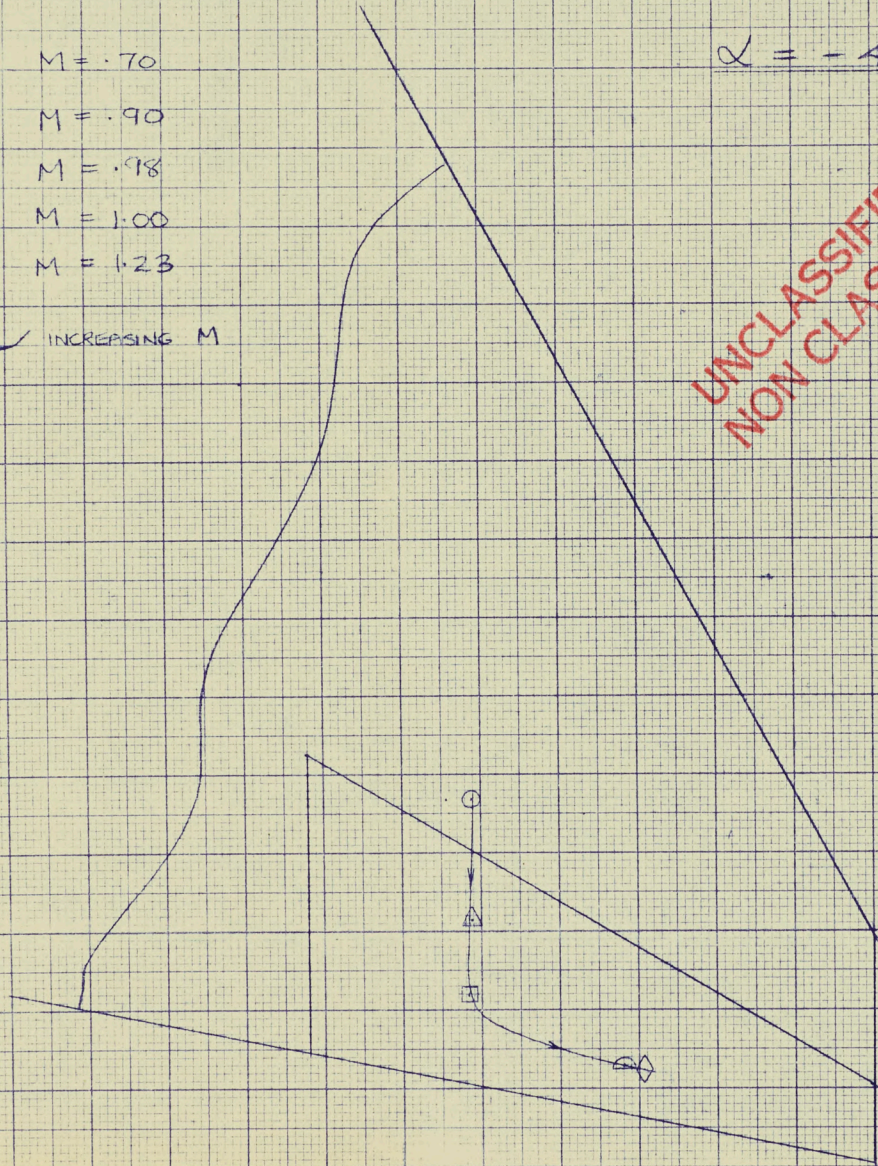
$(-10^\circ < \delta_{AR} < 0^\circ)$

$\alpha = -4^\circ$

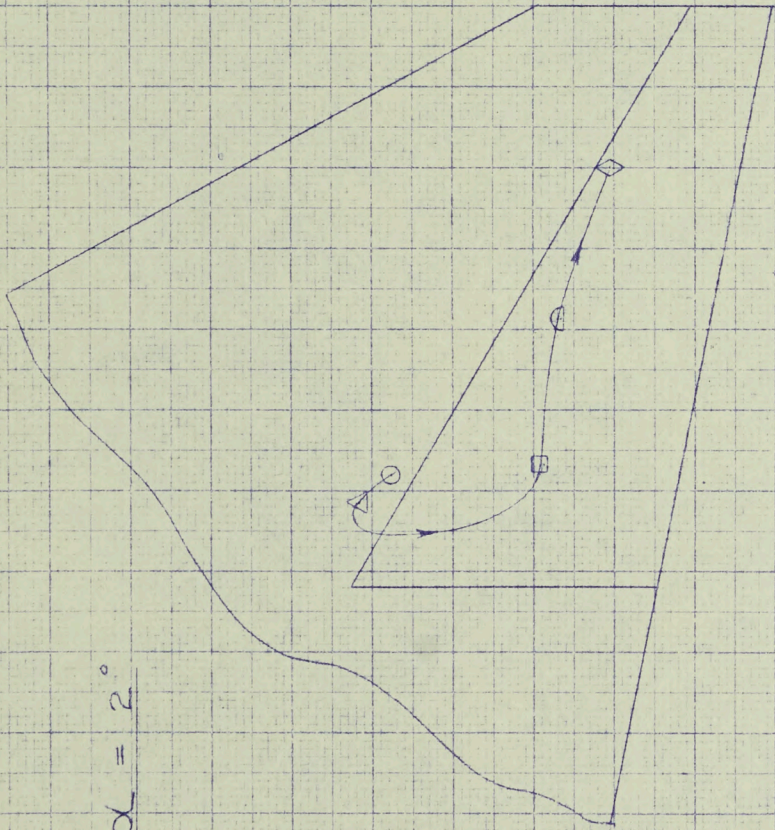
- M = .70
- △ M = .90
- M = .98
- ◇ M = 1.00
- ◇ M = 1.23

↘ INCREASING M

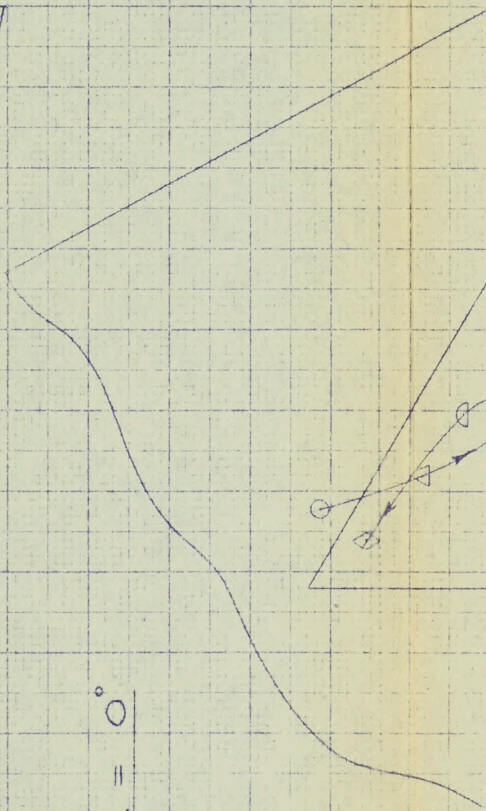
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$\alpha = 2^\circ$



