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ANNEXE
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June 10, 1957.

M.A. Pesando, Chief Project Research Engineer.

W. Kuzyk, Senior Project Research Engineer.

The design report of the reconnaissance version of the Arrow
No. 1 fighter was shown on 6-7-57 at 10,000 ft. altitude. This version
requires a considerable reduction in both take off and landing speed as well
as doubling the rate of climb. This version requires a considerable
reduction in the rate of climb.

Herewith attached is Reconnaissance Arrow Drag and Power
Summary.

The configuration proposed for a reconnaissance version is shown
in Figure 1, and the pertinent data are as follows:

Summary

Wing Area	40 = 1410 sq. ft.
Canard Area	40 = 12 sq. ft.
Vertical Fin Area	40 = 12 sq. ft.
Side Fin Area	40 = 12 sq. ft. (vertical)
Fuselage	40 = 12 sq. ft.
Rudder	40 = 12 sq. ft.
Alarons	40 = 12 sq. ft.

W. Kuzyk

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cc: R.F. Marshall.

Wing Tip Devices	1,000 lb.
Canard (12 sq. ft.)	200 lb.
Additional Wing Area	700 lb.
Side Fin (12 sq. ft.)	200 lb.
Additional Rudder	10 lb.
(12 sq. ft.)	10 lb.

Reconnaissance Arrow - O.S.E. 49,714 lb.

Internal Fuel	19,000 lb.
Less Outer Wing	1,000 lb.

Reconnaissance Arrow - Fuel Internal Fuel 18,000 lb.

1000 Pounds Reconnaissance Arrow

Plus One External Tank - Fuel	1,000 lb.
Plus Two External Wing Tanks	- Fuel 1,000 lb.
Plus Tank Structures	1,000 lb. 11,000 lb.
Total	35,412 lb.

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RECONNAISSANCE ARROW DRAG AND POWER SUMMARY

by W. Kuzyk

1.0 INTRODUCTION

The design target of the reconnaissance version of the Avro Arrow Mk. 3 fighter was chosen as $M = 2.5$ at 90,000 ft. altitude. This choice requires a considerable reduction in both trim and induced drag as well as doubling of power at altitude. This greatly improved performance capability provides the reconnaissance airplane with a very useful "dash" for (1) evading potential enemies and (2) for positioning prior to the observance and photographing of target areas.

The configuration proposed for a reconnaissance version is shown on figure 9, and the pertinent data are as follows:

Geometry

Wing Area	$S_w = 1410 \text{ ft.}^2$
Canard Area	$S_c = 32 \text{ ft.}^2$
Aspect Ratio	$AR = 2.65$
Side Fins	$S_{SF} = 90 \text{ ft.}^2 \text{ (total)}$
Fin	$S_F = 170 \text{ ft.}^2$
Rudder	$S_R = 50 \text{ ft.}^2$
Ailerons	$S_A = 100 \text{ ft.}^2 \text{ (total)}$

Weight Estimate

Mk. II O.W.E. (incl. arm. & cameras)	44,214 lb.
Wing Tip Ramjets	3,600 lb.
Canard (32 ft. ²)	200 lb.
Additional Wing Area (155 ft. ²)	750 lb.
Side Fins (90 ft. ²)	400 lb.
Additional Rudder (12 ft. ²)	50 lb.

Reconnaissance Arrow - O.W.E. 49,214 lb.

Fuel Internal Fuel	19,438 lb.
plus Outer Wing	6,000 lb.

Arrow - Full Internal Fuel 25,438 lb.
74,652 lb.

Long Range Reconnaissance Arrow

Plus One External Tank - Fuel	5,000 lb.
Plus Two External Wing Tanks	
- Fuel	5,000 lb.
Plus Tank Structure	1,000 lb. 11,000 lb.
Total	85,652 lb.

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Undercarriage Development

From the foregoing it is felt that the probable high T.O. weight will warrant some development of the undercarriage. In this regard it is highly recommended that a design stress analysis be carried out on two design proposals.

- (a) increasing capacity of present U/C design (Mk. II)
- (b) Check the feasibility of the addition of outriggers at the wing tips

to cater for an increased normal T.O. weight of the order of 90,000 lb.

Location of Canard

The canard has been tentatively positioned so that there is minimum interference to the pilot's vision and to the intake. (Note that at altitude the fuselage angle of attack is around 10° .) However further study is required.

2.0 DRAW SUMMARY

A drag analysis of the Avro Arrow Mk. II showed that at $M = 2.5$, 90,000 ft. altitude and a $W/P = 250,000 \text{ in.}^2$ the drag components to be

	<u>D/P in.²</u>	<u>D lb.</u>	<u>% of Total</u>
Profile Drag	16,600	4,080	18.5
Induced Drag	45,200	11,080	50
Trim Drag	28,200	6,960	31.5
	90,000	22,120	

The profile drag is a "fixed item" and any improvement of it was unlikely. Therefore the reduction is more probable in induced and trim drags. Increasing the wing area from 1225 ft.² to 1410 ft.² and the addition of the canard resulted in the following:

	<u>D/P in.²</u>	<u>D lb.</u>	<u>% Total</u>	<u>% Change over Mk. II</u>
Profile Drag	19,900	4,900	37.5	+20%
Induced Drag	28,250	6,950	53.0	-37%
Trim Drag	5,600	1,230	9.5	-82%
	53,750	13,080		-41%

The separate effects of increasing the wing area, and addition of a canard is clearly shown in fig. 7. It follows then that modification of the Avro Arrow for increased speed and altitude should include a canard. The trim effect of the canard elevator combination is shown in fig. 6. Point "A" shows the trim drag to be $28,800 \times .246 \text{ psi} = 7,100 \text{ lb.}$ for zero canard effect and a required -26° elevator angle, however utilization of the canard (see point "B") to the extent of its buffet limit results in a trim drag of $5600 \times .246 \text{ psi} = 1230 \text{ lb.}$ for α_c canard = $+23^\circ$ and δ_e elevator = -8° - a reduction of 5,870 at $M = 2.5$, 90,000 ft. $W/P = 250,000$.

It is noteworthy that total drag of this version at $M = .92$, 22,000 ft. altitude, $W/P 22,000$ is 7,000 lb. as compared to 6,660 lb. for the Avro Arrow Mk. II at the same speed, altitude, and weight and this is not too great an increase in drag during a subsonic "cruise".