$\alpha = 0^\circ$



C-105

C.A.L. WIND TUNNEL TESTS

PIVOTON LOAD POSITION

$(-10^\circ \leq \delta_{\alpha R} \leq 0^\circ)$

M = .70 ○

M = .90 △

M = .98 □

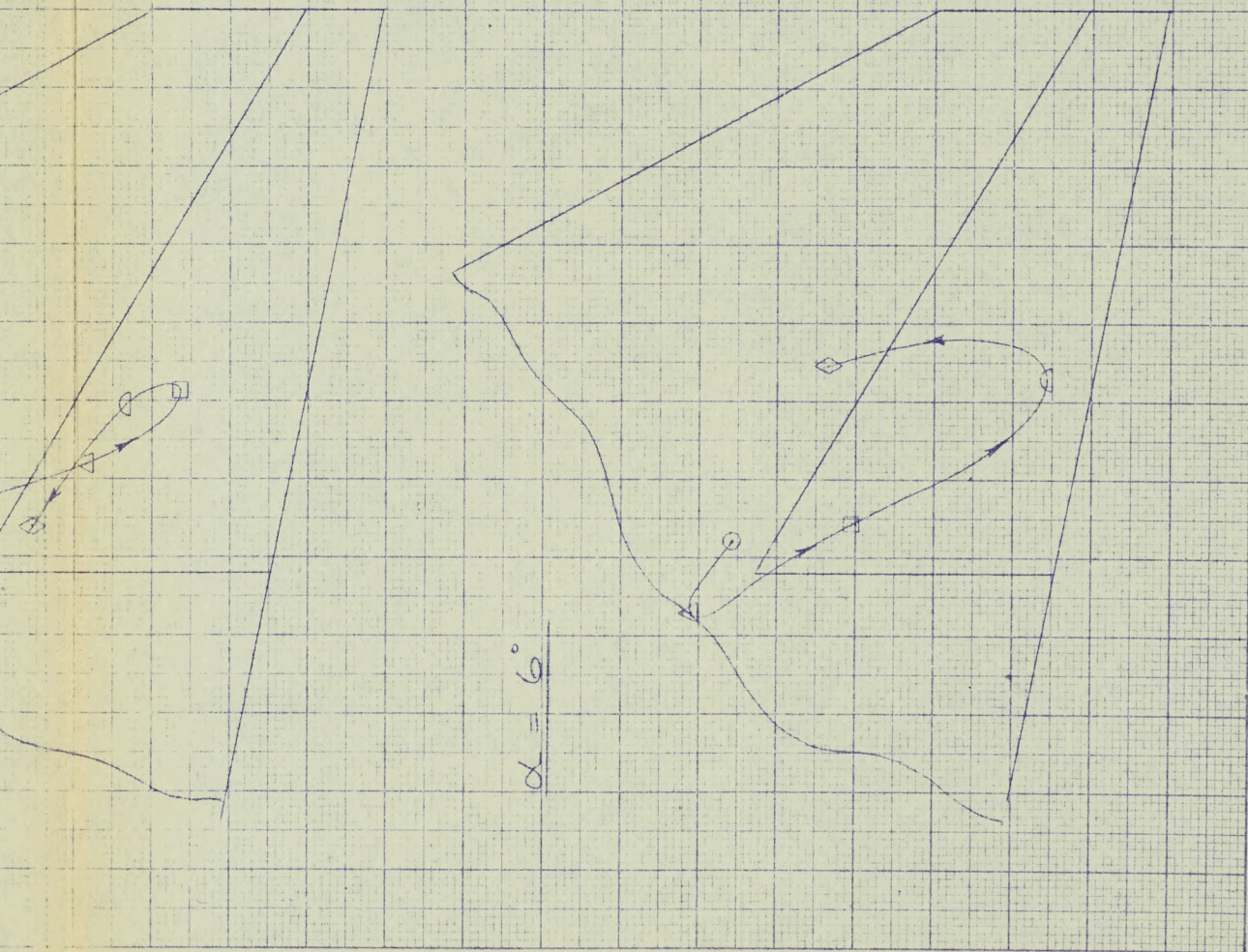
M = 1.00 ◇

M = 1.23 ◇

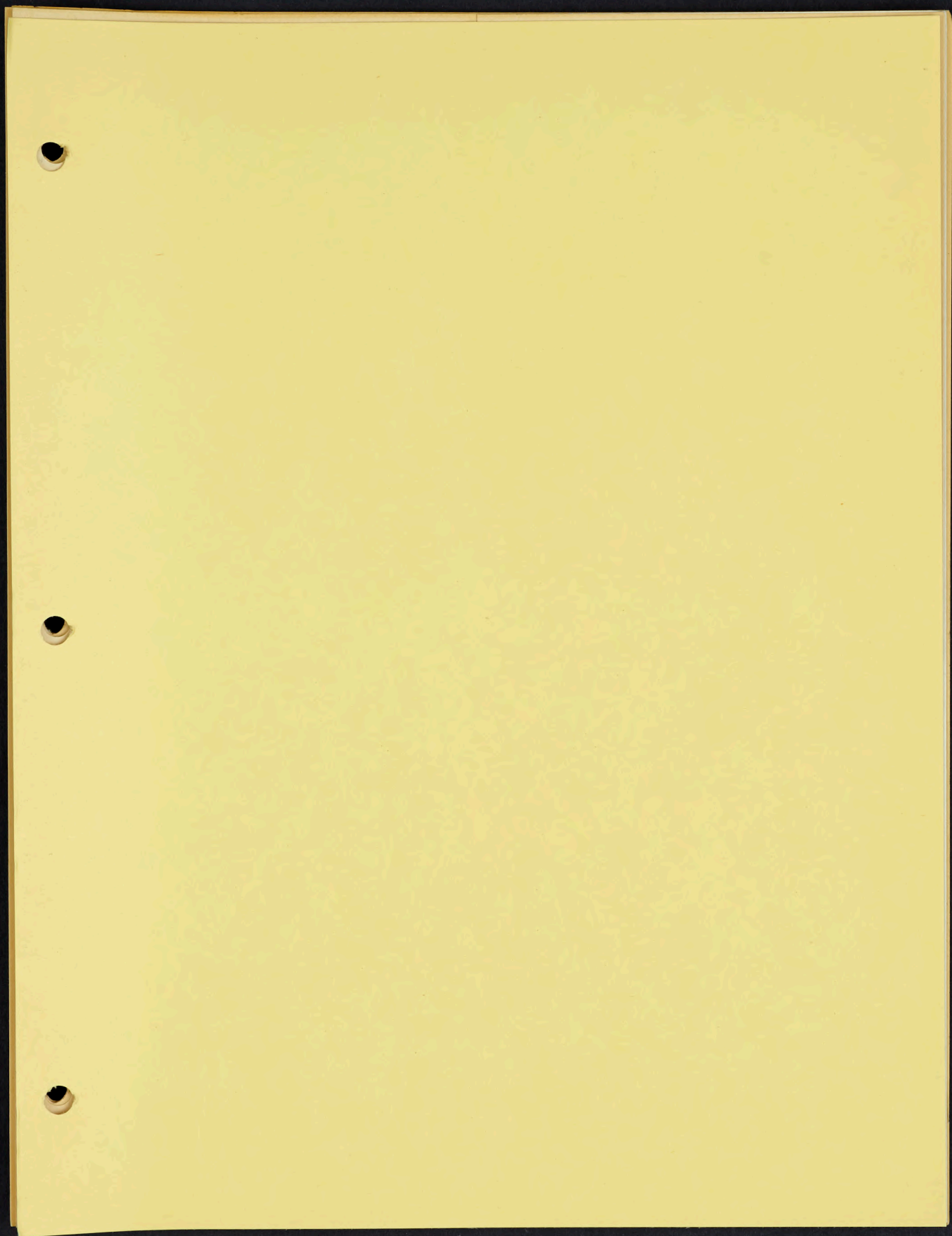
M = 1.00 @

M = 1.23 @

INCREASING M



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C-105 C.A.L. W-T Tests

Deflection of Loaded Controls

Surface	δ°	$\frac{+HM}{G}$	$\frac{G\Delta\delta}{HM}$	δ°	$\frac{G\Delta\delta}{HM}$	$\frac{-HM}{G}$	$\frac{G\Delta\delta}{HM}$
---------	----------------	-----------------	----------------------------	----------------	----------------------------	-----------------	----------------------------

$$\Delta\delta^\circ = \frac{HM}{G} \times \frac{G\Delta\delta}{HM}$$

Aileron	0	.00633	-.00527	0	.00479		.00428
-(R.H.)	+5	—	-.00469	-5	-.00472		-.00428
+(L.H.)	+10	—	.00383	-10	.00304		.00574
	+15	—	-.00602	-15	-.00428		-.00414
	+20	—	-.00428	-20	.00369		-.00434

Flevator	-30	.00502	—				
(L.H.)	-20	.00461	—				
	-10	.00469	—				
	-5	.00576	.00494				
	0	.00510	.00535				
	+10	—	.00518				

$\frac{+HM}{G}$ 300

Rudder	0	.00430	-.00495				
	+5	.00499	-.00438				
	+10	—	.00731				
	+20	—	.00430				

250

M=1.23
M=1.15
M=1.10
M=1.05

M=1.00

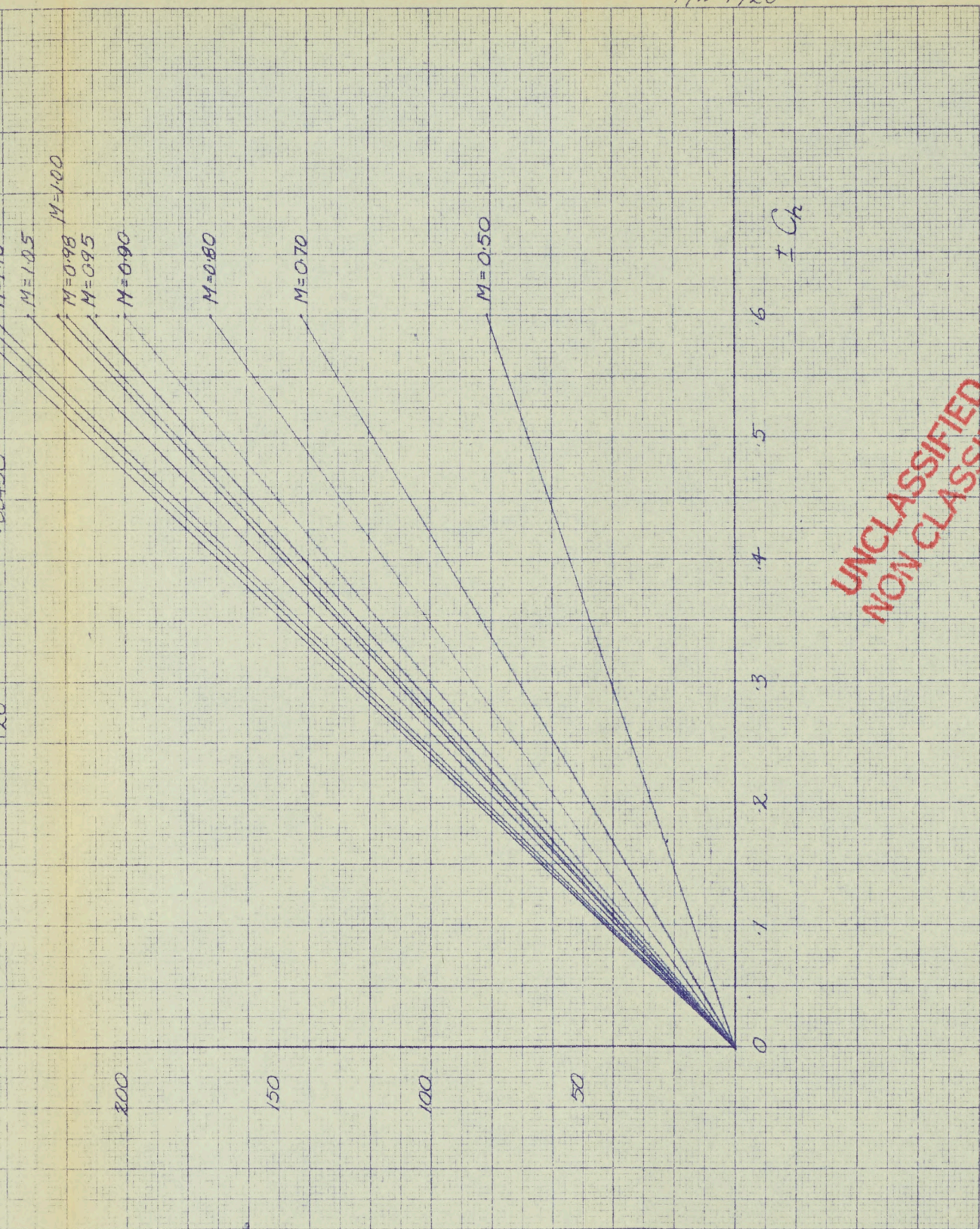
M=0.98
M=0.95

M=0.90

300

C.A Ford.
P/W-T/20

3.1.5.



359-12 KEUFFEL & ESSER CO.
10 x 10 to the 1" (both sides) grid
MADE IN U. S. A.

C-105
C.A.L. W-T Tests
C_{mp} 15 M
 $\alpha = -2^\circ$

C_{mp}
per
degree

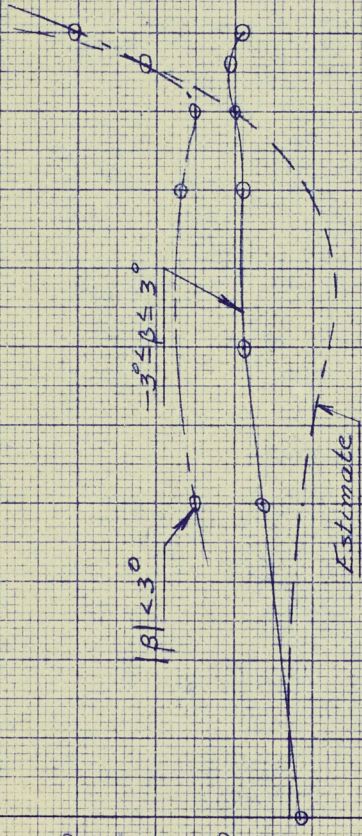
.0080

.0060

.0040

.0020

0



UNCLASSIFIED
NON CLASSIFIE

Mach No.

1.2

1.1

1.0

.9

.8

.7

.6

359-12 KEUFFEL & ESSER CO.
107 1/2 Third Ave., New York 10003, N.Y.

C-105

C.A.L. W-T Tests

Chp 15 M

$\alpha = 0^\circ$

Chp
per degree.

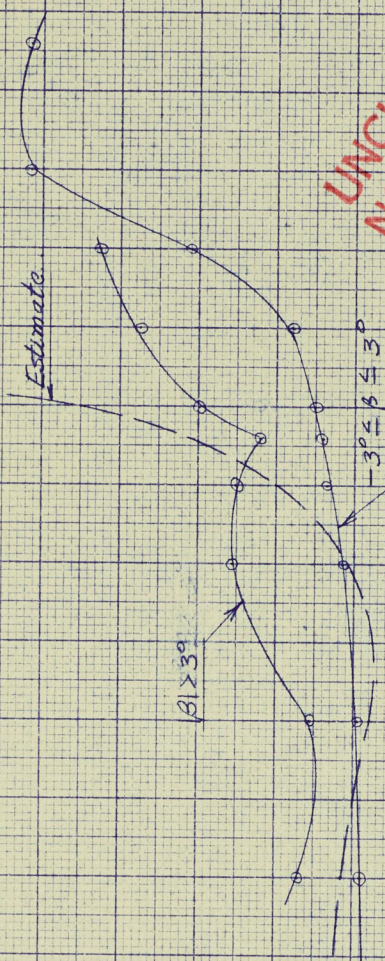
.0080

.0060

.0040

.0020

0



UNCLASSIFIED
NON CLASSIFIED

Mach Number

1.2

1.1

1.0

.9

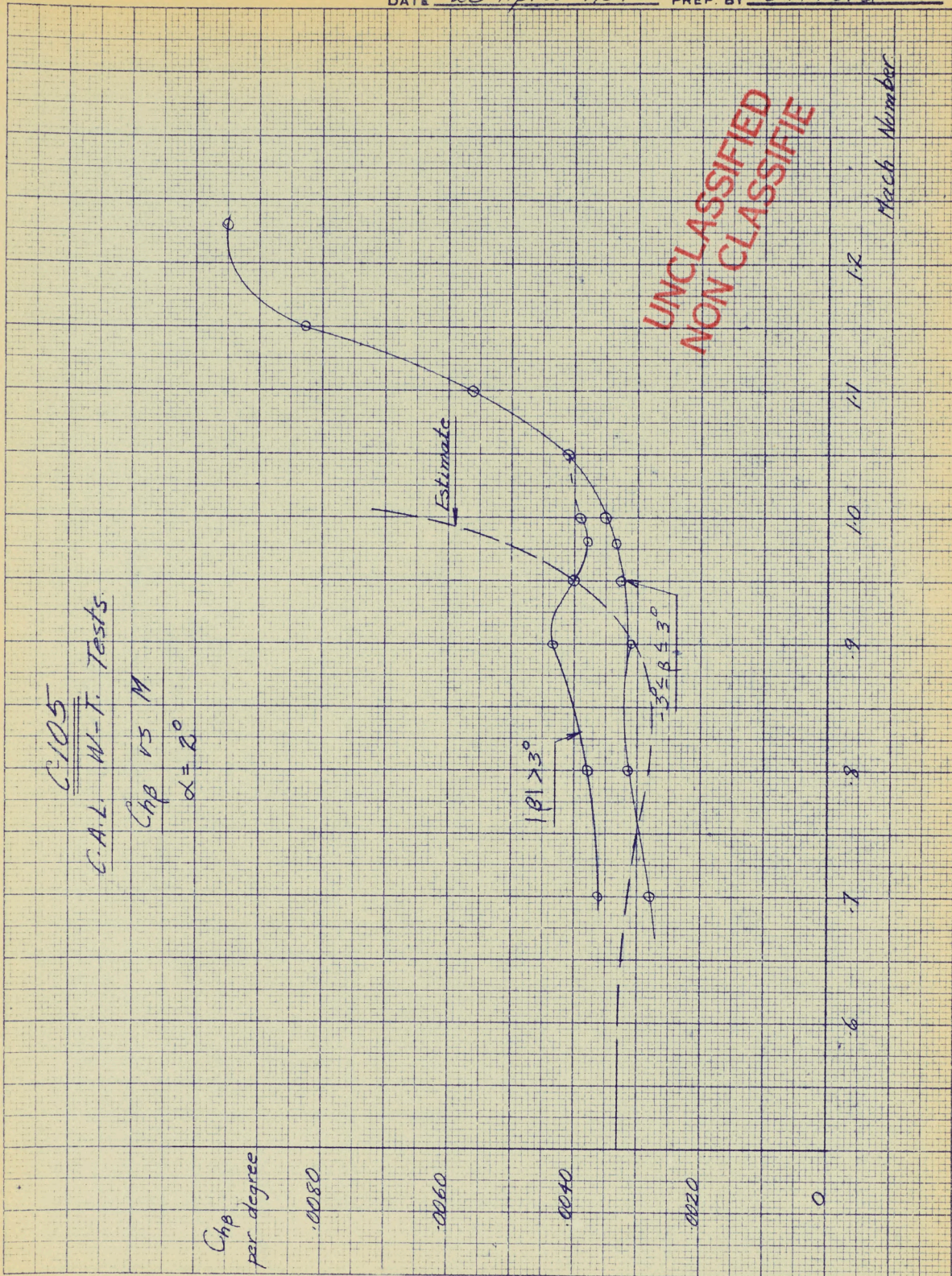
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356-12 KROFFEL & ESSER CO.
1000 North 10th Street, Minneapolis, Minnesota
BASE No. 1

C-105
C.A.L. M-T. Tests
Chp 15 M.
 $\alpha = 0^\circ$



UNCLASSIFIED
NON CLASSIFIE

March Number

12

11

10

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359-12 KEUFFEL & ESSER CO.
10 x 10 in (254 x 254 mm) film mounted.
MAY 1954