At $M = 2.5$ at 90,000 ft. altitude for an operational weight of 61,400 lb. requires a total of 13,000 lb. thrust, with 7,000 lb. being contributed by the Iroquois engines with after-burning, and the balance of 6,000 lb. by some other power source. Recommended on fig. 9 are wing tip ramjet pods.

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3.0 POWER PLANT OPTIONS

The additional 6000 lb. thrust may be obtained by several different combinations of power plant and fuels, some of which are listed below:

	Powerplant	Fuel			
		Turbojet	A/B	Ramjet	Rocket
1	(Turbojet + A/B) + Ramjet	JP4	JP4	JP4	
2	(Turbojet + A/B) + Ramjet	JP4	JP4	Pentaborane	
3	(Turbojet + A/B) + Ramjet	JP4 + H ₂ O	JP4	JP4	
4	(Turbojet + A/B) + Ramjet	JP4 + H ₂ O	JP4	Pentaborane	
5	(Turbojet + A/B) + Rocket	JP4	JP4		855H-02 15000

Some of the characteristics of each combination are tabulated in Table 1. following.

The fuel consumed during a dash of M 2.5, 90,000' alt. and $W/P = 250,000'$ for a Reconnaissance Arrow shows that combinations (1) and (2) are the best (see fig. 10). Since combination (2) involves the use of solid fuels and that the gains afforded by the use of High Energy fuels are not great it is felt that combination (1) is the most suitable for the Reconnaissance Arrow, and this combination is shown in fig. 9.

The use of high energy fuels such as pentaborane results in a decrease of ramjet frontal area from 14.1 ft.² to 11.9 ft.² (4.25 to 3.9' dia.) and a reduction of specific fuel consumption from 3.15 to 2.57. Somewhat lesser gains are to be realized from the use of a Boron Slurry.

Water injection is an easy way of "souping up" existing power plant and intake combinations. However, this feature is somewhat curtailed by the large increase in specific fuel consumption, e.g. the recommended Reconnaissance Arrow power plant combination would use at least 2½ times more liquid fuel by weight when water is injected into the turbojet intakes to the saturation point.

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4. RECOMMENDATIONS - FURTHER INVESTIGATIONS

The indications of this note are that a M = 2.5, 90,000' altitude Reconnaissance Arrow is feasible within the present state of art. However, it needs to be immediately established whether there is a need for a reconnaissance or tactical bomber version of the Arrow via Market Research. Further, power investigations are also recommended with an effort to improving the range potential of the Arrow.

With respect to the Reconnaissance Arrow two plausible locations for reconnaissance equipment are:

- (a) In the two inner stalls of the armament bay, thus removing $\frac{1}{2}$ of the armament.
- (b) In an extended portion of the nose section aft of the radar, thus maintaining full armament.

Further investigations are required to substantiate this. Some of the more important items to be looked into more fully are lined in table 2.