C-105
G.A.L. W.T. Tests
Gap 15 M
 $\alpha = 6^\circ$

Chp
per degree

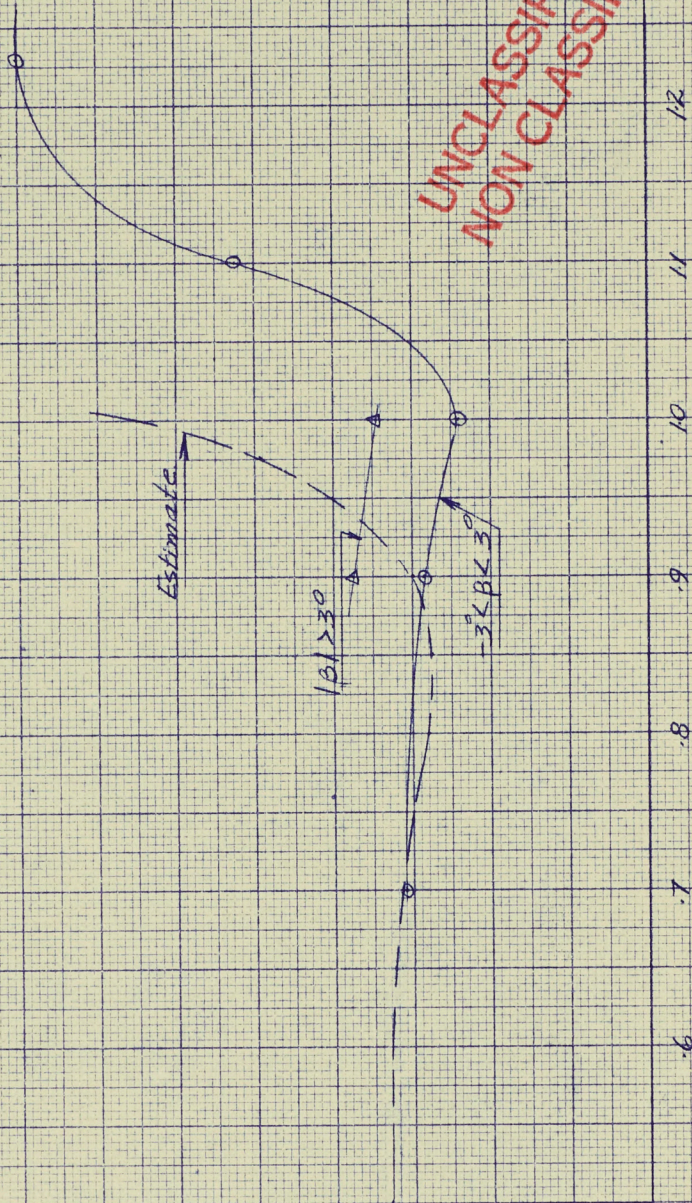
.0080

.0060

.0040

.0020

0



UNCLASSIFIED
NON CLASSIFIE

Mach Number

1.2

1.1

1.0

.9

.8

.7

.6

359-12 KEUFFEL & ESSLER CO.
10 x 10 to 1/2 inch grid lines measured.
MADE IN U.S.A.

C-105

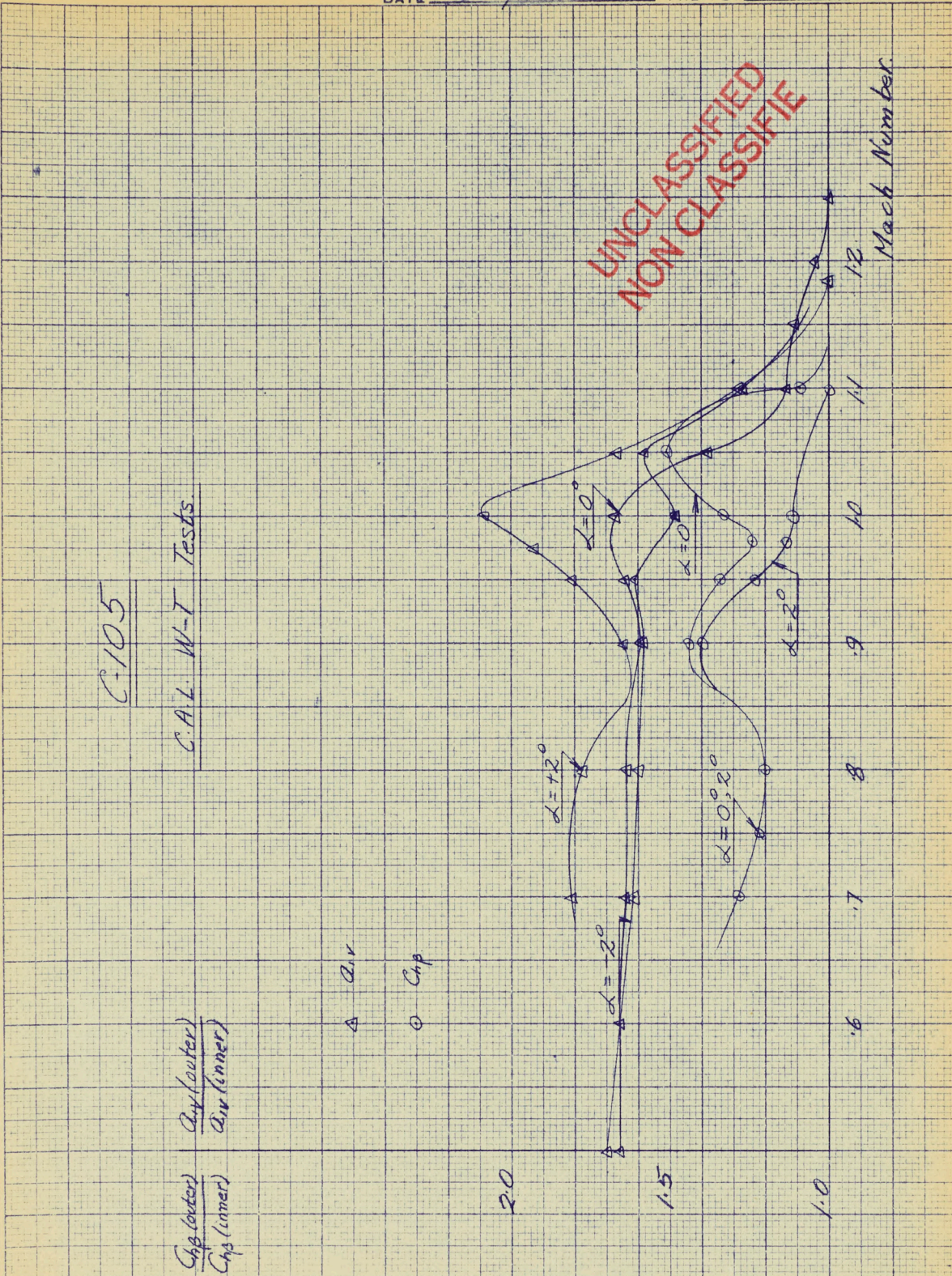
C.A.L. W-T Tests.

Sp (outer)
Cp (inner)

Q_w (outer)
Q_w (inner)

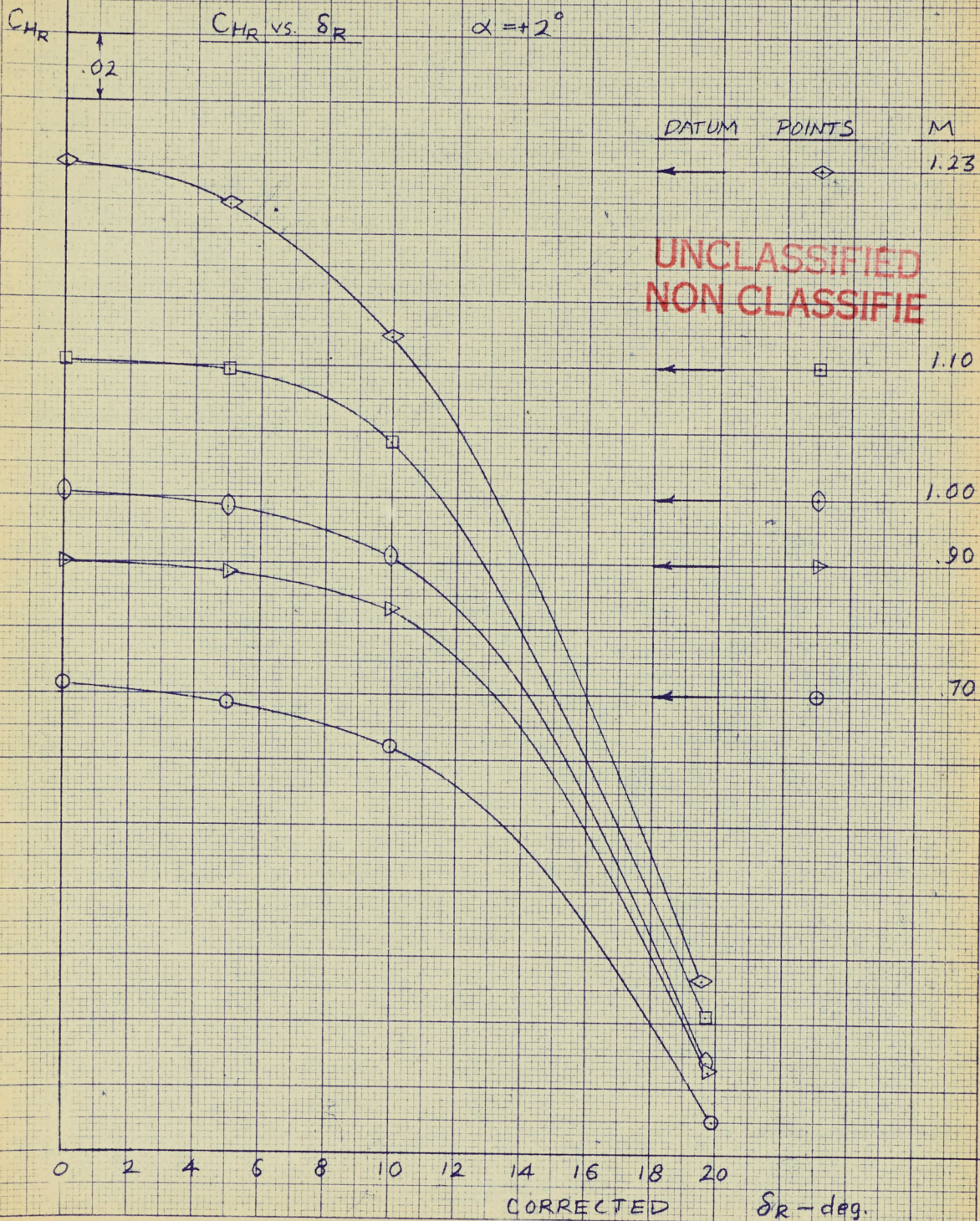
△ Q_w

○ Cp



Mach Number.

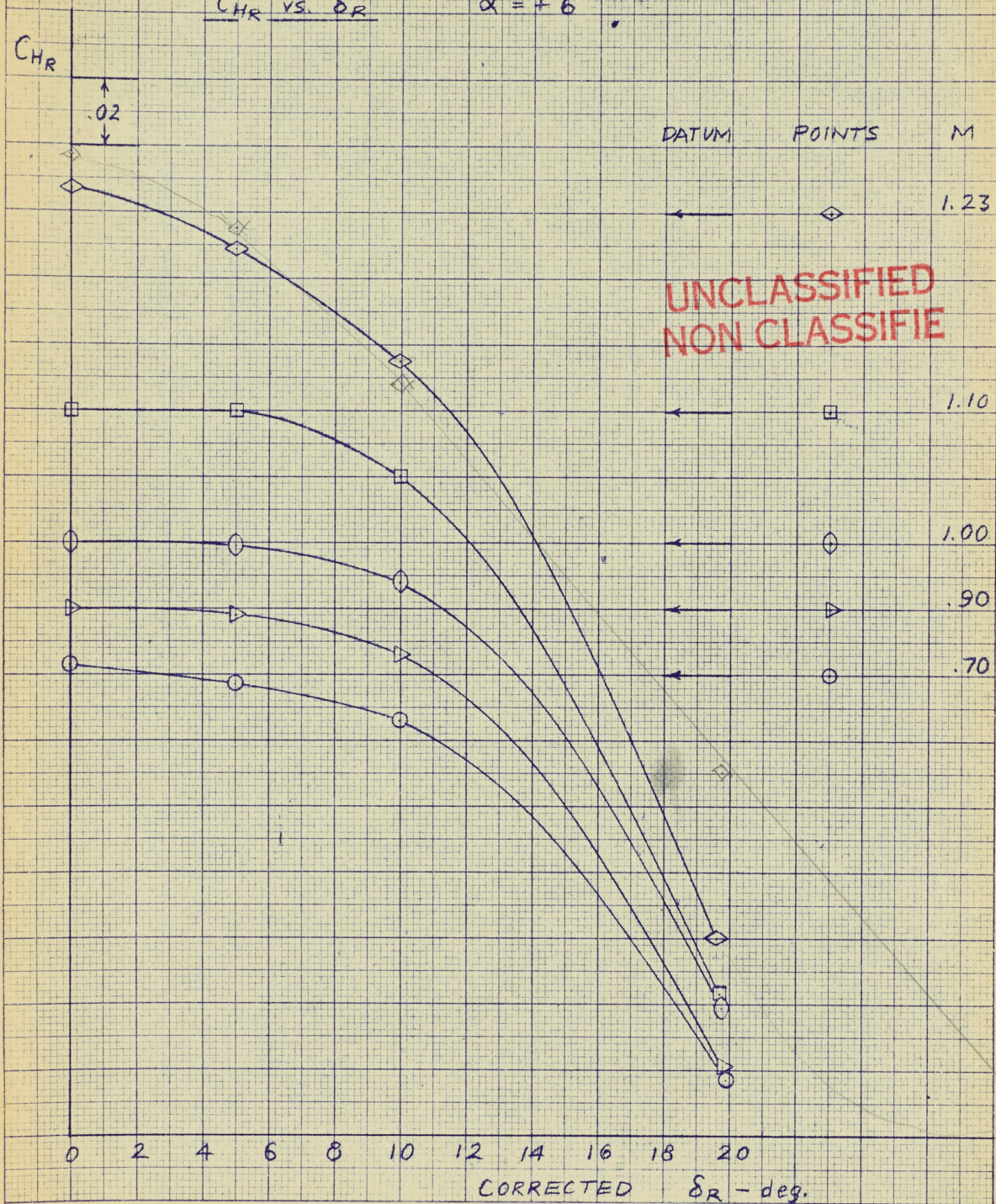
C105 - C.A.L. WIND TUNNEL TESTS APRIL 1954



C105 C.A.L. WIND TUNNEL TESTS APRIL 1954

C_{HR} vs. δ_R

$\alpha = +6^\circ$



C-105

C.A.L. W-T Tests (April 1954)

Ch_{Dr} 15 Mach Number

$10^\circ \leq \delta r \leq 20^\circ$

$\delta c = \delta a = 0$
 $\beta = 0$

Configuration B₁ C₁ B₂

Ch_{Dr}
per deg.