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C105 DRAG ESTIMATE
AT M=2.5

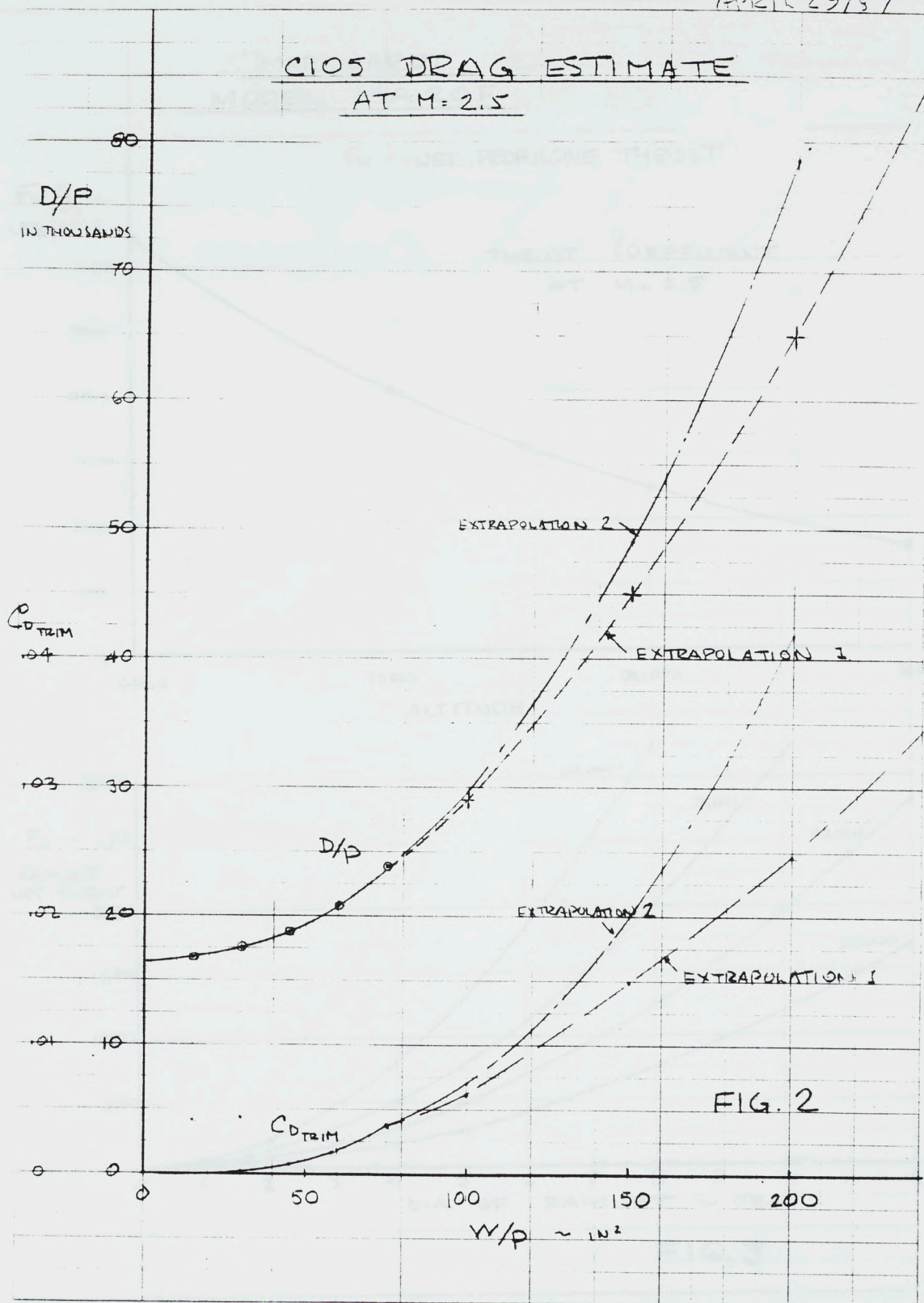


FIG. 2

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APRIL 27, 1957

MARQUARDT