$\alpha = 20^\circ$

$\alpha = 6^\circ$

-03

-02

-01

0

0.5

0.6

0.7

0.8

0.9

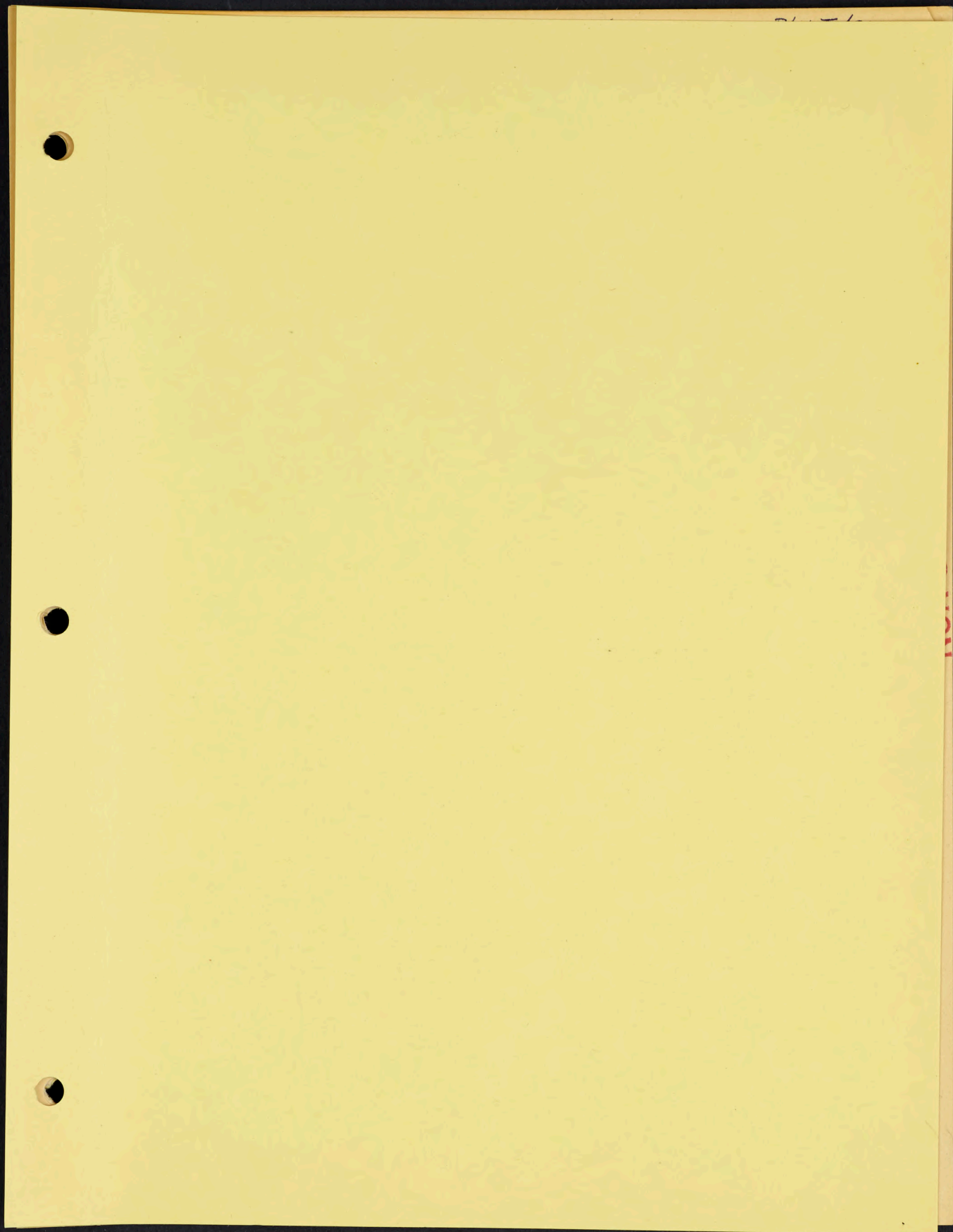
1.0

1.1

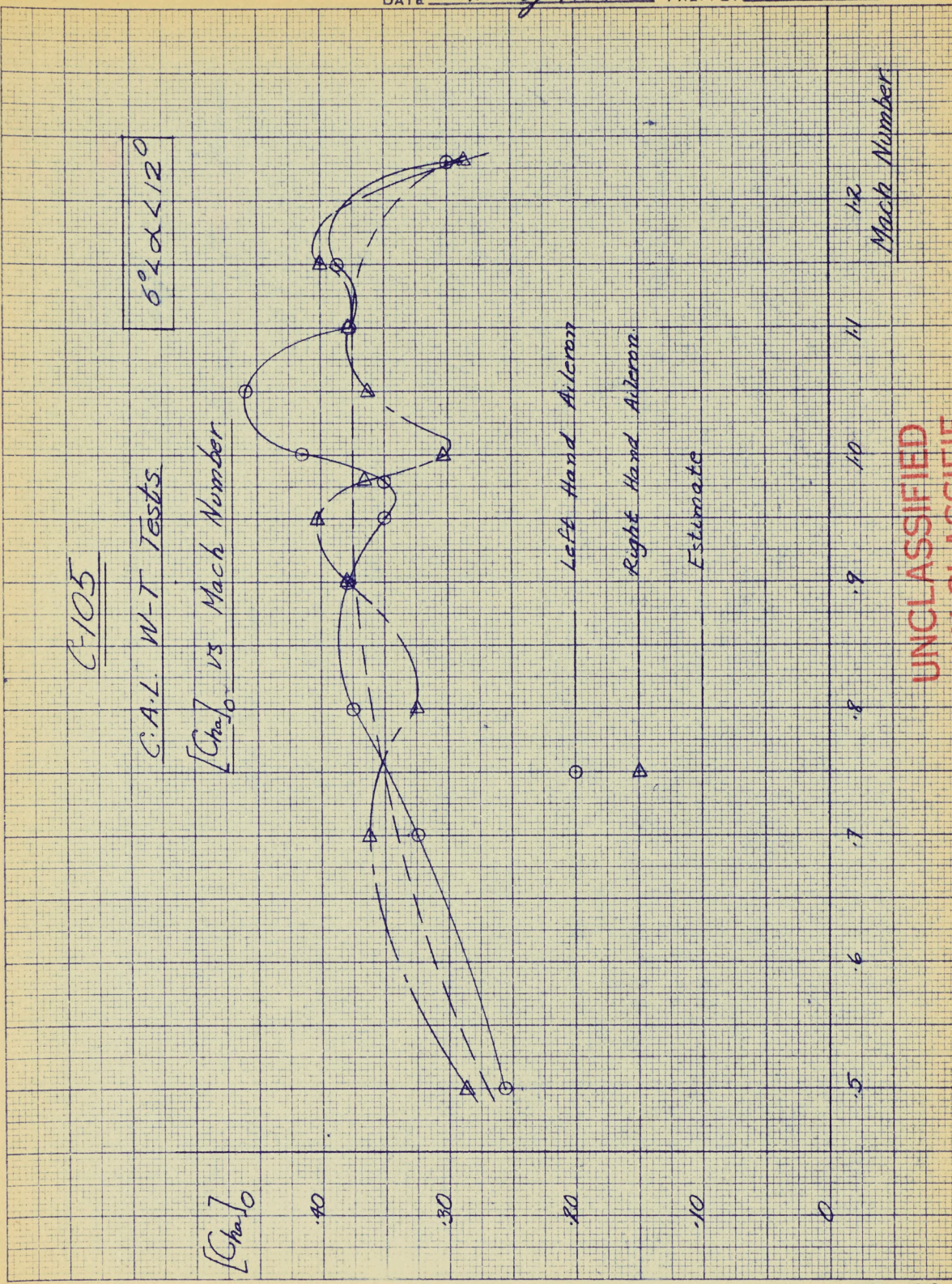
1.2

Mach Number

UNCLASSIFIED
NON CLASSIFIED



359-12 KEUFFEL & ESSER CO.
10 x 10 (to 100) 1/2 inch (50) lines per inch
MADE IN U.S.A.



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NON CLASSIFIE

C-105

C.A.L. W-T Tests

[Char] vs Mach Number

-5° α $\leq 6^\circ$

Right Hand Aileron

Left Hand Aileron

Estimate for Either Aileron

[Char]

0.10

0.05

0

-0.05

0.5

0.6

0.7

0.8

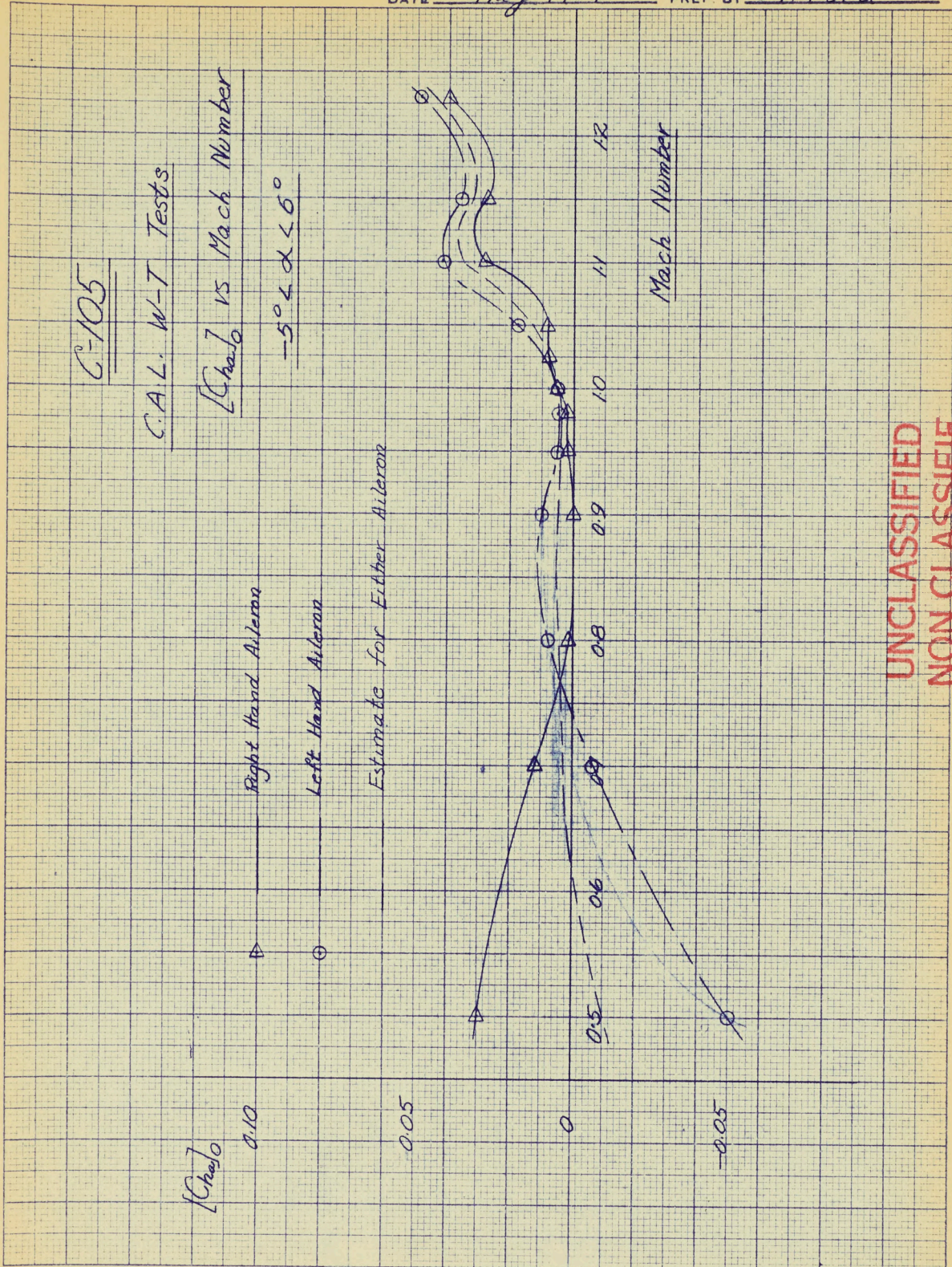
0.9

1.0

1.1

1.2

Mach Number



UNCLASSIFIED
NON CLASSIFIE

356-12 KEUFFEL & ESSER CO.
10 x 10 to the 1/2 inch, 20 lines per inch.
MADE IN U.S.A.

350-12 KEUFFEL & ESSER CO.
111 - 11th Street, Philadelphia, Pennsylvania
MADE IN U.S.A.

C-105

C.A.L. W-T Tests

Chox vs Mach Number

62° α 12°

Chox
per degree

-.06

-.04

-.02

0

New Estimate ~ either aileron.

Left Aileron

Right Aileron

Estimate $P(\text{control})/46$
($\alpha=0$)

Mach Number

11

10

.9

.8

.7

.6

.5

UNCLASSIFIED
NON CLASSIFIED

C-105

CAL. W-T Tests

Chord vs Mach Number

-5° L & +6°

Chord
per degree

0.0200

-0.0100

0

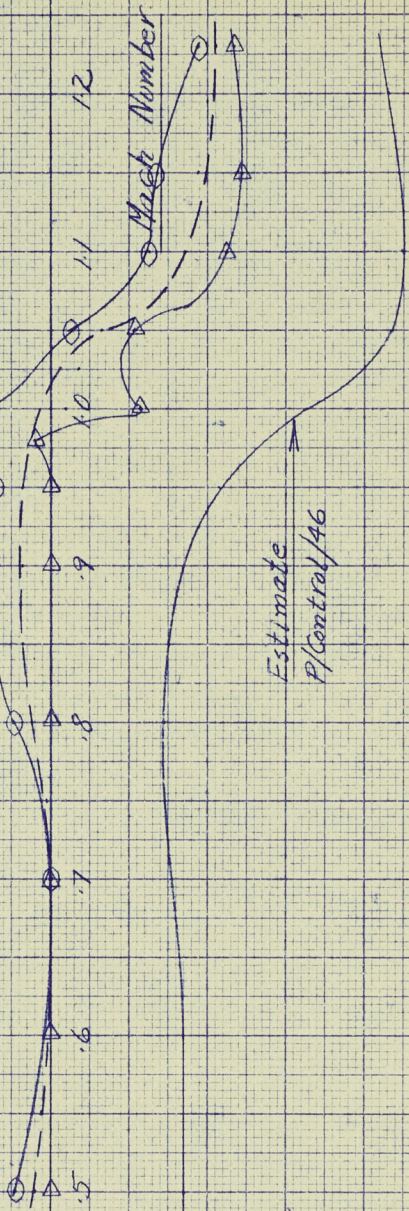
-0.0100

-0.0200

⊕ Left Aileron

▷ Right Aileron

Estimate -
Either Aileron



Estimate
P/Control/46

UNCLASSIFIED
NON CLASSIFIE

C-105

C.A.L. W-T Tests

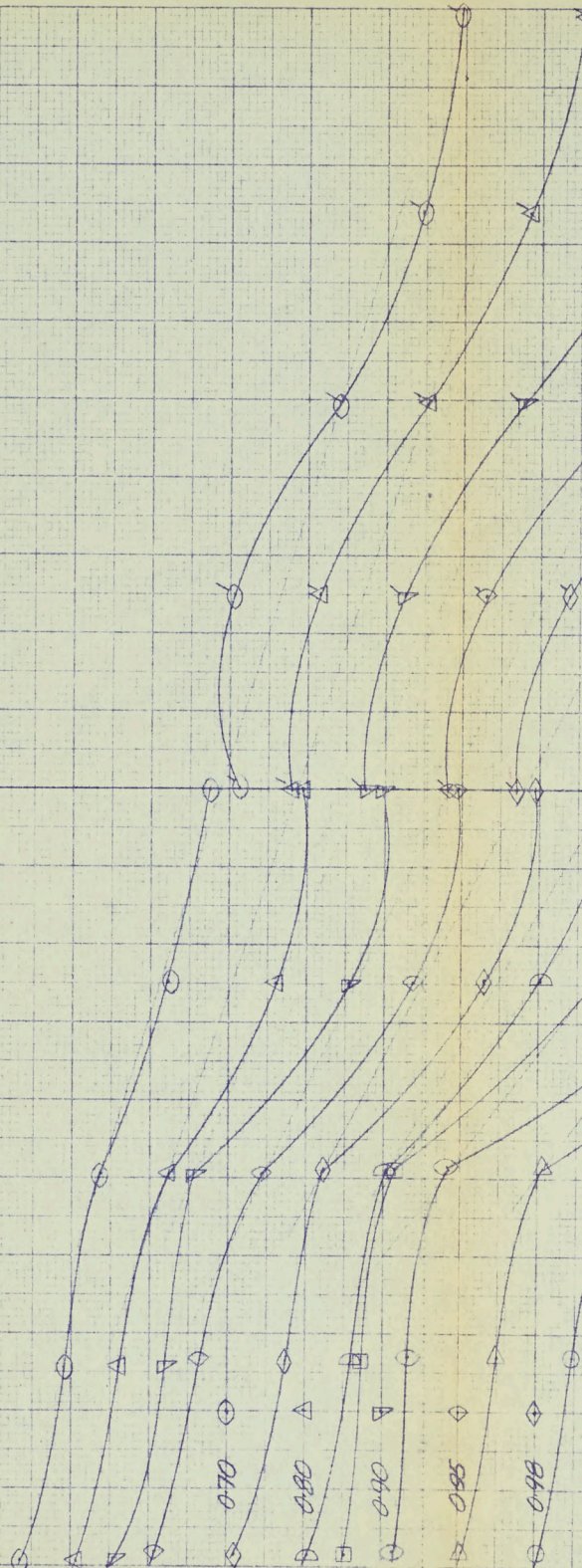
C_{A2} vs d_a

$\alpha = 20^\circ$

C_{A0}

$$\delta_e = \delta_r = 0^\circ$$
$$\beta = 0^\circ$$
$$-20^\circ \leq \delta_a \leq +20^\circ$$

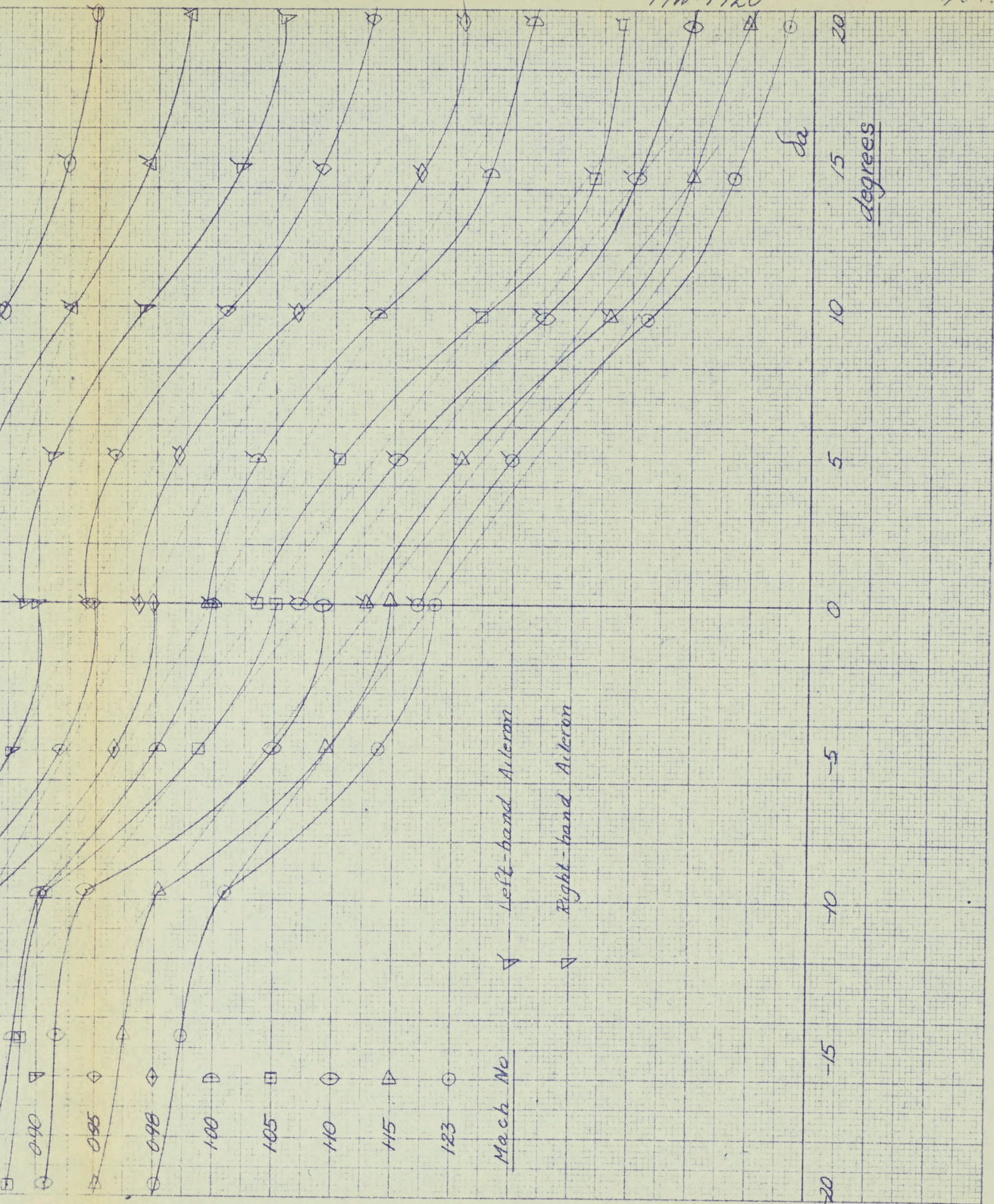
Configuration $B_0 C_2 M_3 K_2 B_3$



C.A. Ford
P/W-T/20

May 1954

A 3.1.