MODEL MIA 20F

F_u = NET PROPULSIVE THRUST

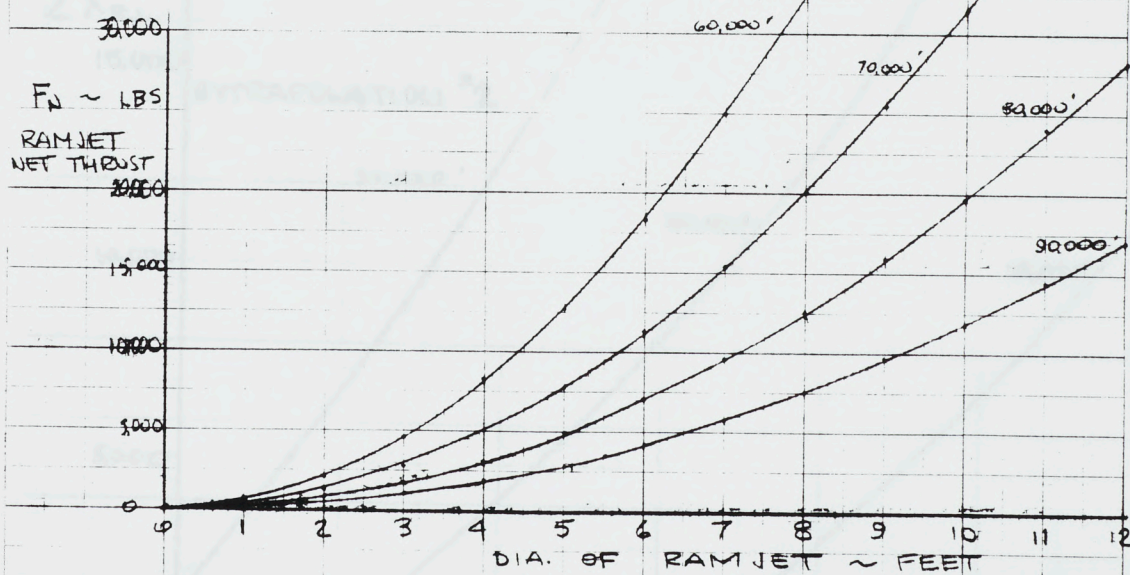
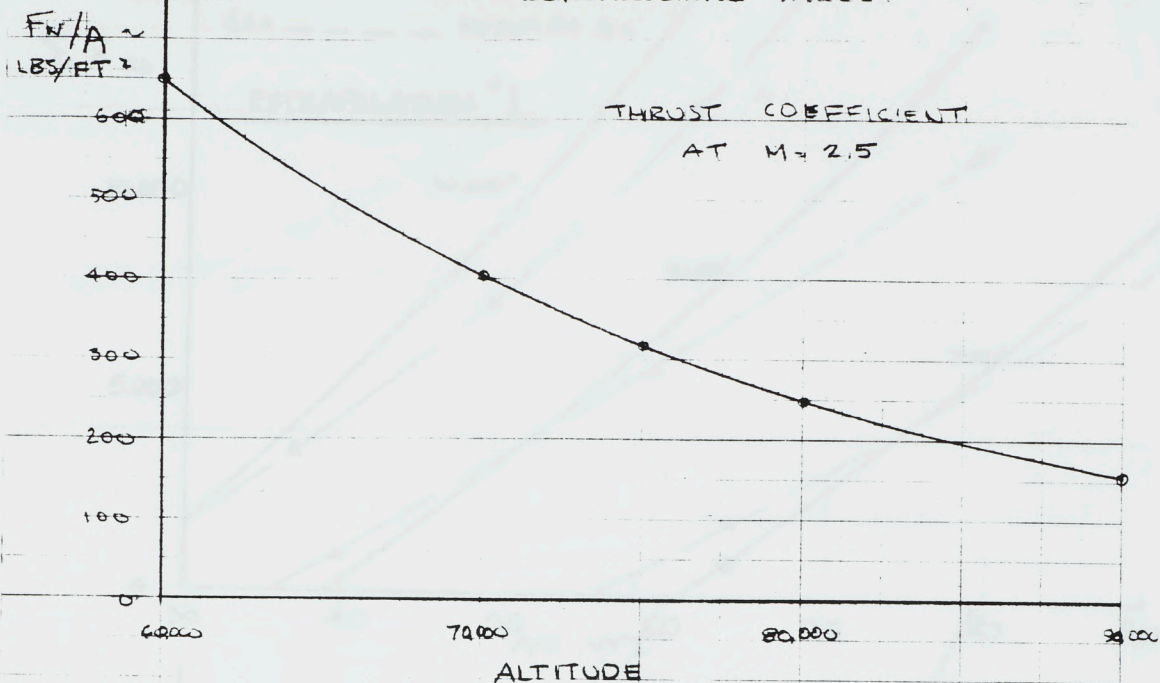
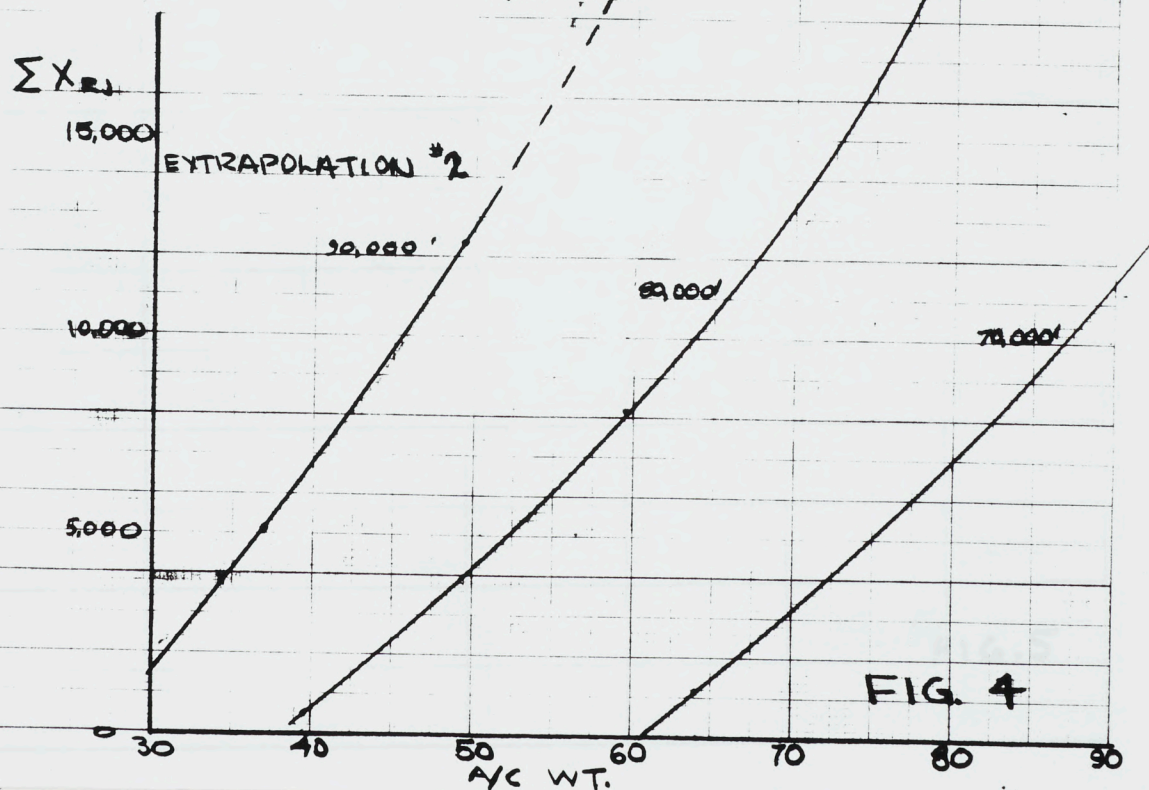
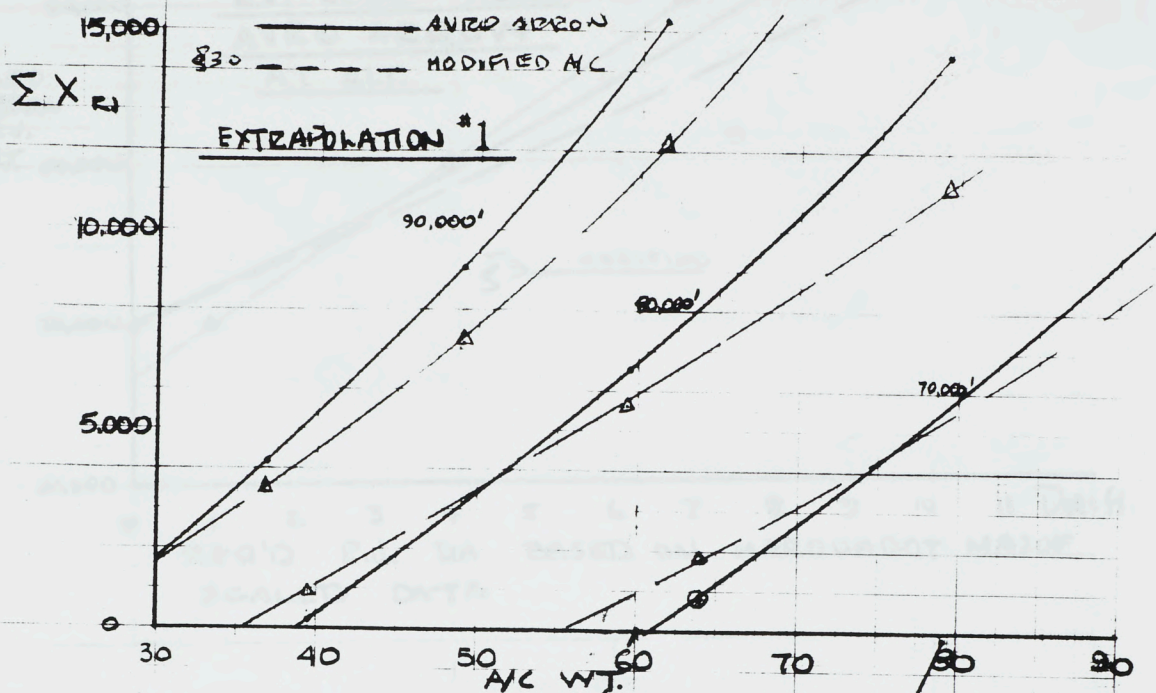


FIG. 3

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TOTAL RAMJET THRUST REQ'D TO
ACHIEVE M 2.5 AT ALT.



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W. King

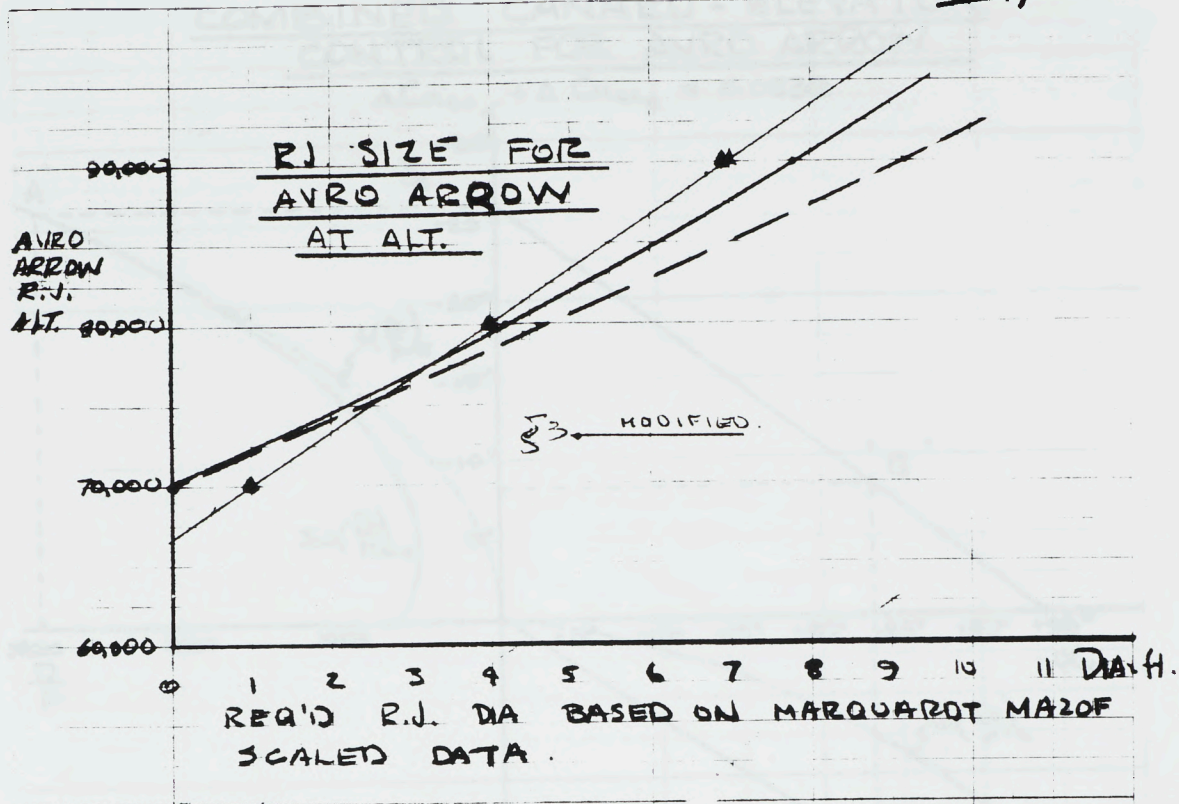


FIG. 5

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W. Knight

DRAG REDUCTION SUMMARY

W/P = 250,000, ALT = 90,000'