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C-105

C.A.L. W-T Tests

Ch_{5a} vs Mach No.

$\alpha = 2^\circ$

Ch_{5a}
per degree

-0020

-0010

0

Mach Number

1.1

1.0

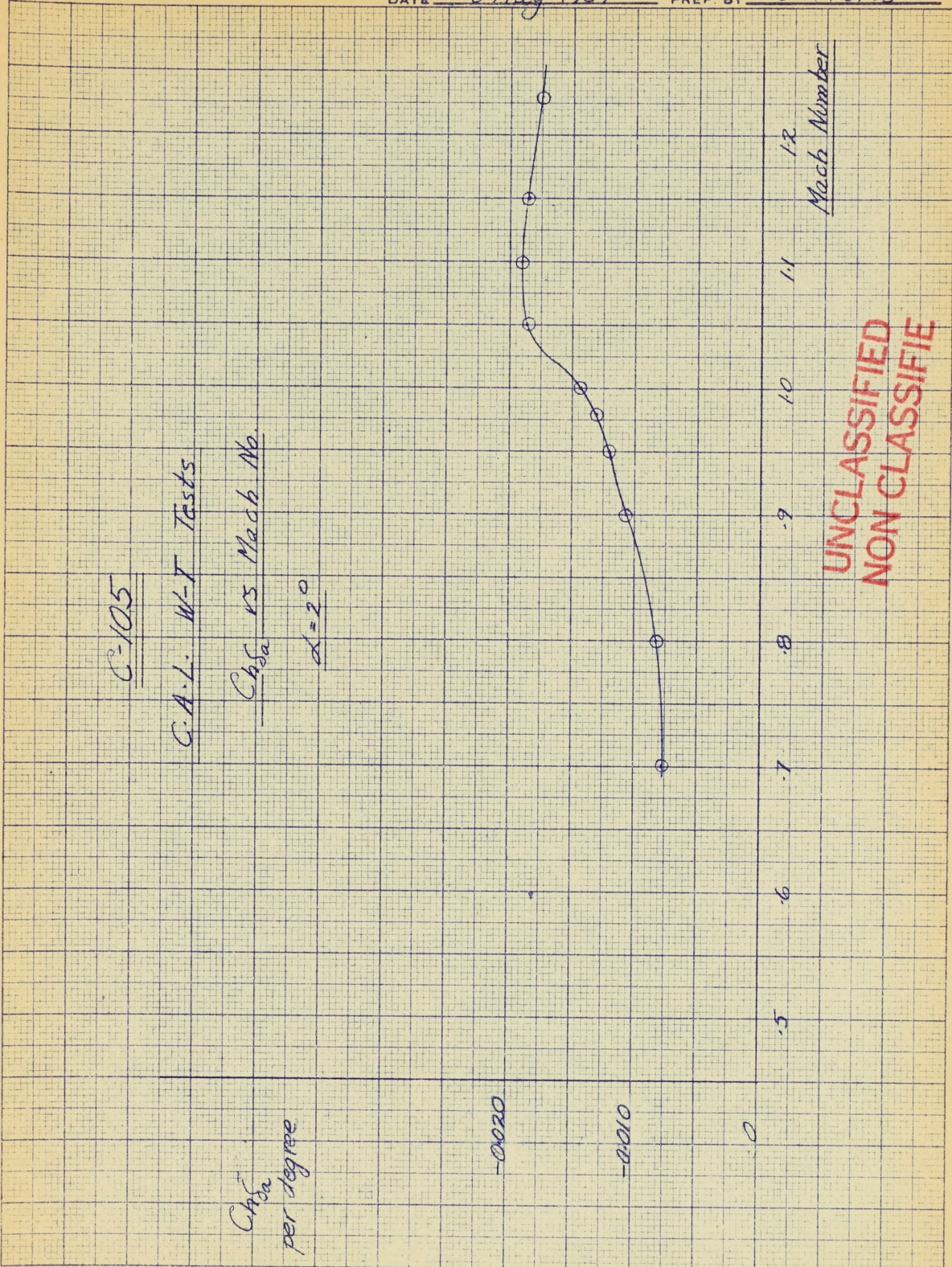
.9

.8

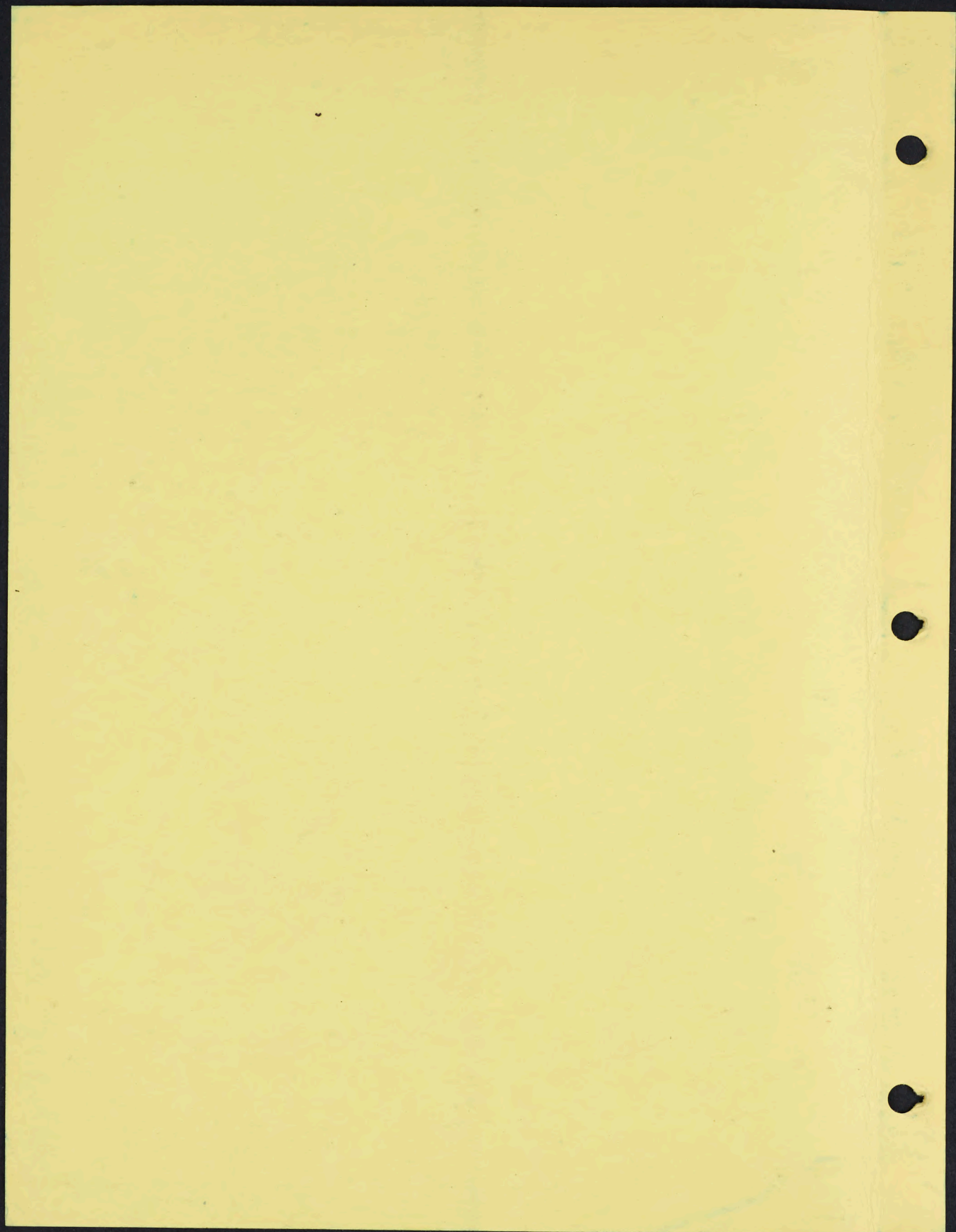
.7

.6

.5



UNCLASSIFIED
NON CLASSIFIE



OU-TANG
3558
MADE IN U.S.A.