M = 2.5

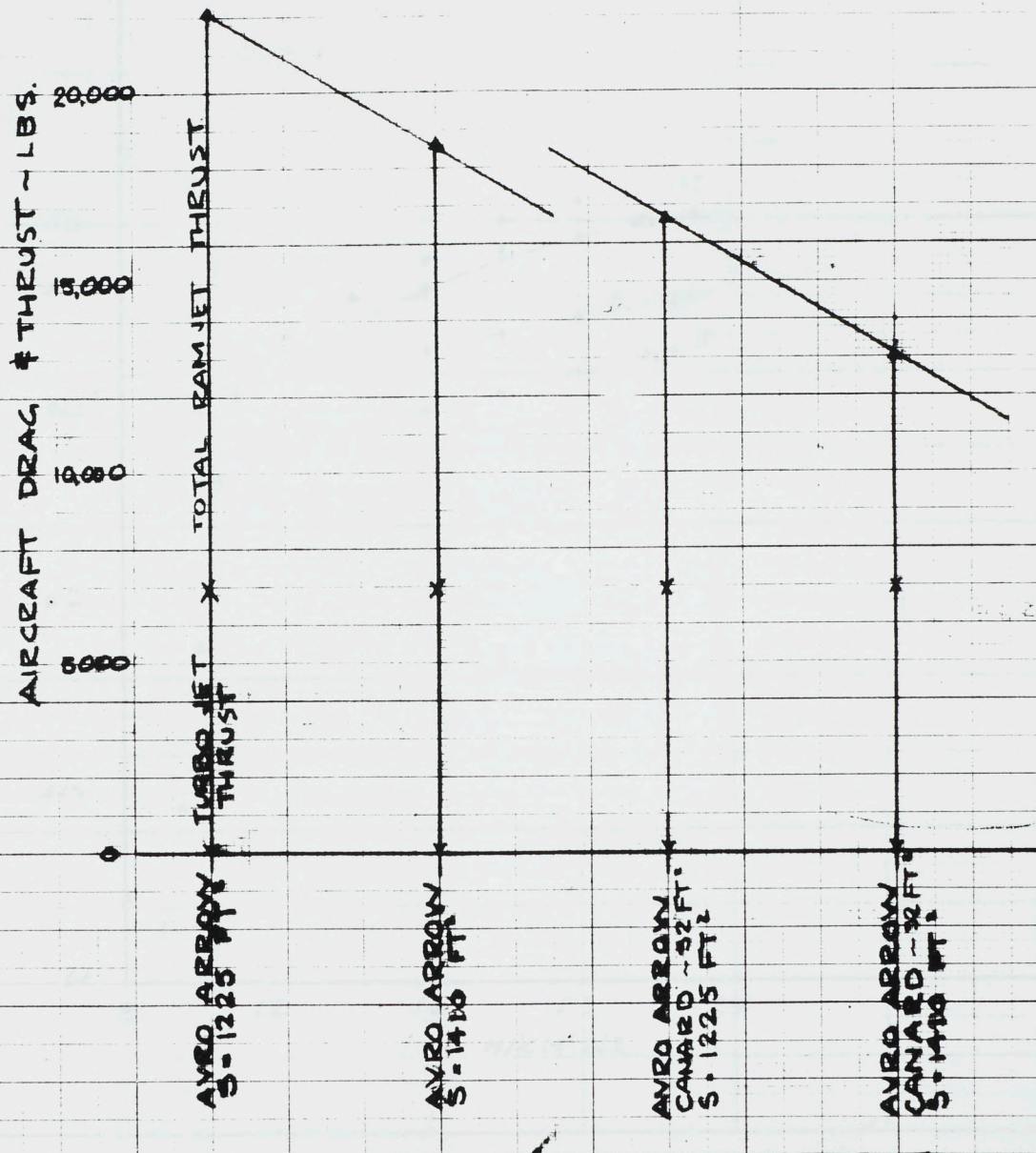
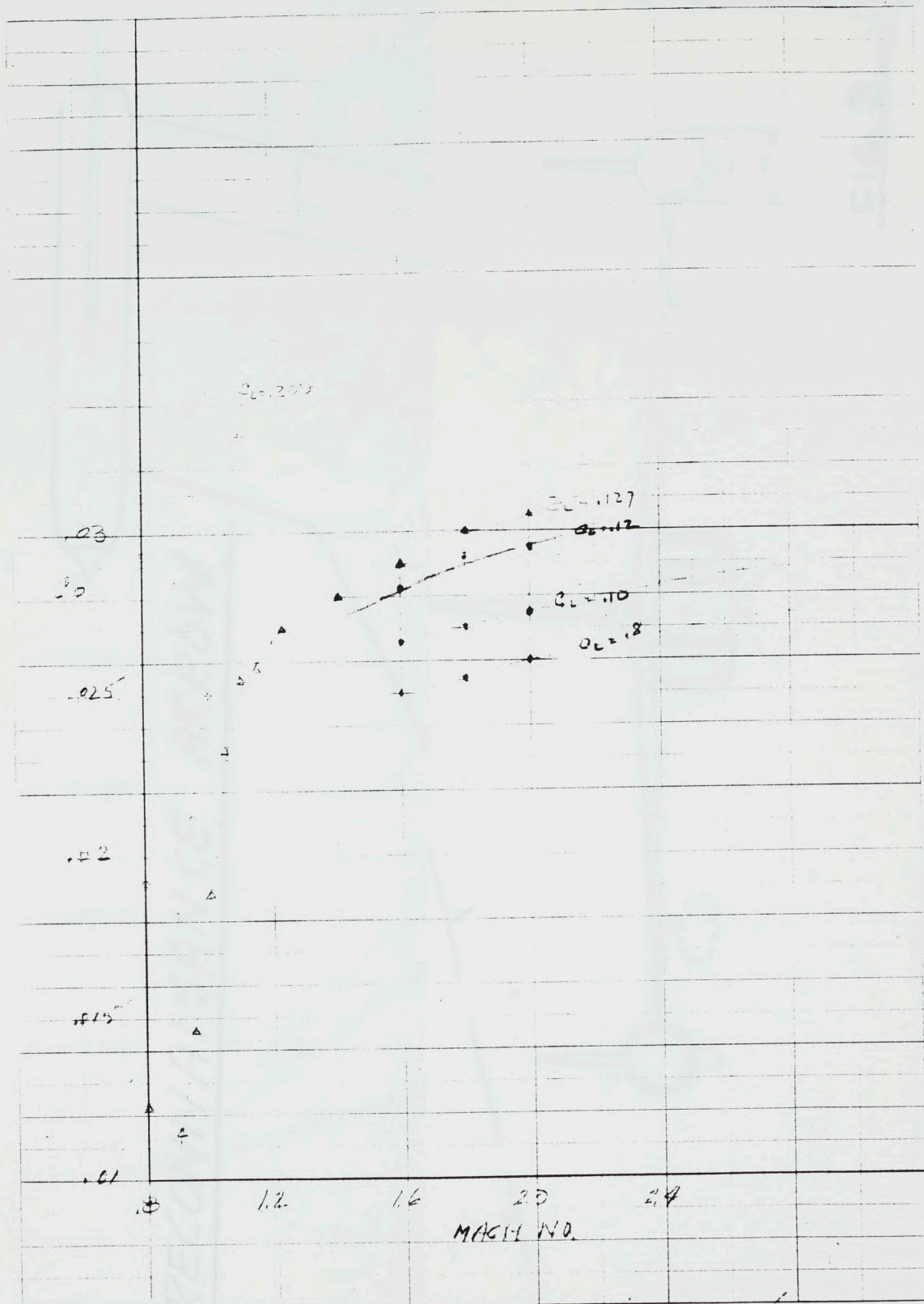
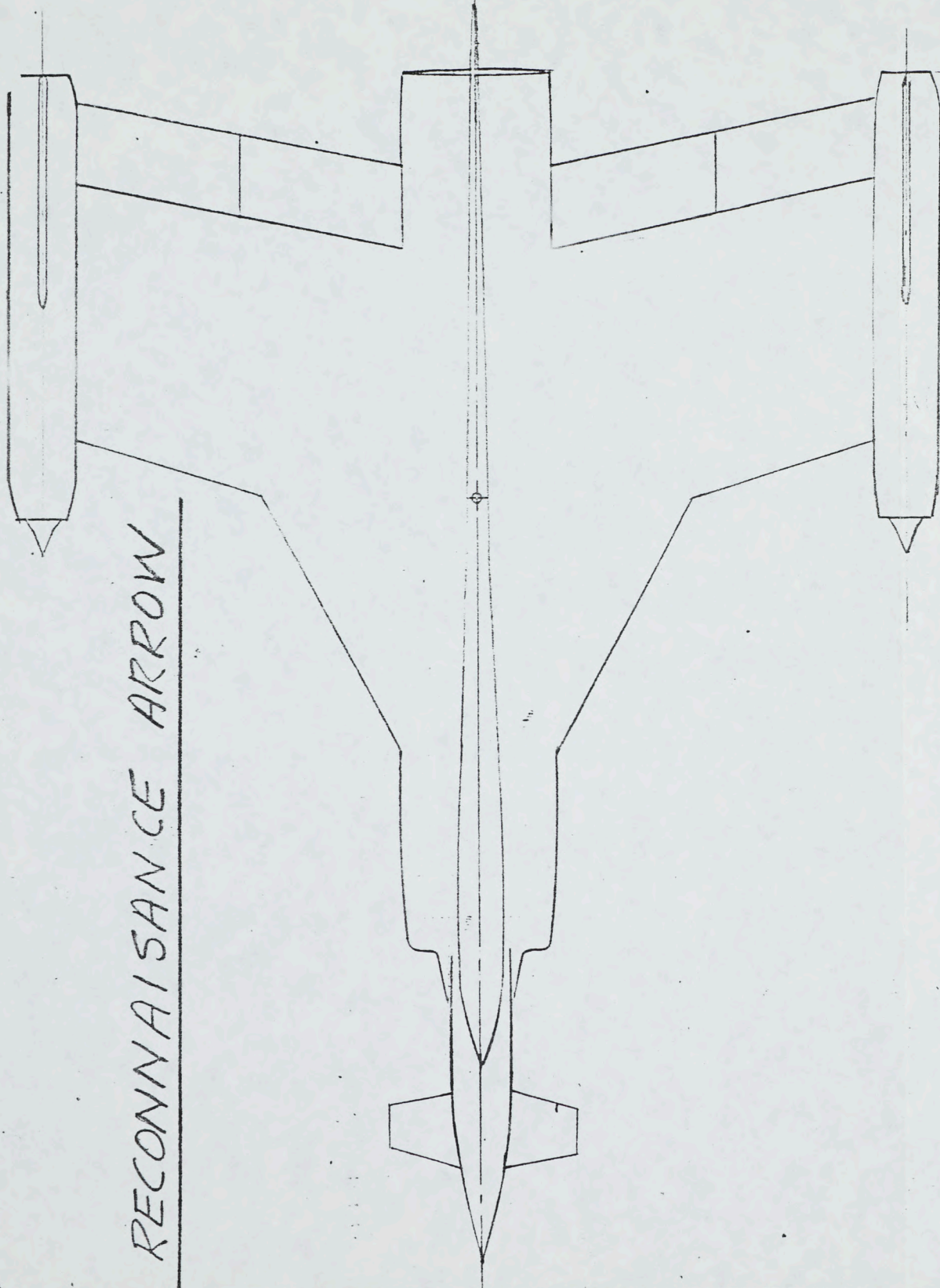


FIG. 7

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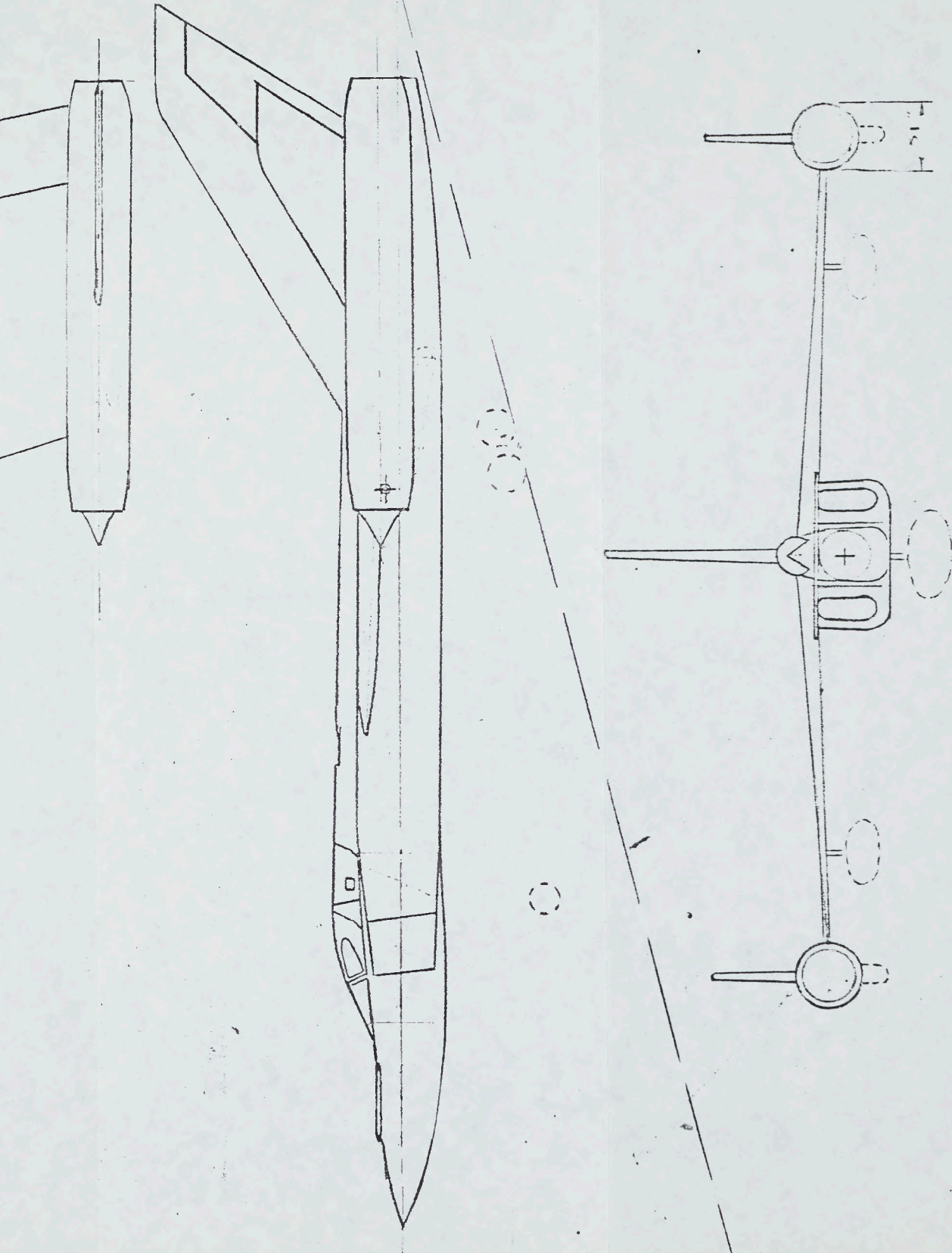


RECONNAISSANCE ARROW



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FIG. 9



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FUEL CONSUMPTION
DURING A DASH AT M=2.5
90000 FT ALT. * W/P = 250,000 IN²

NOTE SEE TABLE 1 FOR CODE

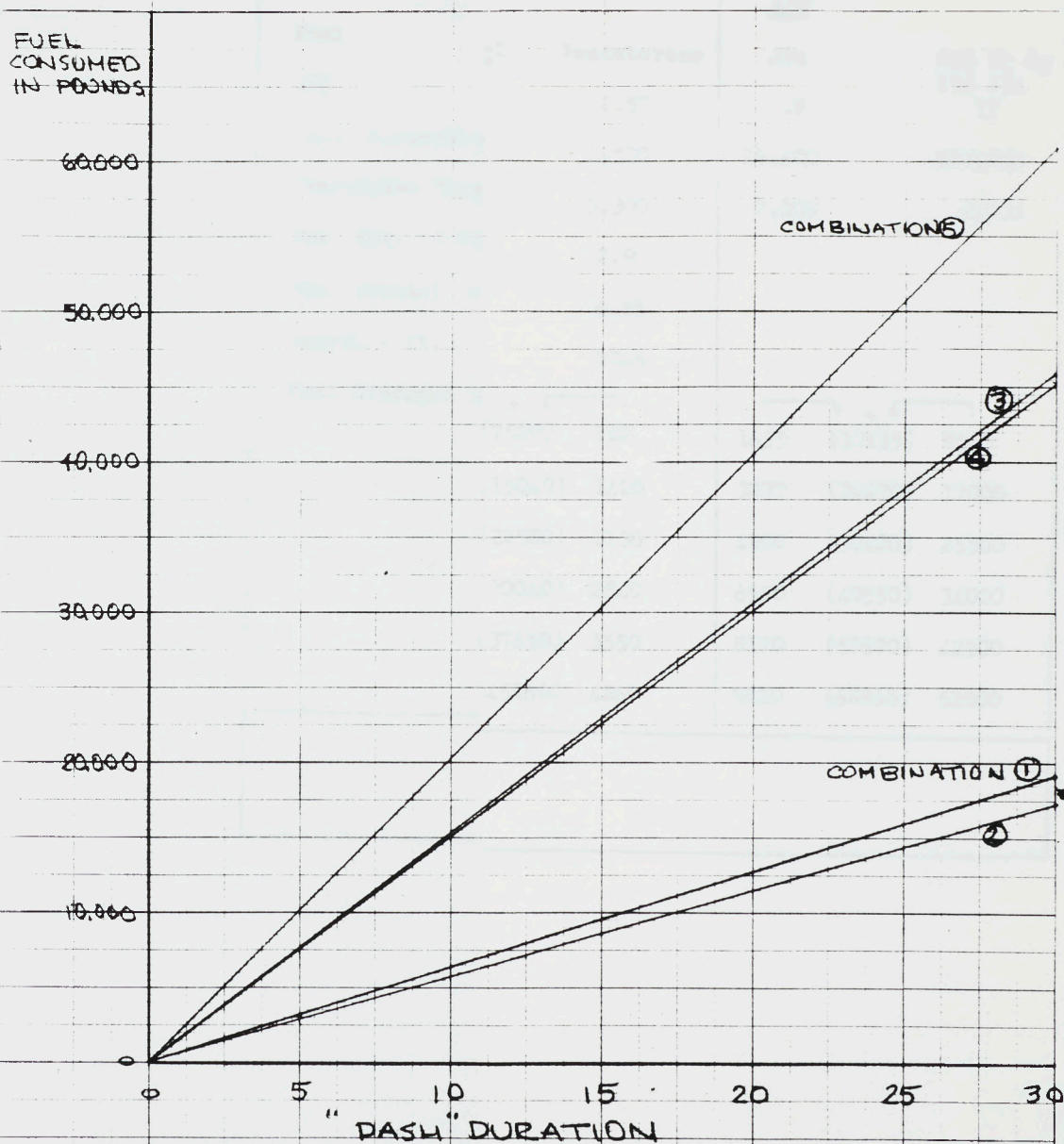


FIG. 10

TABLE 1

Power Plant Summary S M 2.5, 90

<u>Power Plant Combination</u>	①		③	
	<u>Turbojet</u> + <u>A/B</u>	<u>Ramjet</u>	<u>Turbojet</u> + <u>A/B</u>	<u>Ramjet</u>
Fuel	JP4	JP4	JP4 + H ₂ O	J
SFC	2.8	3.15	3.42	3
Fuel Consumption lb./hr.	19,600	18,900	21,700	10
Propulsive Thrust lb.	7,000	6,000	9,700	3
Max. Dia. - ft.		4.25		3
Max. Frontal Area - ft. ²		14.1		7
Length - ft.		30		22
Fuel Consumed in Pounds	↓ + ↓		↓ + ↓	
- 5 min.	1635	(3210)	1575	6310 (7670) 86
- 10 min.	3270	(6420)	3150	13620 (15340) 17
- 15 min.	4900	(9620)	4720	20450 (23030) 25
- 20 min.	6550	(12850)	6300	27200 (30640) 34
- 25 min.	8170	(15050)	7880	34100 (38400) 43
- 30 min.	9810	(19260)	9450	40800 (45960) 51

NOTE: "Saturation" water injection considered in this tab

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TABLE 1

Summary @ M 2.5, 90,000' Alt., W/P = 250,000 in.²

③		②		④		⑤	
<u>Turbojet</u> + <u>A/B</u>	<u>Ramjet</u>	<u>Turbojet</u> + <u>A/B</u>	<u>Ramjet</u>	<u>Turbojet</u> + <u>A/B</u>	<u>Ramjet</u>	<u>Turbojet</u> + <u>A/B</u>	<u>Pocket</u>
JP4 + H ₂ O	JP4	JP4	Pentaborane	JP4 + H ₂ O	Pentaborane	JP4	85% H ₂ O ₂ 15% JP4 17
8.42	3.15	2.8	2.57	8.42	2.57	2.8	
81,700	10,300	19,600	15,430	81,700	8,500	19,600	102,000
9,700	3,300	7,000	6,000	9,700	3,300	7,000	6,000
	3.14		3.9		2.9		
	7.25		11.9		6.55		
	22		27.5		20.5		
6810 (7670) 860		1635 (2923) 1288		6810 (7520) 710		1635 (10135) 8500	
13620 (15340) 1720		3270 (5845) 2575		13620 (15040) 1420		3270 (20270) 17000	
20450 (23030) 2580		4900 (8040) 3860		20450 (22580) 2130		4900 (30400) 25500	
27200 (30640) 3440		6550 (11700) 5150		27,200 (30040) 2840		6550 (40550) 34000	
34100 (38400) 4300		8170 (14610) 6440		34100 (37650) 3550		8170 (50670) 42500	
40800 (45960) 5160		9810 (17540) 7730		40900 (45160) 4260		9810 (60810) 51000	

sidered in this table.

TABLE 2

FURTHER INVESTIGATIONS OF RECONNAISSANCE ARROW

<u>Market Research</u>	<u>Possible Uses</u>	<u>Power Plant & Fuels</u>	<u>Range & Performance</u>	<u>St</u>
Is there a need for	Reconnaissance	Turbojet + A/B	Exact Range &	
(1) Reconnaissance	Tactical Bomber	Ramjet	Mission Analysis	
version with M 2.5		Rocket		
90,000' dash	Advanced Fighter	Hybrid		
		Mixed		
(2) Tactical Bomber		High Energy Fuels		
with M 2.5				
90,000' dash				
Suggest that Project	Suggest that Project	The state of art	Suggest this aspect	
Research and Sales &	Research conduct an	presently being	be looked into by	
Service investigate	operational research	investigated by	John Lucas of the	
this together, and an	study into the use-	Project Research	Technical Office	
effort be made to pro-	fullness of such	Group		
duce a specification.	vehicles in the			
	western air forces.			

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CONNAISSANCE ARROW

<u>Range & Performance</u>	<u>Stability & Control</u>	<u>Flutter & Vibration</u>	<u>Undercarriage</u>	<u>Structure & Weight Est.</u>
Alt Range & Mission Analysis	Trim control of Canard, and effect of canard and increased wing area on C.G. limits	Ramjet Buzz Flutter & Vibration of Wing	Undercarriage Development 90,000 lb. T.O. Weight and 65,000 lb. landing weight	Weight estimate of Arrow
Suggest this aspect be looked into by Stan Lucas of the Technical Office	Suggest this aspect be looked into by Stan Kwiatkowski of the Technical Office	Suggest this aspect be looked into by John McKillop	W. Alford of the Stress Office indicated an interest in this problem.	Suggest this aspect be looked into by Al Sentance of the Initial Project Office.

